# Bryant Development and Review Committee Meeting

Boswell Municipal Complex - City Hall Conference Room

210 SW 3rd Street

**Date:** July 17, 2025 - **Time:** 9:00 AM

## Call to Order

## Old Business

## New Business

**1. Bryant Schools - ALE Addition** - 1200 S Reynolds Road

*Josh Minton - Requesting Approval for Site Plan Addition*

- 0974-DRN-01.pdf
- 0974-PLN-02.pdf
- 0974-RSP-01.pdf

**2. The Shoppes at Dogwood Springs** - Final Plat

*Richardson Engineering - Requesting Recommendation for Approval of Final Plat*

- 0978-LTR-01.pdf
- 0978-PLT-01.pdf

**3. New Beginnings** - Hwy 5 and Midland Road

*PLE - Requesting Site Plan Approval*

- 0977-PLN-01.pdf
- 0977-DRN-01.pdf
- 0977-ARCH-01.pdf

**4. Good Day Farms - 3205 HWY 5** - Site Plan

*Regan Ethridge - Requesting Site Plan Approval*

- 0967-DRN-01.pdf
- 0967-PLN-02.pdf

**5. Springhill Tavern - 2224 Brandon Loop** - Site Addition

*Ronnie Beard - Requesting Approval for New Building Addition*

- 0979-PLN-01.pdf

**6. REQUEST TO ADD: Creekside Addition Ph 2 - Replat** - Lot 15

*GarNat Engineering - Requesting Recommendation for Approval of Replat*

- 0980-APP-01.pdf
- 0980-LTR-01.pdf

- 0980-PLT-01.pdf

## Staff Approved

**7. Kinfolk Acres - 22000 I-30 - Sign Permit**

*Ace Sign Company - Requesting Sign Permit Approval - STAFF APPROVED*

- 93885-SGN-01.pdf

**8. Wine Night - 6221 Hwy 5 - Sign Permit**

*Amy Clark - Requesting Sign Permit Approval - STAFF APPROVED*

- 93928-SGN-01.jpeg

**9. FCPS - 212 McClanahan Dr - Sign Permit**

*Lumatech - Requesting Sign Permit Approval - STAFF APPROVED*

- 93974-SGNAPP-01.pdf

## Adjournments

# Bryant ALE Addition

# Stormwater Management Report

City of Bryant, Saline County, Arkansas

Original Submittal:
July 9, 2025

**MINTON ENGINEERING, INC.**
300 Northport Dr.
Cabot, AR 72023
501.941.5559 phone
501.941.5557 fax

## I. Pre-Development Conditions

This property is located at the southwest corner of Wilkerson & Reynolds Roads. The site is developed and is currently occupied by the Bryant Schools ALE program. The site has two drainage areas and is split almost in half draining east and west.

## II. Post-Development Conditions

This project will construct a 3,500 SF addition on the west side of the existing building along Wilkerson Road. The drainage patters for this property will remain the same except for an additional 0.11 acres of hard surface added to the west drainage area.

## III. Design Considerations

The detention for this project was designed using the rational method. The pre-development flow and post development flow were determined by the attached calculations are summarized below. The calculations were compiled using Autodesk Hydraflow, information used is attached to this report.

Only Drainage Area 1 is shown in the Summary Table, there were no changes to Drainage Area 2.

**Summary Table:**

| Description | Pre-Dev DA 1 | Post-Dev DA 1 | Difference |
|---|---|---|---|
| 2-Year Storm | 2.49 cfs | 2.81 cfs | +0.32 |
| 5-Year Storm | 2.90 cfs | 3.28 cfs | +0.38 |
| 10-Year Storm | 3.21 cfs | 3.63 cfs | +0.42 |
| 25-Year Storm | 3.67 cfs | 4.15 cfs | +0.48 |
| 50-Year Storm | 4.04 cfs | 4.56 cfs | +0.52 |
| 100-Year Storm | 4.40 cfs | 4.98 cfs | +0.58 |

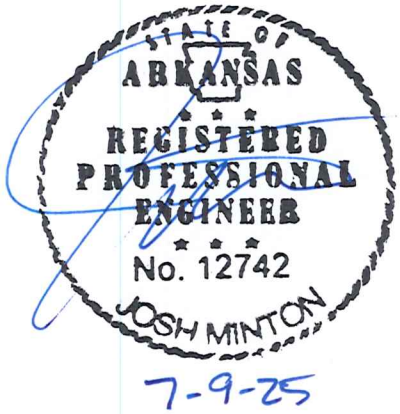
## IV. Conclusion

This development will add less than 0.6 cfs to the west drainage area for the 100-year storm. We feel this minor increase will be mitigated by the storm water running through approximately 250' of school property before reaching the residential area to the west. The drainage will run through a wooded area as well as a garden maintained by the school district.

Please consider this report and let me know if any additional information is required.

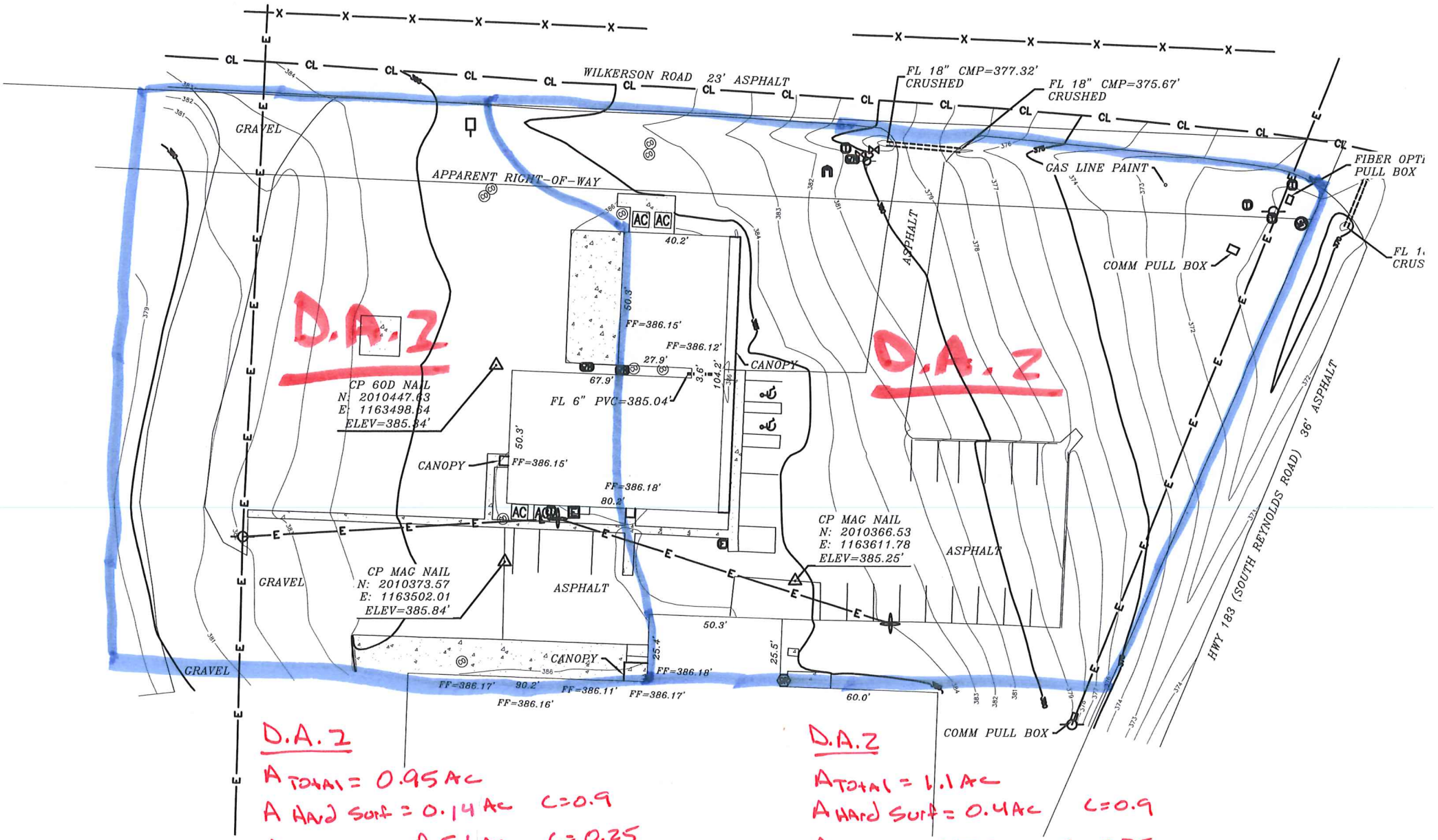
Sincerely,

Josh Minton, PE



# HYDRAULIC CALCULATIONS

# Pre-Dev. Drainage Worksheet




## D.A.2

$A_{TOTAL} = 0.95\ Ac$

$A_{Hard\ Surf} = 0.14\ Ac \quad C = 0.9$

$A_{Grass} = 0.51\ Ac \quad C = 0.25$

$A_{Gravel} = 0.3\ Ac \quad C = 0.6$

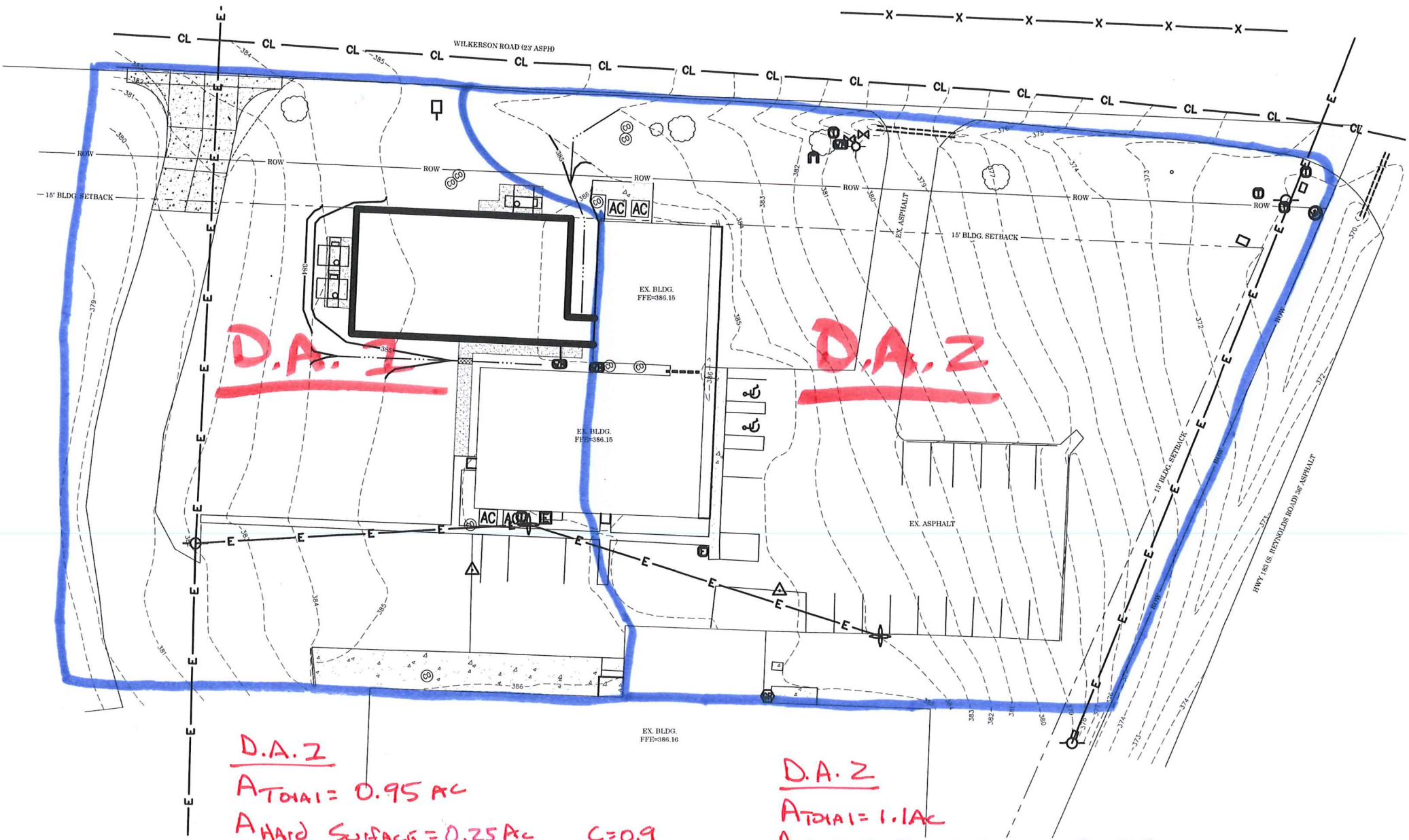
## D.A.2

$A_{TOTAL} = 1.1\ Ac$

$A_{Hard\ Surf} = 0.4\ Ac \quad C = 0.9$

$A_{Grass} = 0.7\ Ac \quad C = 0.25$

# Post-Dev. Drainage Worksheet




## D.A. 1

$A_{TOTAL} = 0.95$ Ac

$A_{Hard\ Surface} = 0.25$ Ac  $C = 0.9$

$A_{green} = 0.43$ Ac  $C = 0.25$

$A_{gravel} = 0.27$ Ac  $C = 0.6$

## D.A. 2

$A_{TOTAL} = 1.1$ Ac

$A_{Hard\ Surf} = 0.4$ Ac  $C = 0.9$

$A_{green} = 0.7$ Ac  $C = 0.25$

# Watershed Model Schematic

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 2.489 | 1 | 5 | 747 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 3.070 | 1 | 5 | 921 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 2.814 | 1 | 5 | 844 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 3.070 | 1 | 5 | 921 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report

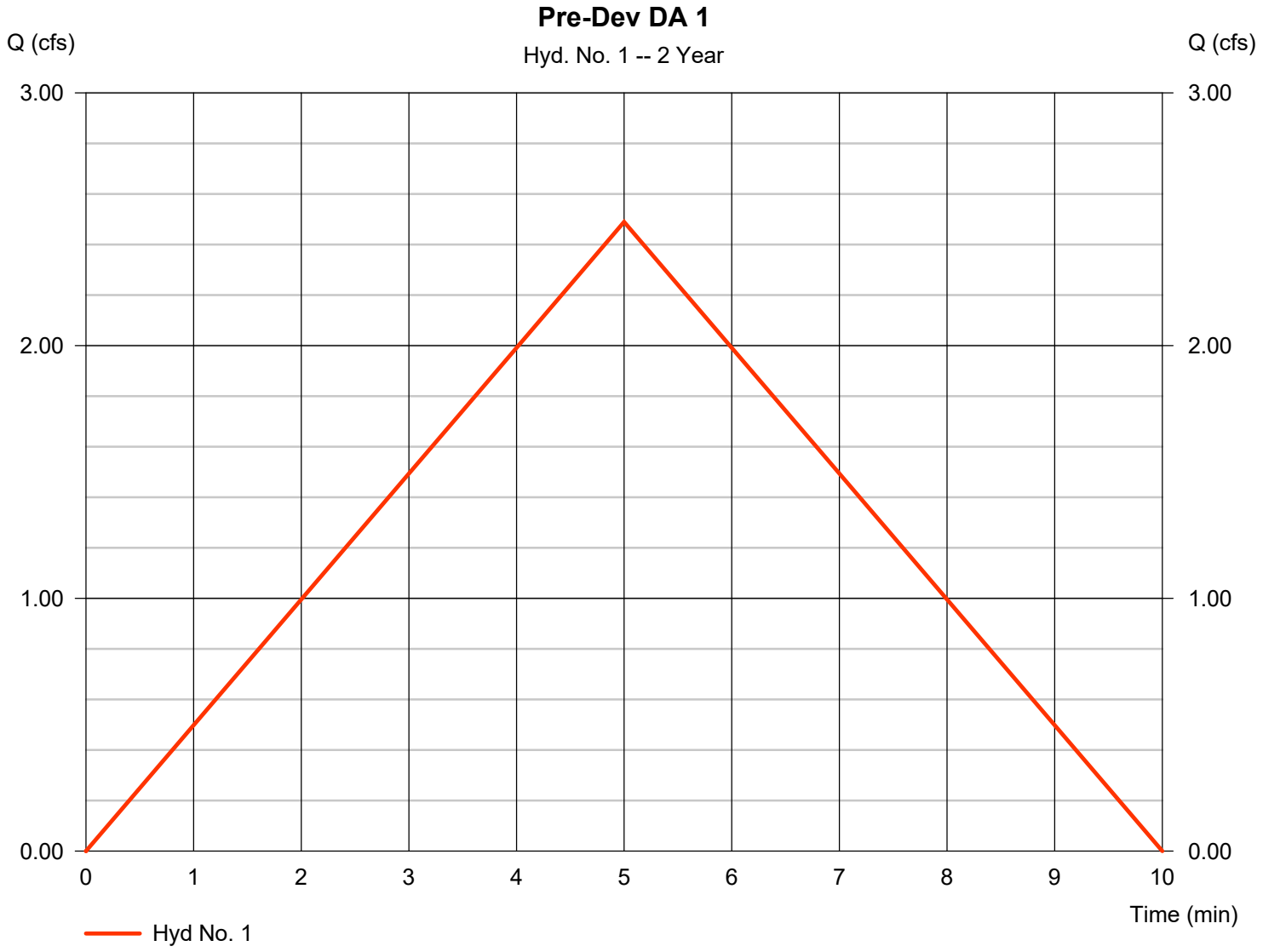


## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 2.489 cfs |
| Storm frequency | = | 2 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 747 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 5.697 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950



# Hydrograph Report

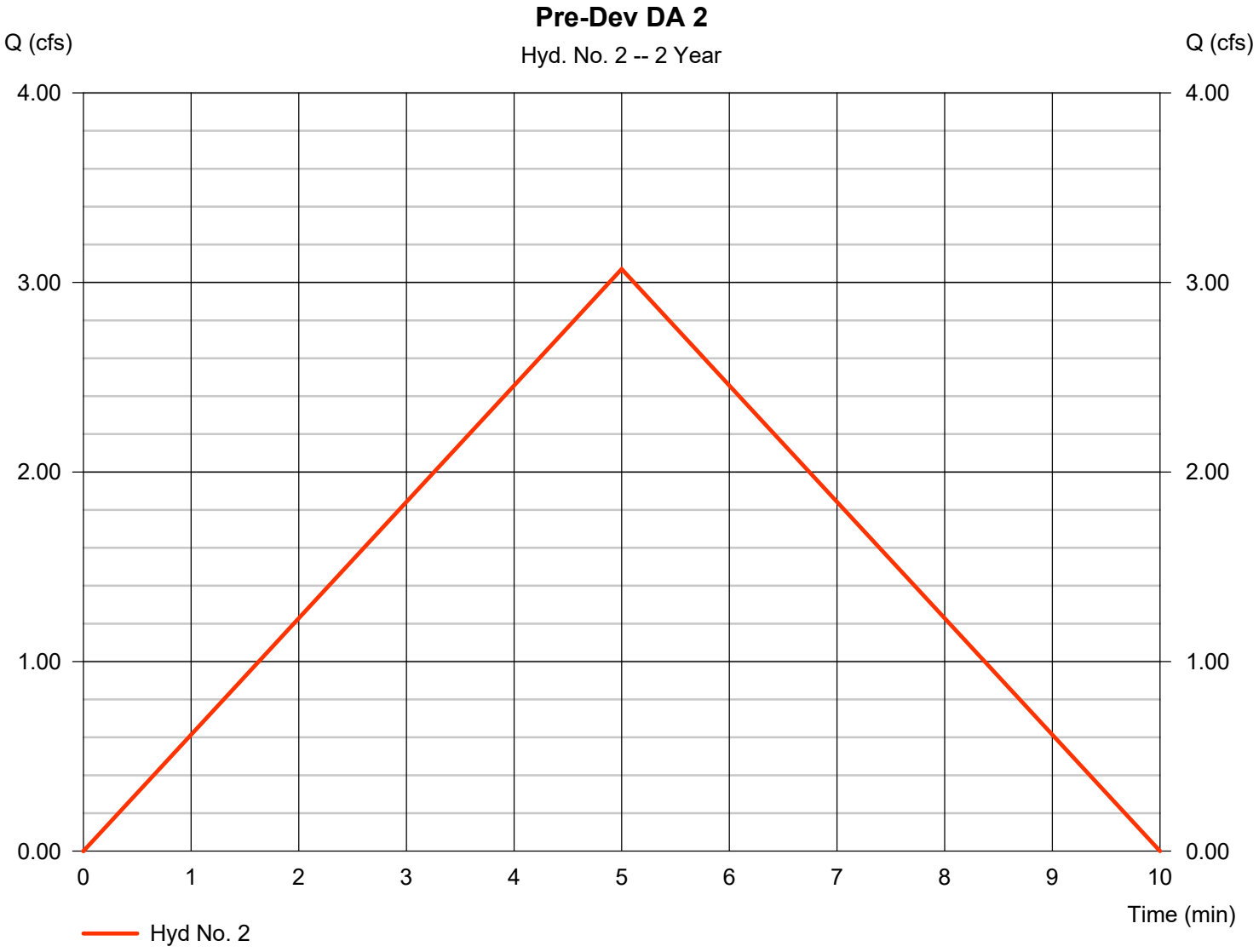


## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.070 cfs |
| Storm frequency | = | 2 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 921 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 5.697 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Report

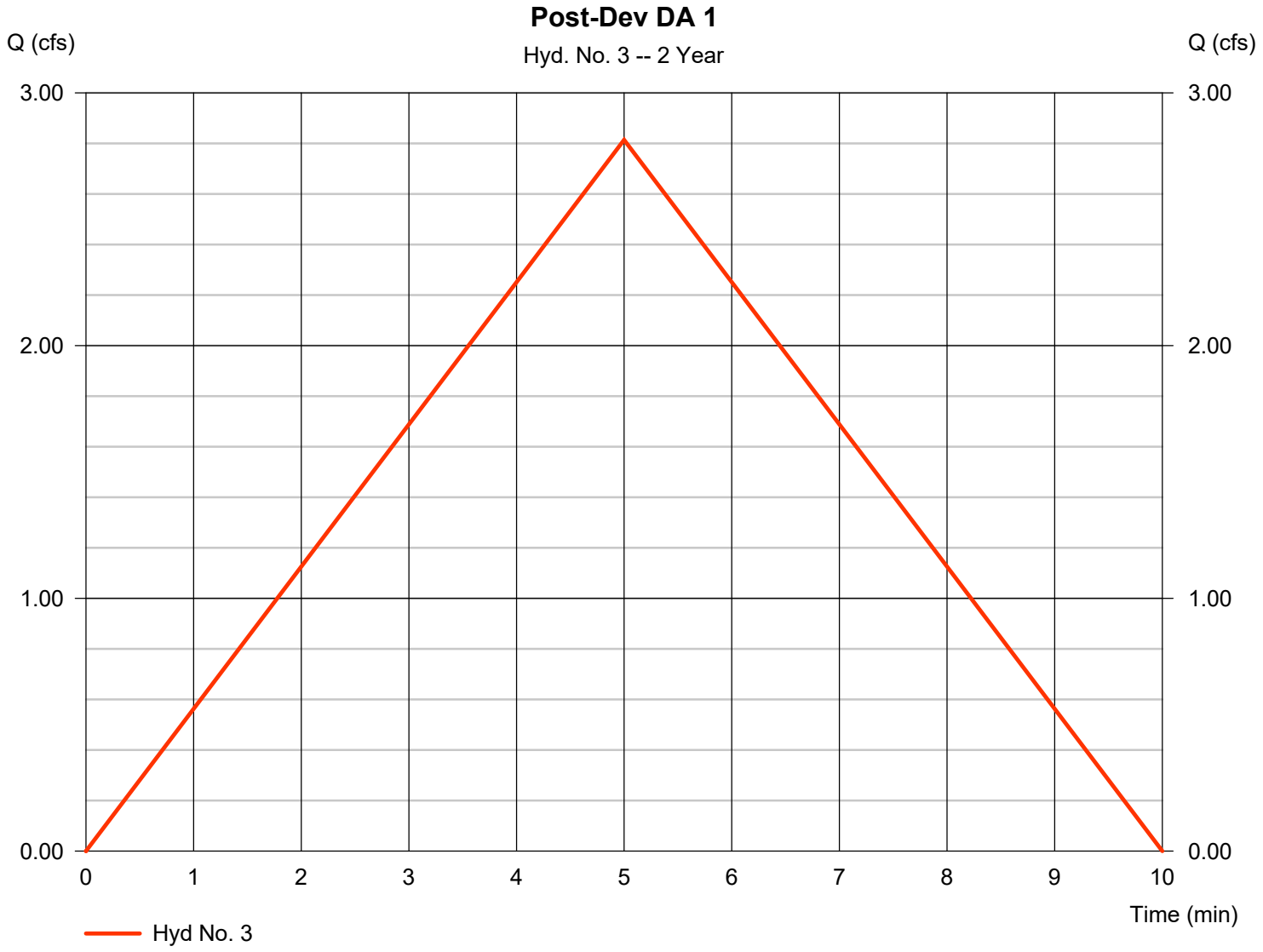


## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 2.814 cfs |
| Storm frequency | = | 2 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 844 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 5.697 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950



# Hydrograph Report

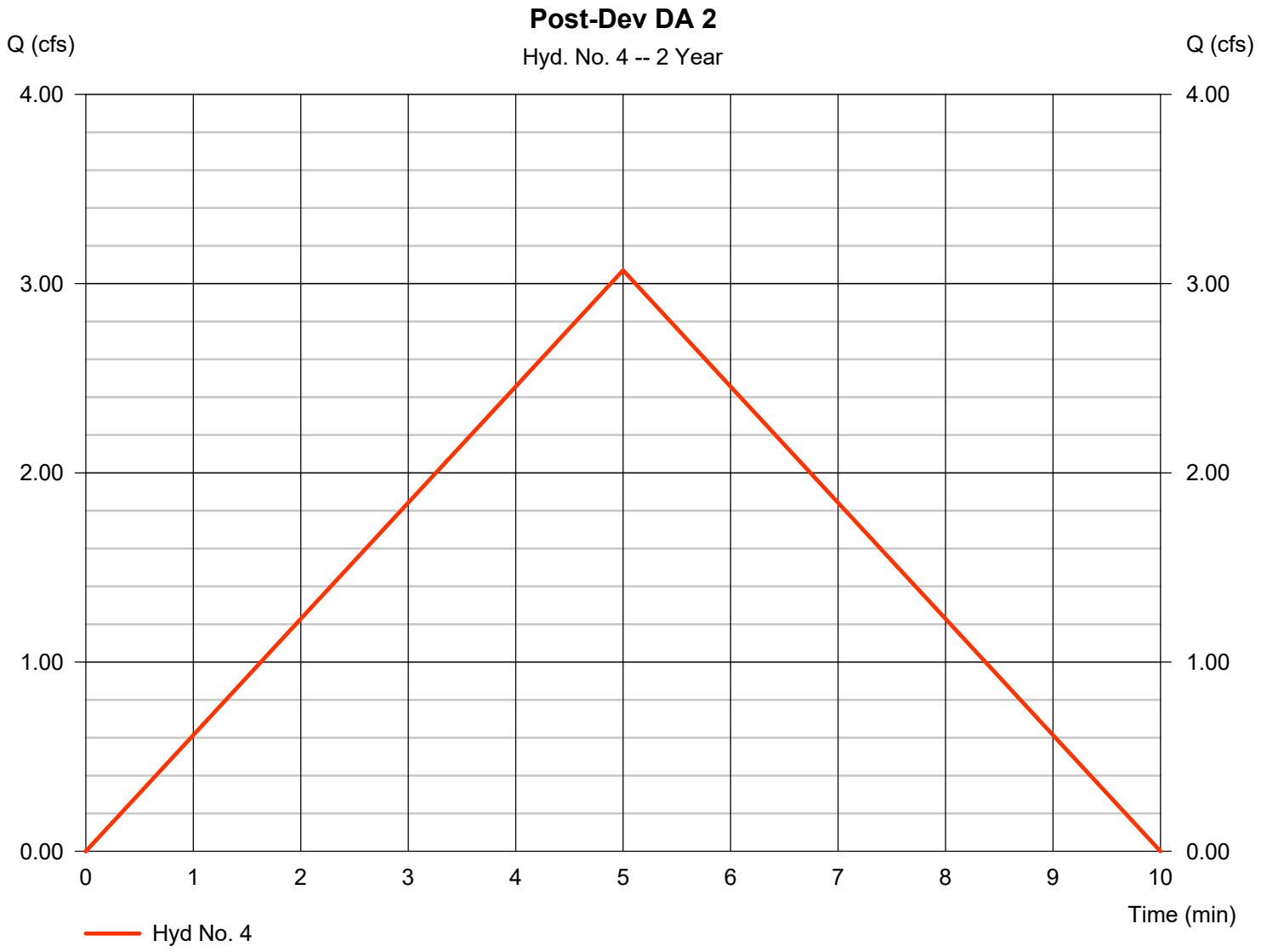


## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.070 cfs |
| Storm frequency | = | 2 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 921 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 5.697 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 2.902 | 1 | 5 | 871 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 3.580 | 1 | 5 | 1,074 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 3.281 | 1 | 5 | 984 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 3.580 | 1 | 5 | 1,074 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report

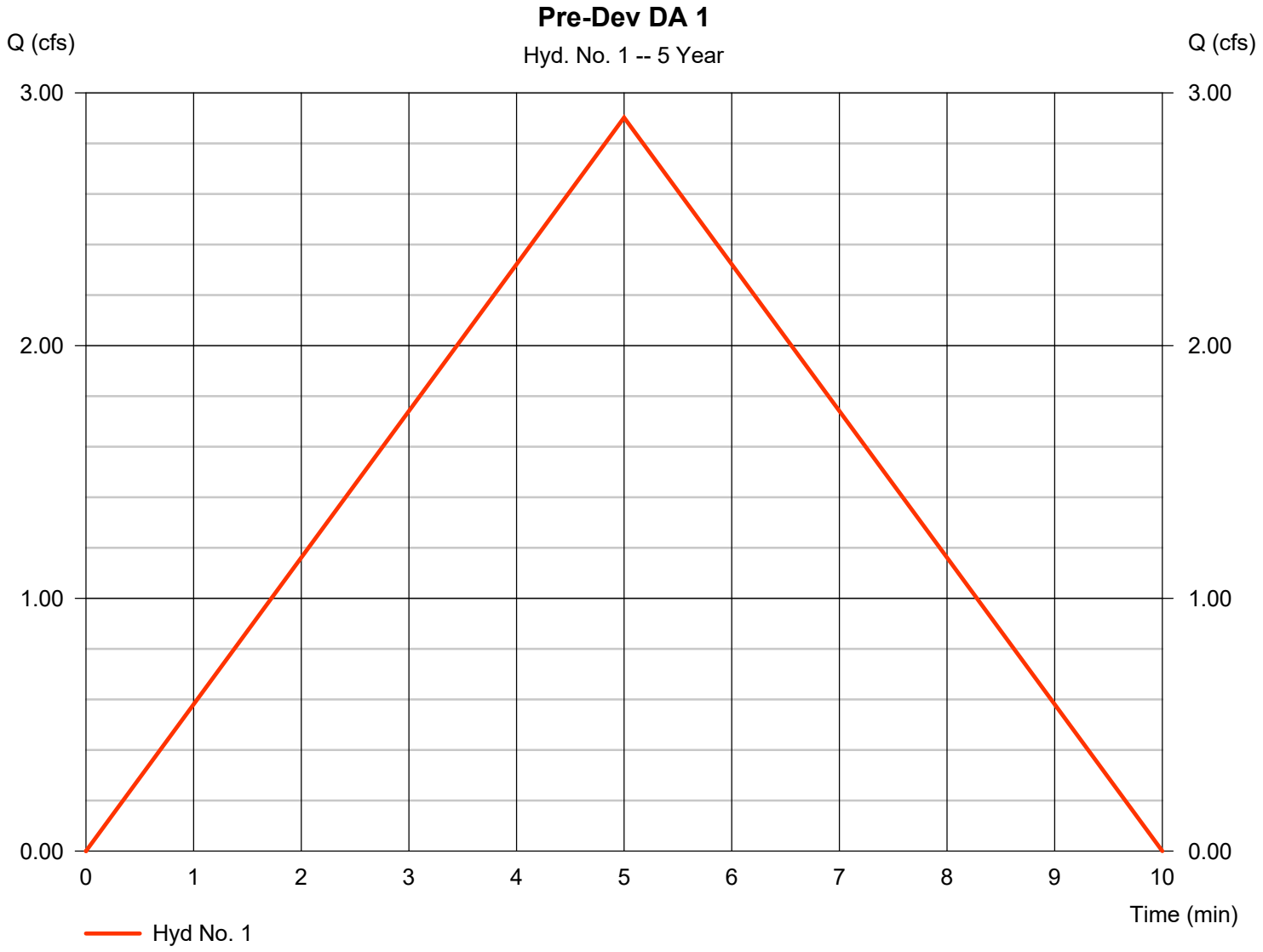


## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 2.902 cfs |
| Storm frequency | = | 5 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 871 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 6.642 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950



# Hydrograph Report



## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.580 cfs |
| Storm frequency | = | 5 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,074 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 6.642 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100

# Hydrograph Report

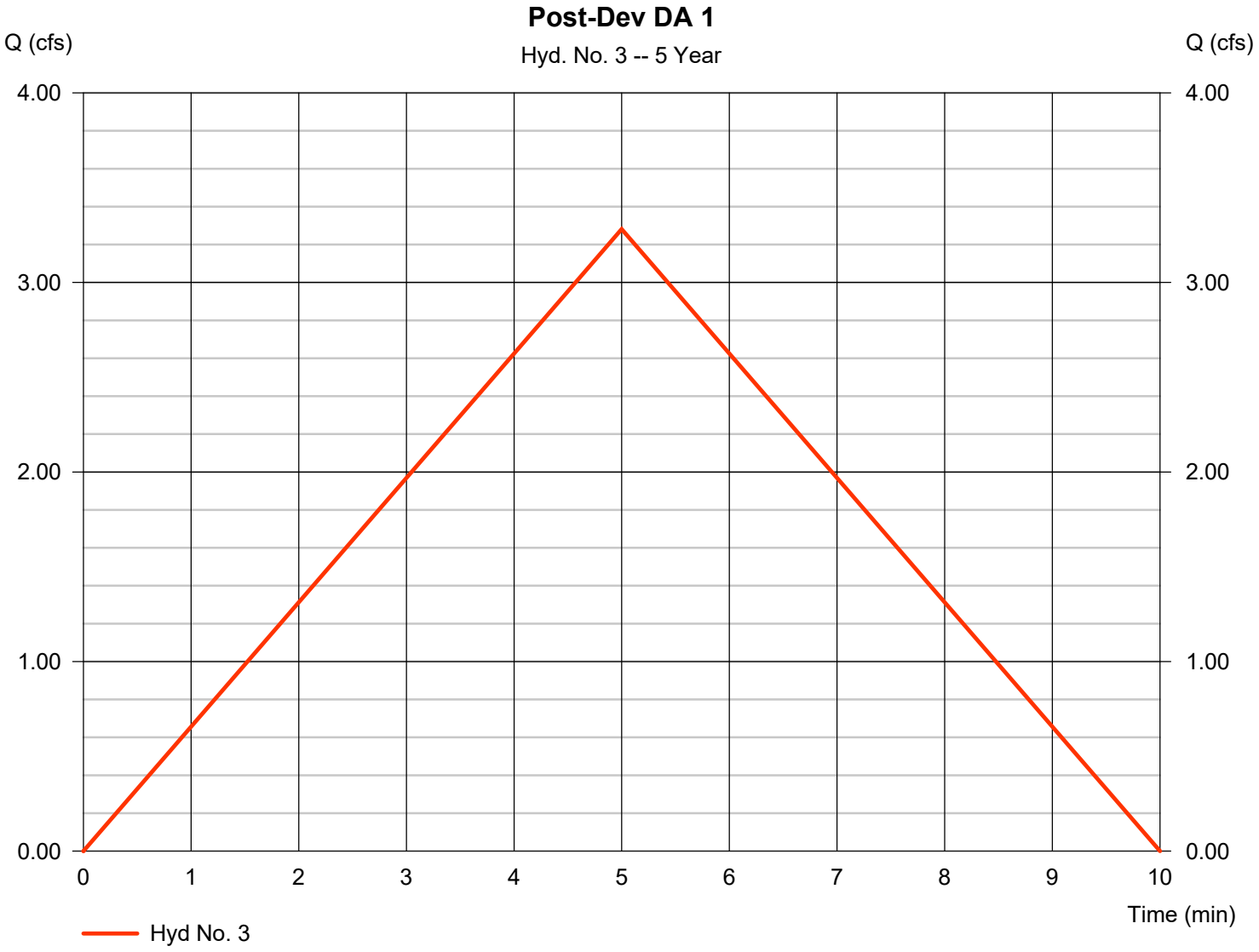


## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.281 cfs |
| Storm frequency | = | 5 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 984 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 6.642 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950



# Hydrograph Report



## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.580 cfs |
| Storm frequency | = | 5 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,074 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 6.642 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 3.212 | 1 | 5 | 964 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 3.962 | 1 | 5 | 1,189 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 3.632 | 1 | 5 | 1,089 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 3.962 | 1 | 5 | 1,189 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report



## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.212 cfs |
| Storm frequency | = | 10 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 964 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 7.351 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950

# Hydrograph Report

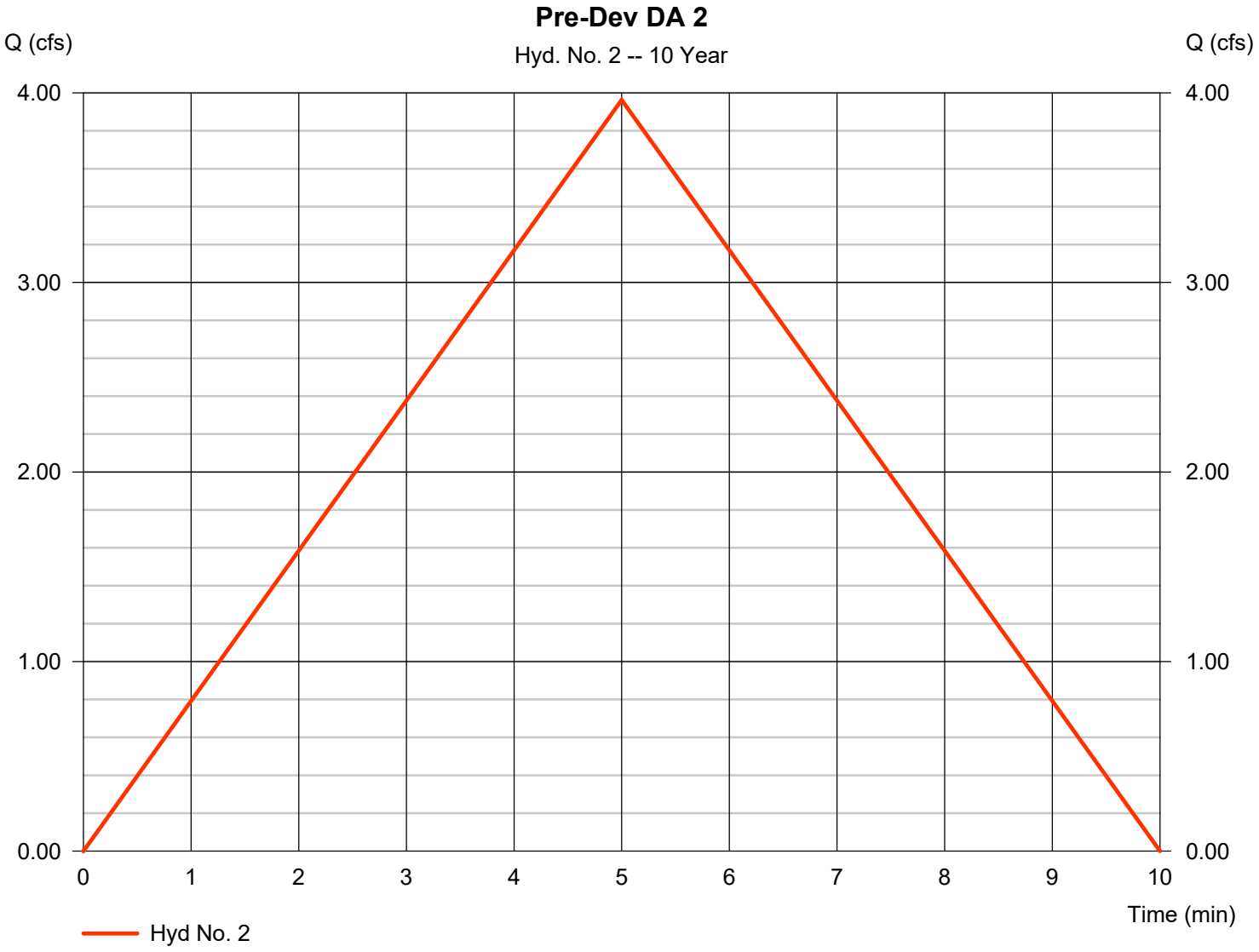


## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.962 cfs |
| Storm frequency | = | 10 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,189 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 7.351 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Report



## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.632 cfs |
| Storm frequency | = | 10 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,089 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 7.351 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950

# Hydrograph Report

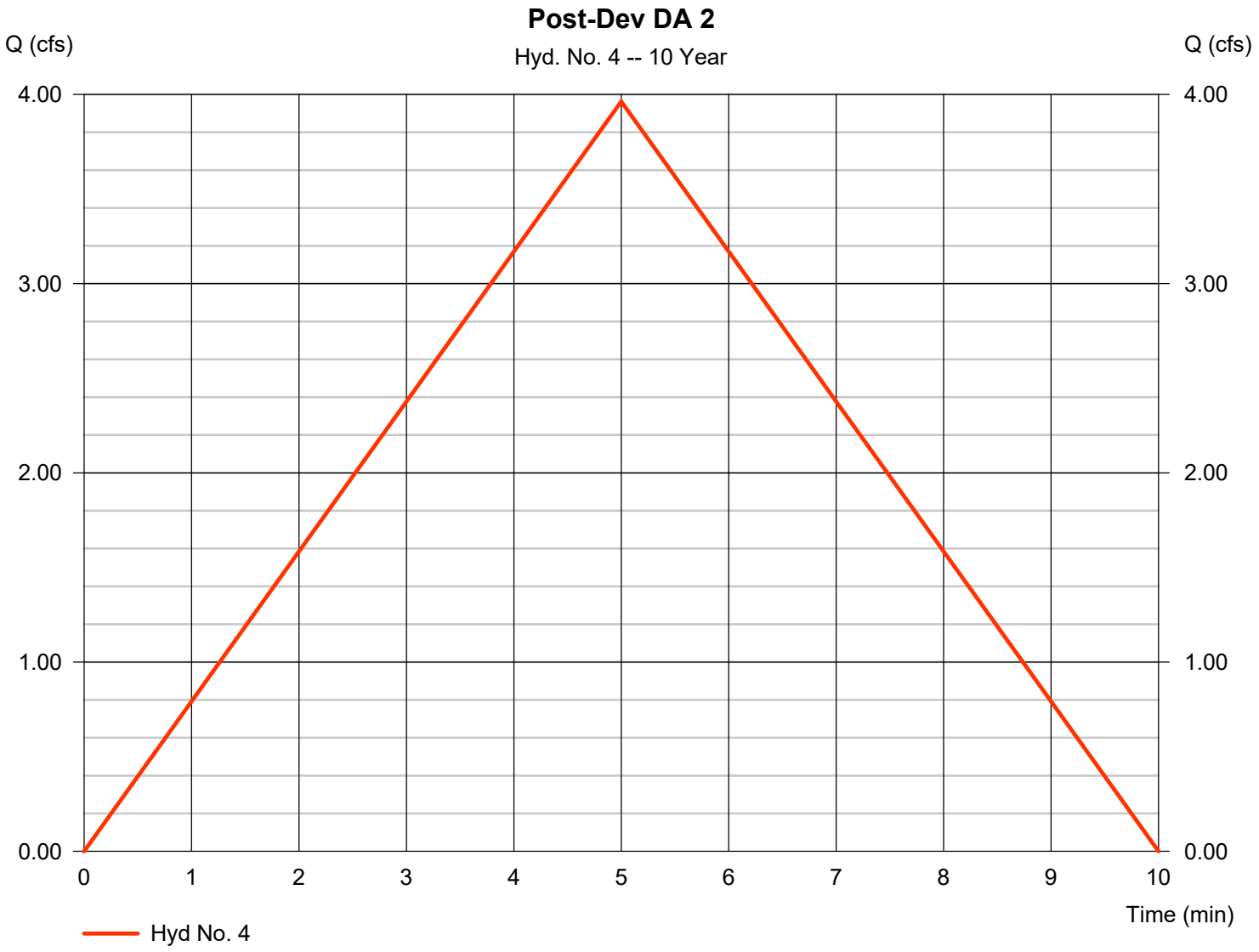


## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.962 cfs |
| Storm frequency | = | 10 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,189 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 7.351 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 3.674 | 1 | 5 | 1,102 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 4.531 | 1 | 5 | 1,359 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 4.153 | 1 | 5 | 1,246 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 4.531 | 1 | 5 | 1,359 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report

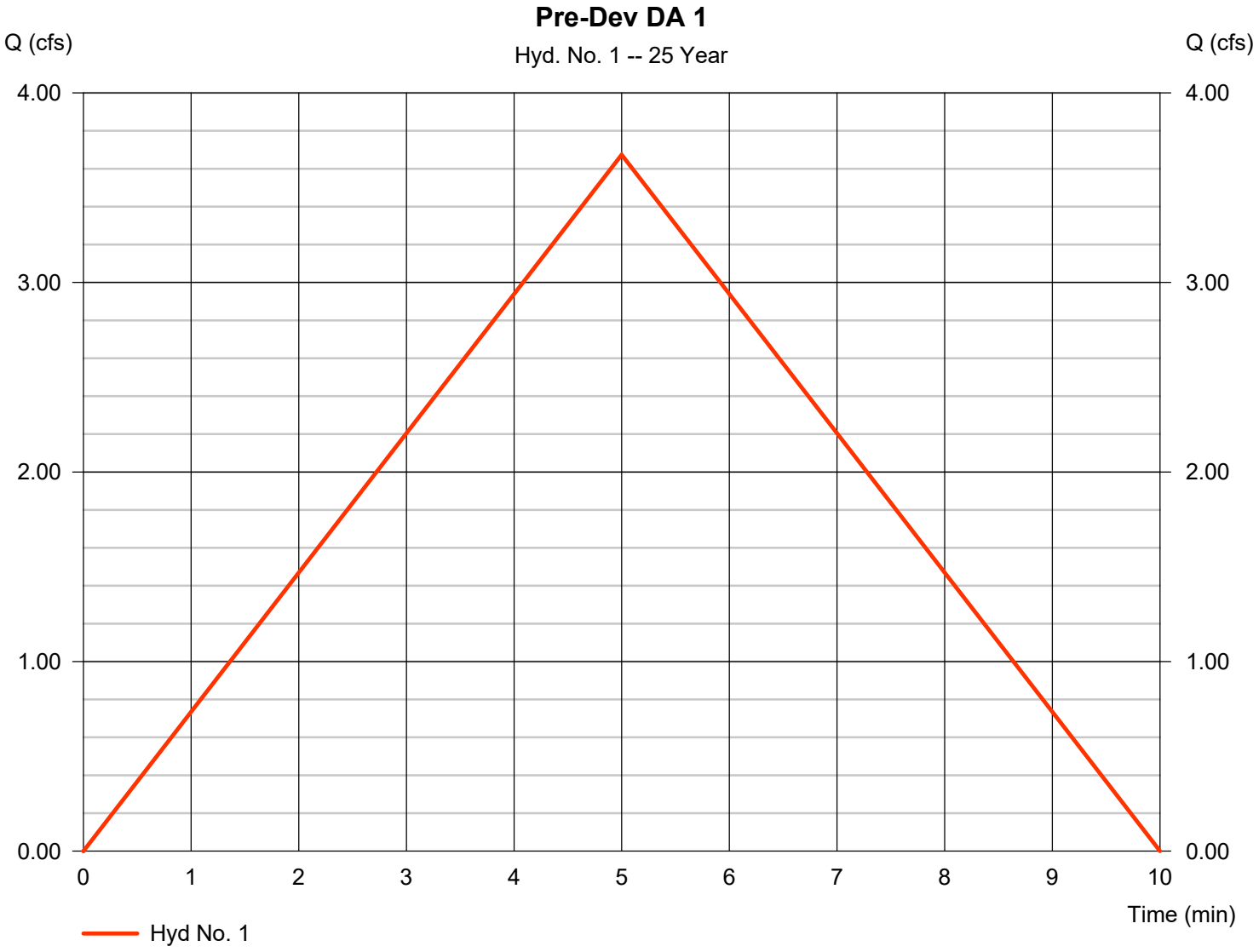


## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 3.674 cfs |
| Storm frequency | = | 25 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,102 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 8.406 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950



# Hydrograph Report

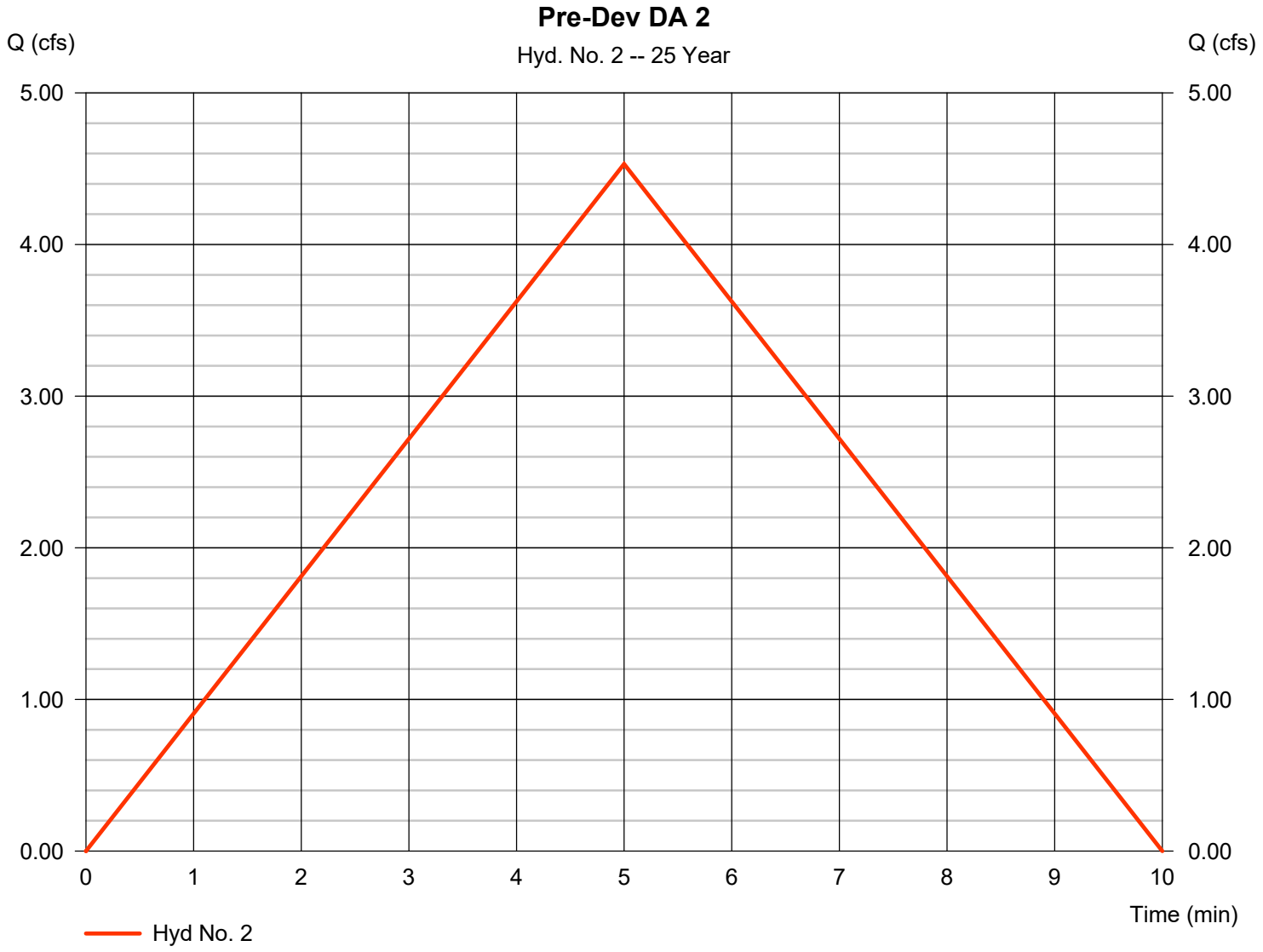


## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.531 cfs |
| Storm frequency | = | 25 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,359 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 8.406 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Report

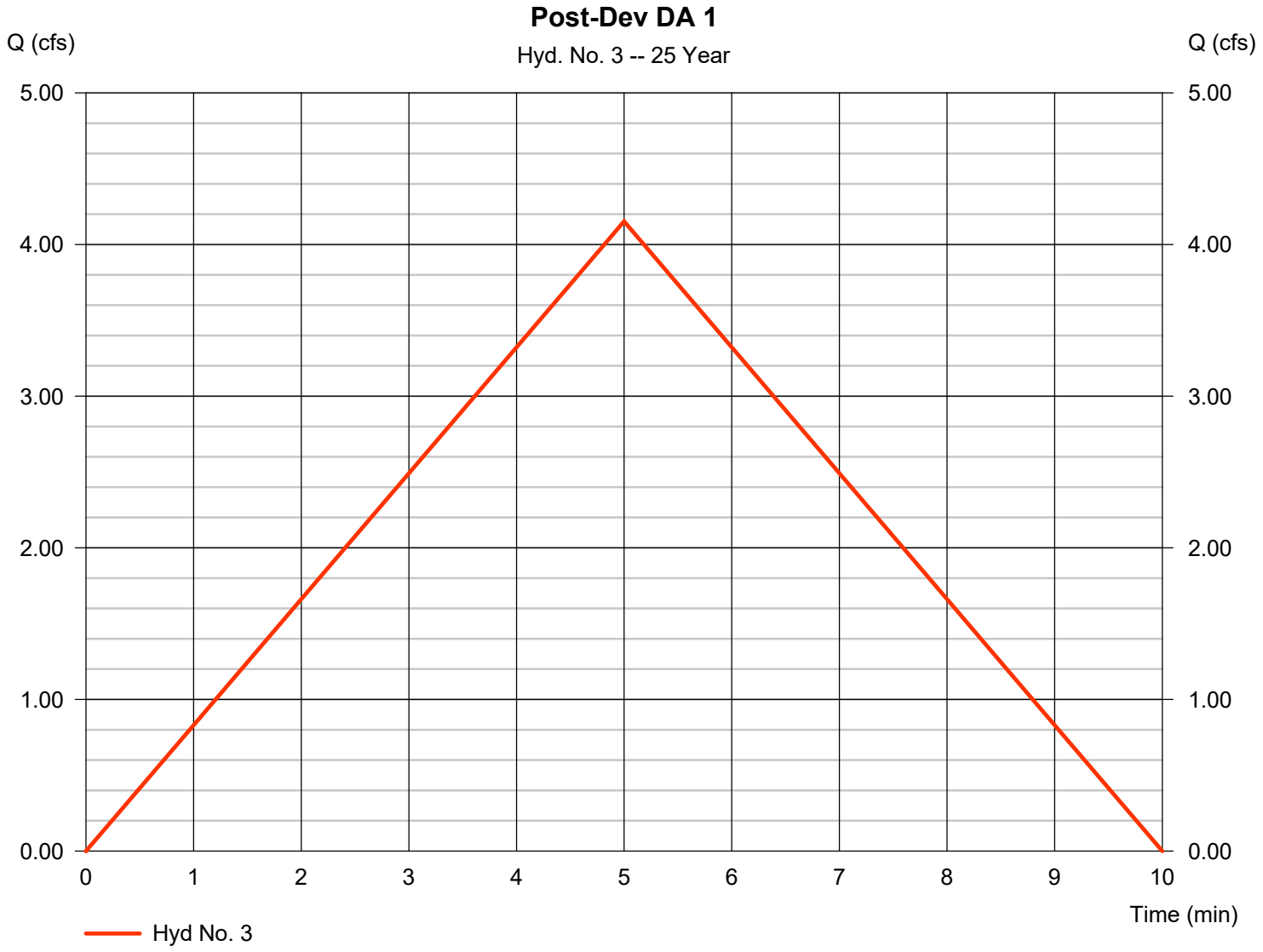


## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.153 cfs |
| Storm frequency | = | 25 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,246 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 8.406 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950



# Hydrograph Report

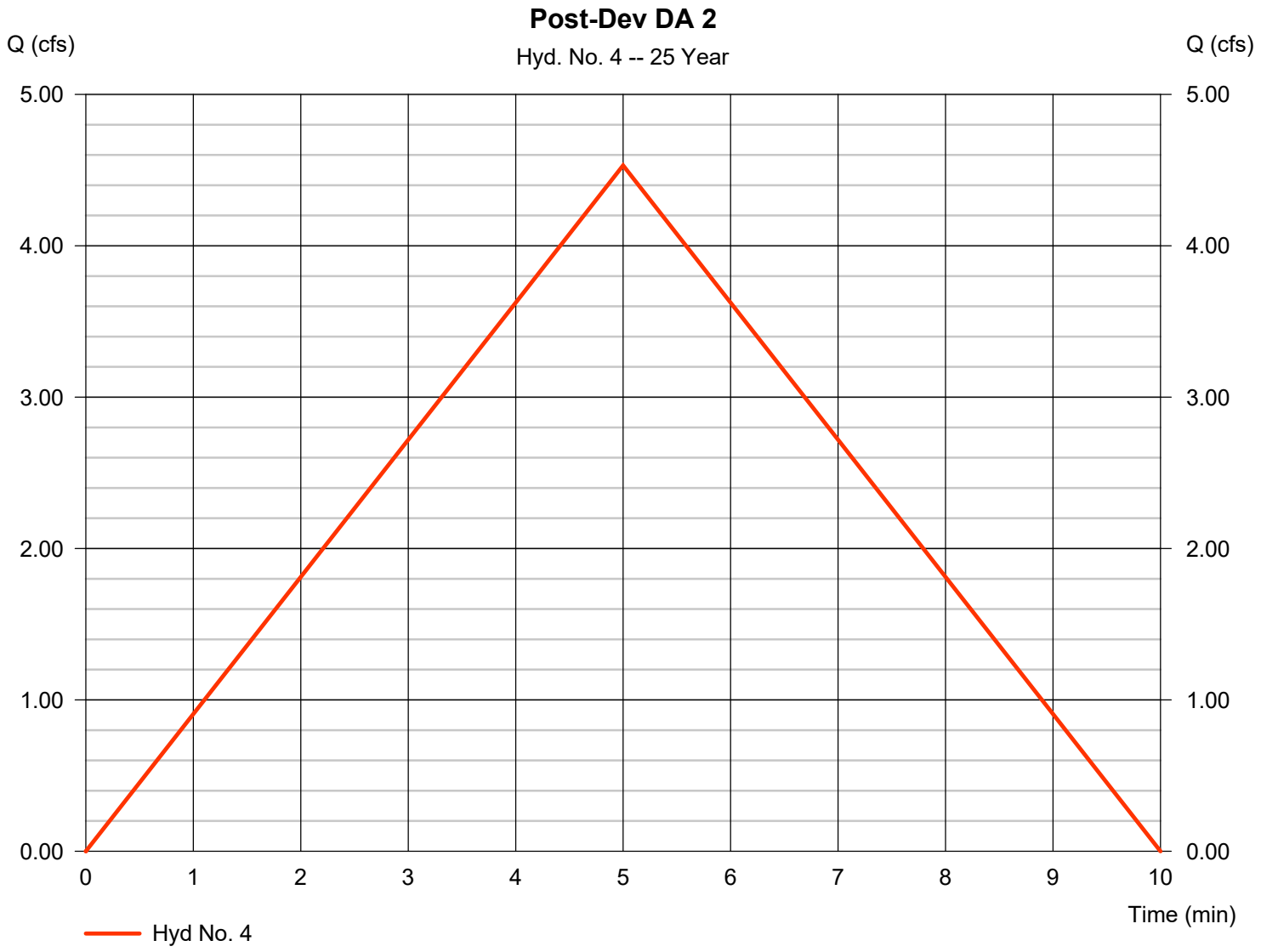


## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.531 cfs |
| Storm frequency | = | 25 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,359 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 8.406 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 4.038 | 1 | 5 | 1,211 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 4.980 | 1 | 5 | 1,494 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 4.564 | 1 | 5 | 1,369 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 4.980 | 1 | 5 | 1,494 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report



## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.038 cfs |
| Storm frequency | = | 50 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,211 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 9.240 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950

# Hydrograph Report

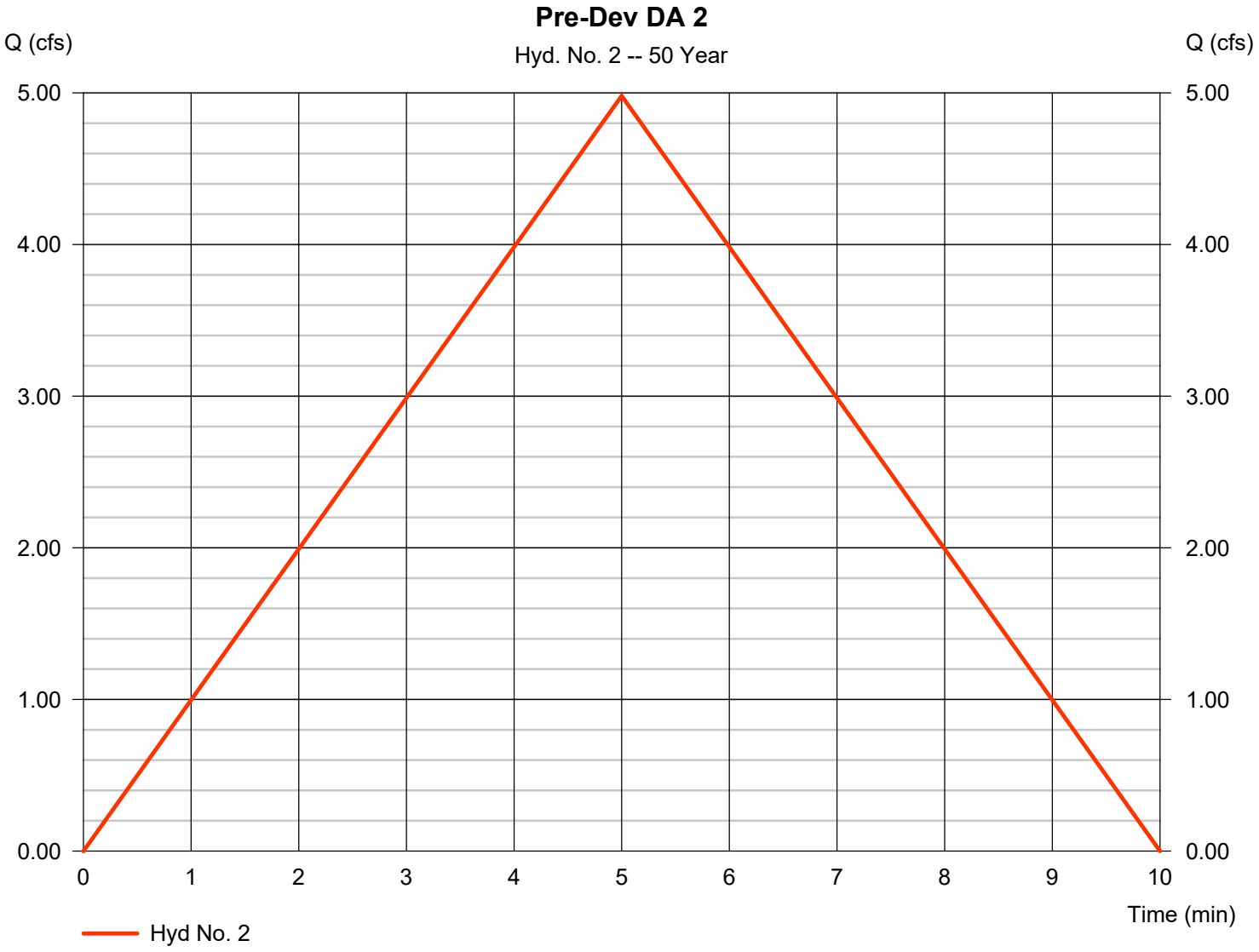


## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.980 cfs |
| Storm frequency | = | 50 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,494 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 9.240 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Report

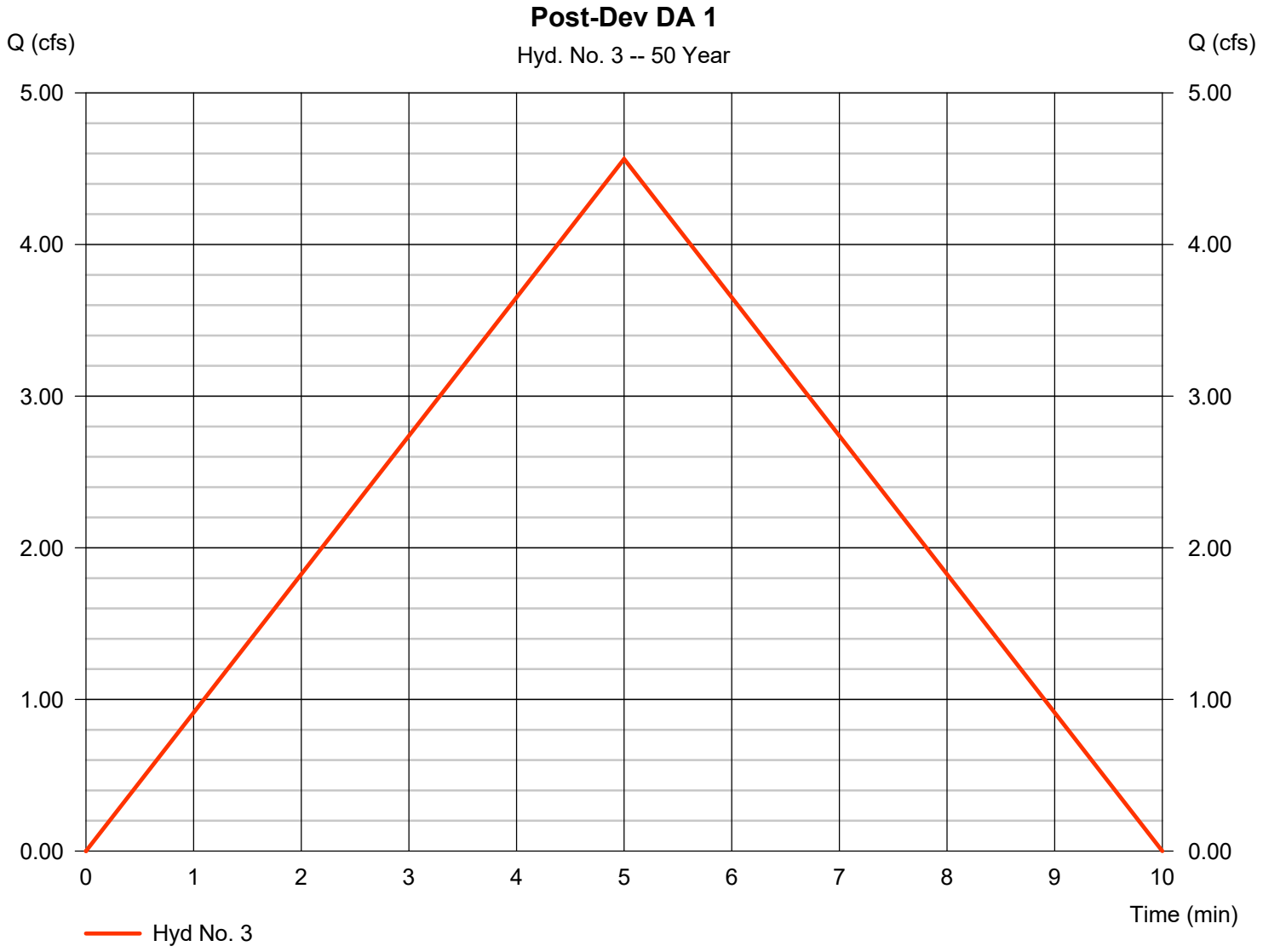


## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.564 cfs |
| Storm frequency | = | 50 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,369 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 9.240 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950



# Hydrograph Report

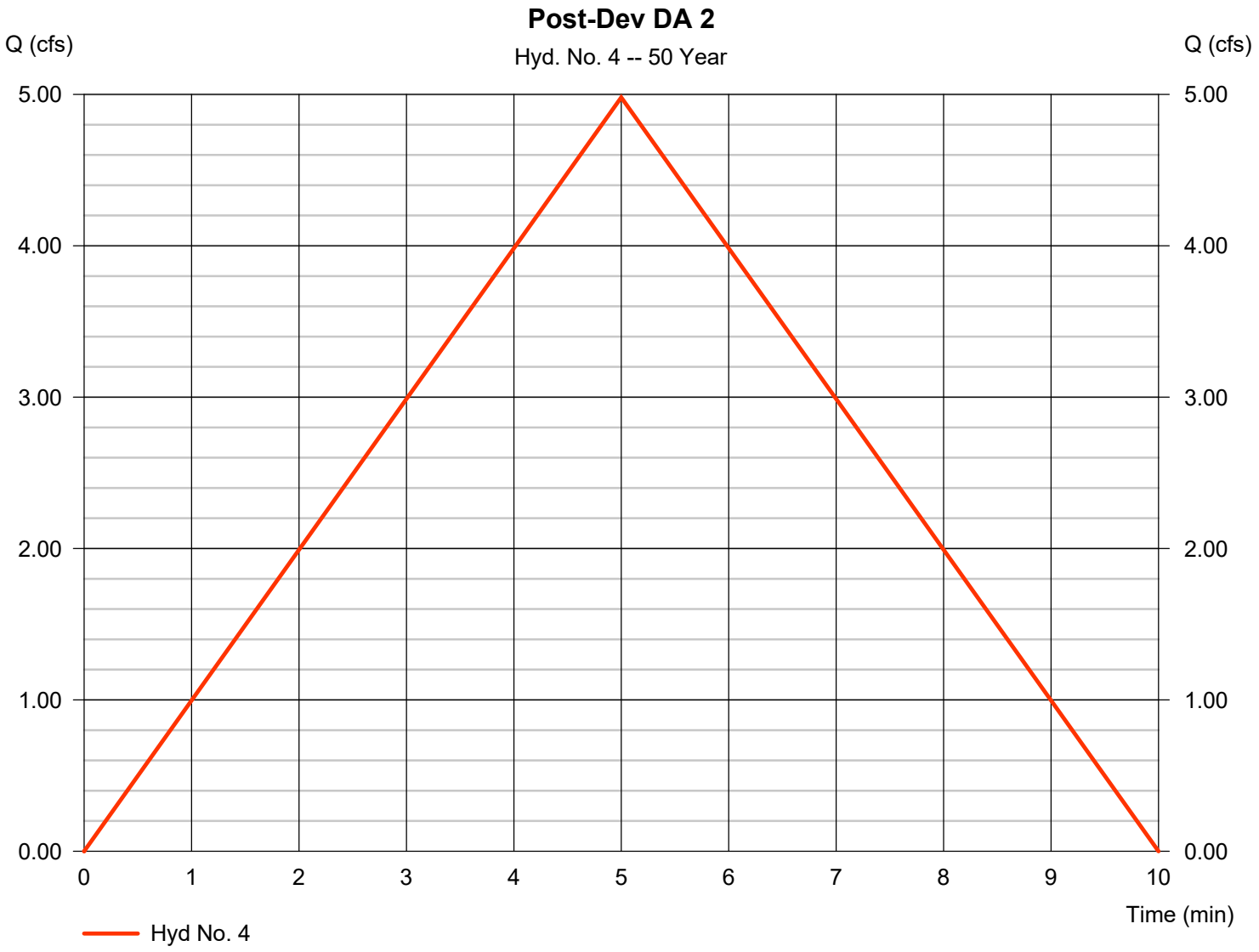


## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.980 cfs |
| Storm frequency | = | 50 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,494 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 9.240 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

| Hyd. No. | Hydrograph type (origin) | Peak flow (cfs) | Time interval (min) | Time to Peak (min) | Hyd. volume (cuft) | Inflow hyd(s) | Maximum elevation (ft) | Total strge used (cuft) | Hydrograph Description |
|---|---|---|---|---|---|---|---|---|---|
| 1 | Rational | 4.403 | 1 | 5 | 1,321 | ------ | ------ | ------ | Pre-Dev DA 1 |
| 2 | Rational | 5.431 | 1 | 5 | 1,629 | ------ | ------ | ------ | Pre-Dev DA 2 |
| 3 | Rational | 4.977 | 1 | 5 | 1,493 | ------ | ------ | ------ | Post-Dev DA 1 |
| 4 | Rational | 5.431 | 1 | 5 | 1,629 | ------ | ------ | ------ | Post-Dev DA 2 |

# Hydrograph Report

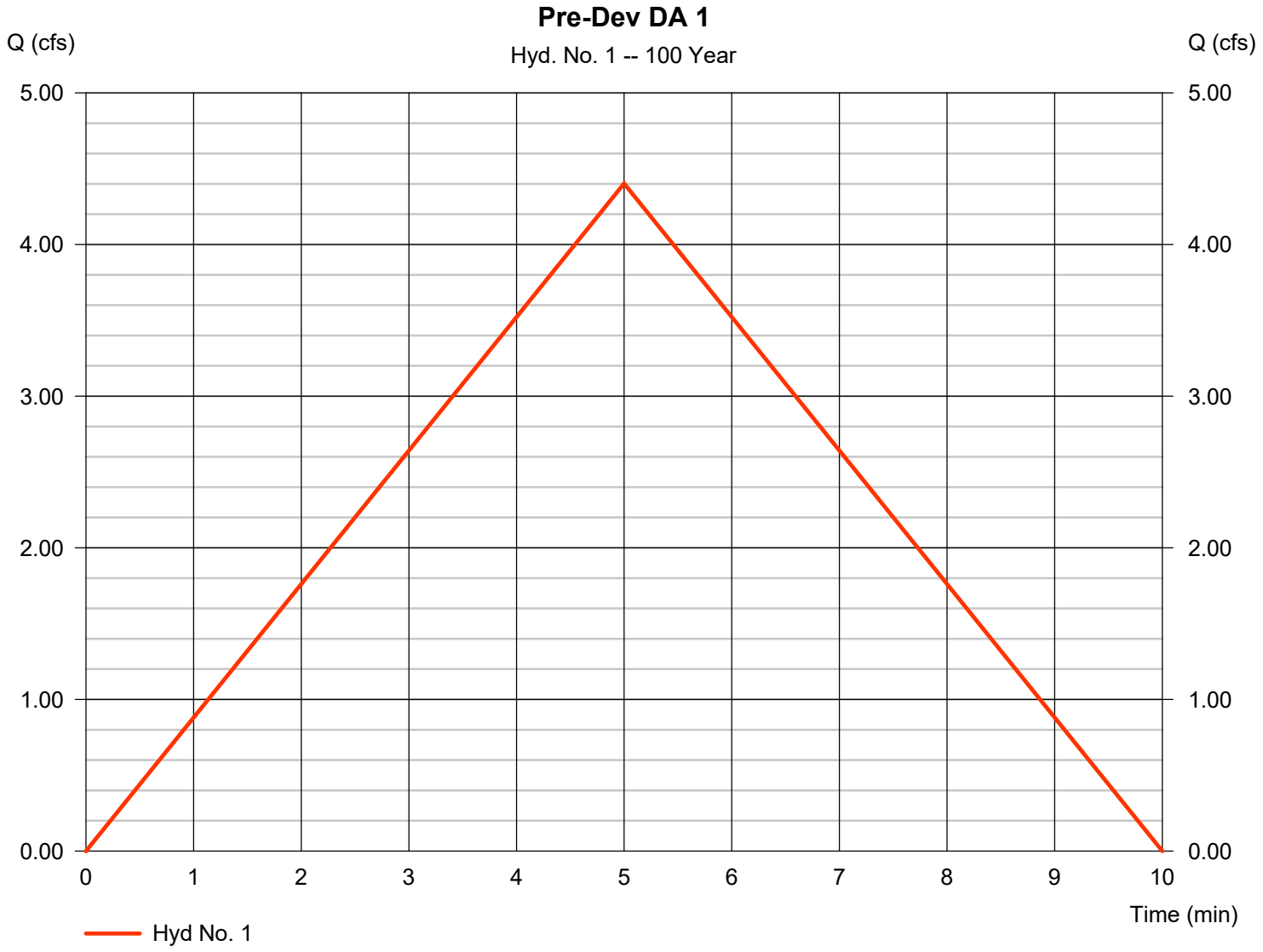


## Hyd. No. 1

Pre-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.403 cfs |
| Storm frequency | = | 100 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,321 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.46* |
| Intensity | = | 10.075 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.140 x 0.90) + (0.510 x 0.25) + (0.300 x 0.60)] / 0.950



# Hydrograph Report

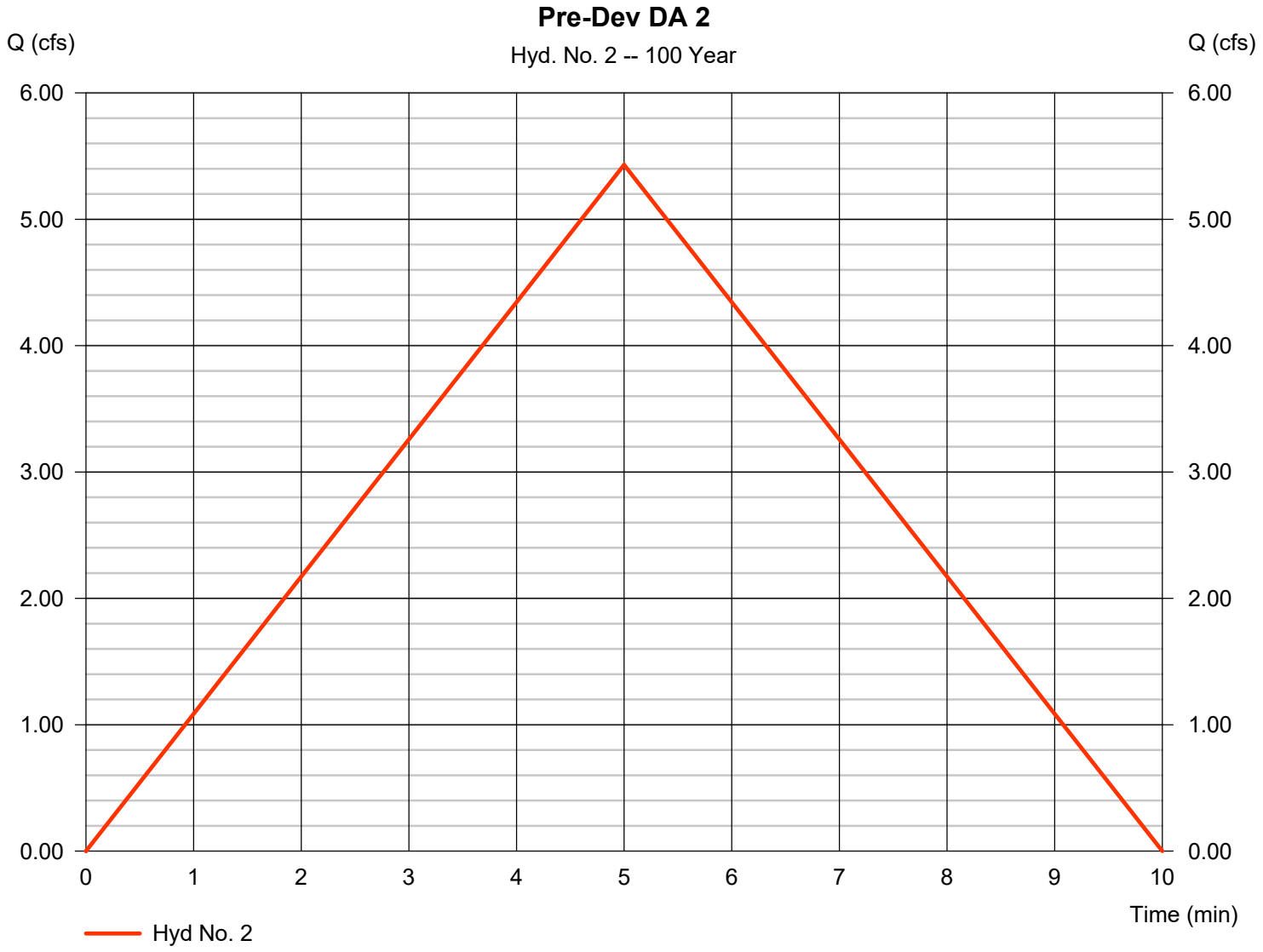


## Hyd. No. 2

Pre-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 5.431 cfs |
| Storm frequency | = | 100 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,629 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 10.075 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# Hydrograph Report



## Hyd. No. 3

Post-Dev DA 1

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 4.977 cfs |
| Storm frequency | = | 100 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,493 cuft |
| Drainage area | = | 0.950 ac | Runoff coeff. | = | 0.52* |
| Intensity | = | 10.075 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.250 x 0.90) + (0.430 x 0.25) + (0.270 x 0.60)] / 0.950

# Hydrograph Report

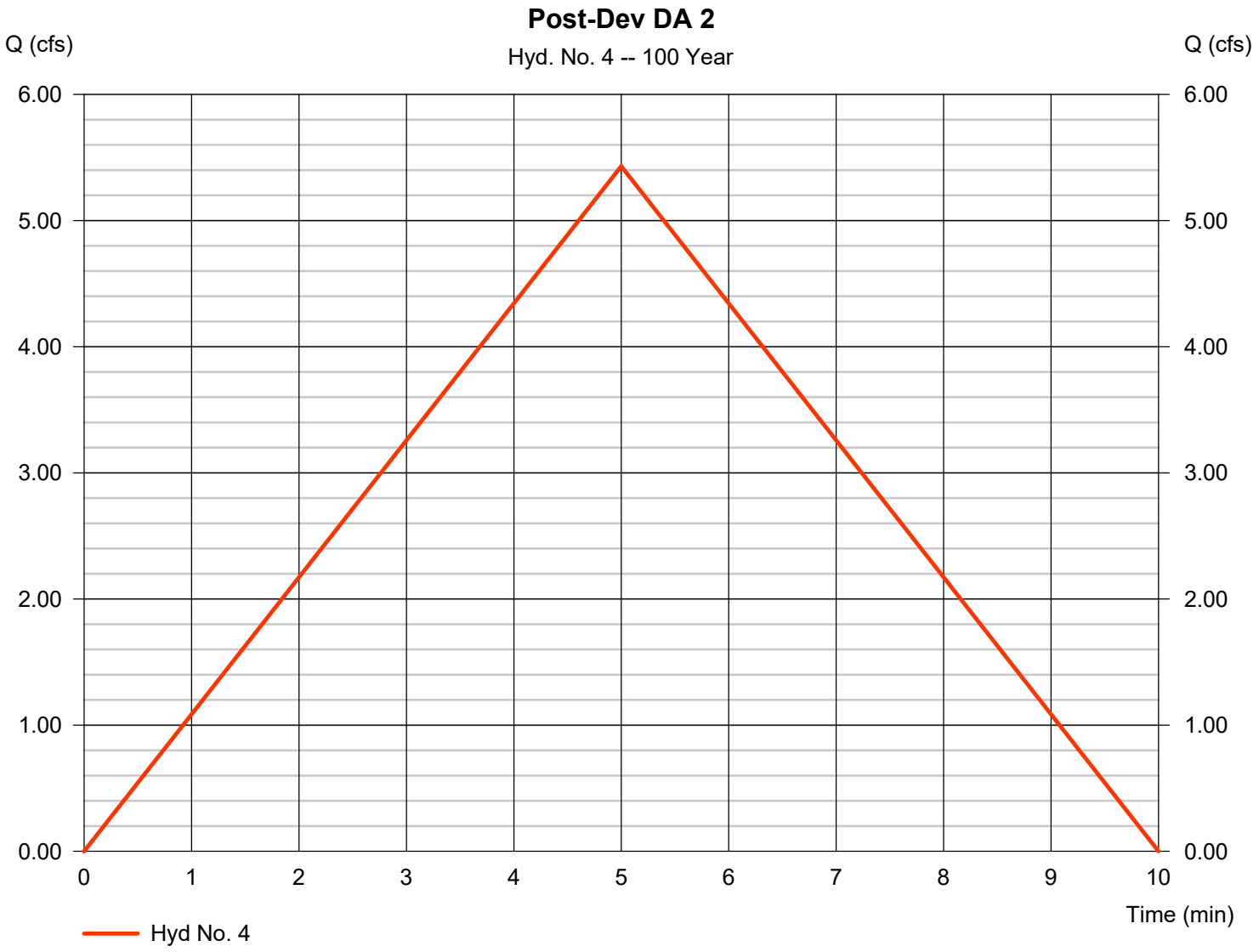


## Hyd. No. 4

Post-Dev DA 2

| | | | | | |
|---|---|---|---|---|---|
| Hydrograph type | = | Rational | Peak discharge | = | 5.431 cfs |
| Storm frequency | = | 100 yrs | Time to peak | = | 5 min |
| Time interval | = | 1 min | Hyd. volume | = | 1,629 cuft |
| Drainage area | = | 1.100 ac | Runoff coeff. | = | 0.49* |
| Intensity | = | 10.075 in/hr | Tc by User | = | 5.00 min |
| IDF Curve | = | Pulaski County.IDF | Asc/Rec limb fact | = | 1/1 |

* Composite (Area/C) = [(0.400 x 0.90) + (0.700 x 0.25)] / 1.100



# BRYANT ALE CLASSROOM ADDITION

BRYANT PUBLIC SCHOOLS

BRYANT, ARKANSAS

## PROJECT INFORMATION

DRAWINGS AND PROJECT MANUAL APPROVED AND IDENTIFIED AS PARTS OF THE OFFICIAL CONTRACT DOCUMENT

OWNER: BRYANT PUBLIC SCHOOLS
FACILITY: BRYANT ALE CLASSROOM ADDITION
LOCATION: BRYANT, ARKANSAS

BY:
DATE:

CONTRACTOR: --
ADDRESS: --
--

BY:
DATE:

ARCHITECT: LEWIS, ELLIOTT, McMORRAN, VADEN, RAGSDALE, & WOODWARD INCORPORATED
ADDRESS: 11225 HURON LANE, SUITE 104 LITTLE ROCK, ARKANSAS 72211

BY:
DATE:

PROJECT NUMBER: 25034
DRAWINGS AND PROJECT MANUAL DATED: 2025 06-09

## DESIGN DATA

**GENERAL CODES:**

| | |
|---|---|
| INTERNATIONAL BUILDING CODE (IBC) | 2021 EDITION |
| ARKANSAS FIRE PREVENTION CODE (AFPC) | 2021 EDITION |

**SEISMIC:**

| | |
|---|---|
| CLASSROOMS: | 2021 IBC |
| SEISMIC RISK CATEGORY II | |
| SEISMIC DESIGN CATEGORY D | |
| SHELTER: | |
| SEISMIC RISK CATEGORY IV | |
| SEISMIC DESIGN CATEGORY D | |
| SALINE COUNTY | AFPC REVISIONS |

**ACCESSIBILITY STANDARDS**

| | |
|---|---|
| ADA STANDARDS FOR ACCESSIBLE DESIGN | 2010 EDITION |

**OCCUPANCY CLASSIFICATION:**

| | |
|---|---|
| EDUCATIONAL | IBC 305 |

**CONSTRUCTION TYPE:**

| | |
|---|---|
| TYPE VB - COMBUSTIBLE | IBC 602.5 |

**ALLOWABLE BUILDING SQUARE FOOTAGE/HEIGHT:**

| | |
|---|---|
| ONE STORY (S1), NOT SPRINKLED (NS) = 9,500 SQFT / 1 STORY 40 FT | IBC 506.2 |

**OCCUPANT LOAD:**

| | |
|---|---|
| EGRESS DESIGN = 20 SQFT/OCC (NET) = 168 OCCUPANTS | IBC 1004 |
| ACTUAL = 2 ELEMENTARY ALE CLASSROOMS ( 23 STUDENTS, 1 TEACHER) = 43 OCCUPANTS | |

**EGRESS:**

| | |
|---|---|
| EGRESS WIDTH REQUIRED: 168 OCCUPANTS x 0.2" = 33.6 | IBC 1005.3.2 |
| EGRESS WIDTH PROVIDED = 2-3' DOORS (32" CLEAR) = 64" (320 OCC) | |
| MINIMUM NUMBER OF EXITS = 2 EXITS (>50 OCC) | IBC 1006.2 |
| MINIMUM CORRIDOR WIDTH = 72" ( E w/ >100 OCC) | IBC 1020.3 |

**TOTAL BUILDING SQUARE FOOTAGE:**

| | |
|---|---|
| MAIN LEVEL | 3,485 SQ. FT. |

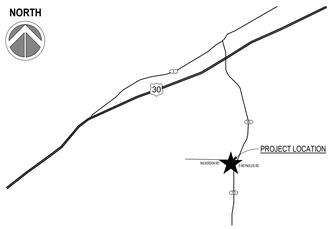
**FIRE PROTECTION**

| | |
|---|---|
| PORTABLE FIRE EXTINGUISHERS | NFPA 10 |
| 1-HR AND 2- HR RATED CONSTRUCTION | IBC TABLE 601 |
| FIRE EXIT (PANIC) HARDWARE AT BUILDING EXITS | 1010.2.9 |

**SEE LIFE SAFETY PLAN FOR LIFE SAFETY INFORMATION**

## VICINITY MAP

NORTH




**CERTIFICATION STATEMENT:**

I HEREBY CERTIFY THAT THESE PLANS AND SPECIFICATIONS HAVE BEEN PREPARED BY ME, OR UNDER MY SUPERVISION. I FURTHER CERTIFY THAT TO THE BEST OF MY KNOWLEDGE THESE PLANS AND SPECIFICATIONS ARE AS REQUIRED BY LAW AND IN COMPLIANCE WITH THE "ARKANSAS FIRE PREVENTION CODE" FOR THE STATE OF ARKANSAS.

LEWIS, ELLIOTT, MCMORRAN, VADEN, RAGSDALE, & WOODWARD, INCORPORATED

## INDEX OF DRAWINGS


T1.1 TITLE SHEET

### CIVIL

### ARCHITECTURAL

A1.0 LIFE SAFETY PLAN
A2.1 DEMO, SITE, & FLOOR PLAN
A3.1 BUILDING ELEVATIONS
A4.1 BUILDING SECTIONS
A5.1 WALL SECTIONS
A5.2 WALL SECTIONS
A6.1 RCP & ROOF PLAN
A8.1 DOORS, WINDOWS, & INTERIOR FINISH SCHEDULE

### STRUCTURAL

S2.1 STRUCTURAL PLANS
S3.1 FOUNDATION DETAILS
S3.2 FOUNDATION DETAILS
S3.3 FRAMING DETAILS

### PLUMBING

P1.1 FLOOR PLAN - PLUMBING
P2.1 PLUMBING SCHEDULES & DETAILS

### MECHANICAL

M1.1 FLOOR PLAN - HVAC
M2.1 HVAC LEGENDS & SCHEDULES
M3.1 HVAC DETAILS

### ELECTRICAL

E1.1 FLOOR PLAN - ELECTRICAL
E2.1 ELECTRICAL RISERS & DETAILS
E3.1 ELECTRICAL LEGENDS, DETAILS, & NOTES


## MATERIAL LEGEND

- CMU (PLAN)
- MASONRY (PLAN)
- METAL STUD FRAMING (PLAN)
- GYPSUM PANELS
- WOOD BLOCKING CONTINUOUS (SECTION)
- WOOD BLOCKING AS NEEDED (SECTION)
- WOOD FINISHED FACE OR SOLID WOOD
- WOOD PLYWOOD (SECTION)
- CONCRETE (SECTION)
- RIGID INSULATION (SECTION)
- BATT INSULATION (SECTION)
- FILL MATERIAL (SECTION)
- REPLACED SOIL (SECTION)

## SYMBOL LEGEND

- 100.1 — DOOR MARK, SEE DOOR SCHEDULE
- A — CASEWORK ELEVATION MARK
- B — WINDOW / STOREFRONT FRAME MARK
- CLASSROOM — ROOM NAME
- 101 — ROOM NUMBER
- LAY-1 | 9'-4" — ROOM CEILING HEIGHT / CEILING FINISH
- 3 / A4.4 — DETAIL / SECTION NUMBER / SHEET NUMBER

## ABBREVIATIONS

| | |
|---|---|
| AFF | ABOVE FINISH FLOOR |
| AT | ALUMINUM THRESHOLD |
| CEJC | CEILING EXPANSION JOINT COVER |
| CJ | CONTROL JOINT |
| CLG | CEILING |
| CONC | CONCRETE |
| CONT | CONTINUOUS |
| DTL | DETAIL |
| FD | FLOOR DRAIN |
| FEC | FIRE EXTINGUISHER CABINET |
| FEJ | FLOOR EXPANSION JOINT |
| FLR | FLOOR |
| GB | GRAB BAR |
| MECH | MECHANICAL |
| NHO | NORMALLY HELD OPEN |
| NTS | NOT TO SCALE |
| OPG | OPENING |
| REQ | REQUIRED |
| SHT | SHEET |
| SIM | SIMILAR |
| STO | STORAGE |
| TYP | TYPICAL |
| WEJC | WALL EXPANSION JOINT COVER |

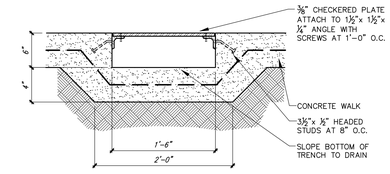

LEWIS ARCHITECTS ENGINEERS
ELLIOTT • MCMORRAN • VADEN
RAGSDALE • WOODWARD • INCORPORATED
501 223 9302 • WWW.LEMVRW.COM


TITLE SHEET

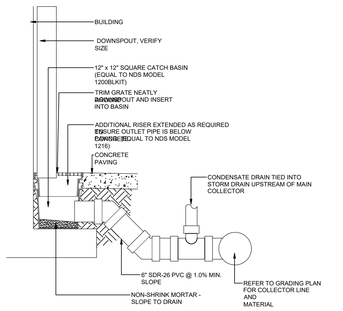
BRYANT ALE CLASSROOM ADDITION
BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

DATE: 2025 06-09
PROJECT NO: 25034
DRAWN BY: BGA
REV:

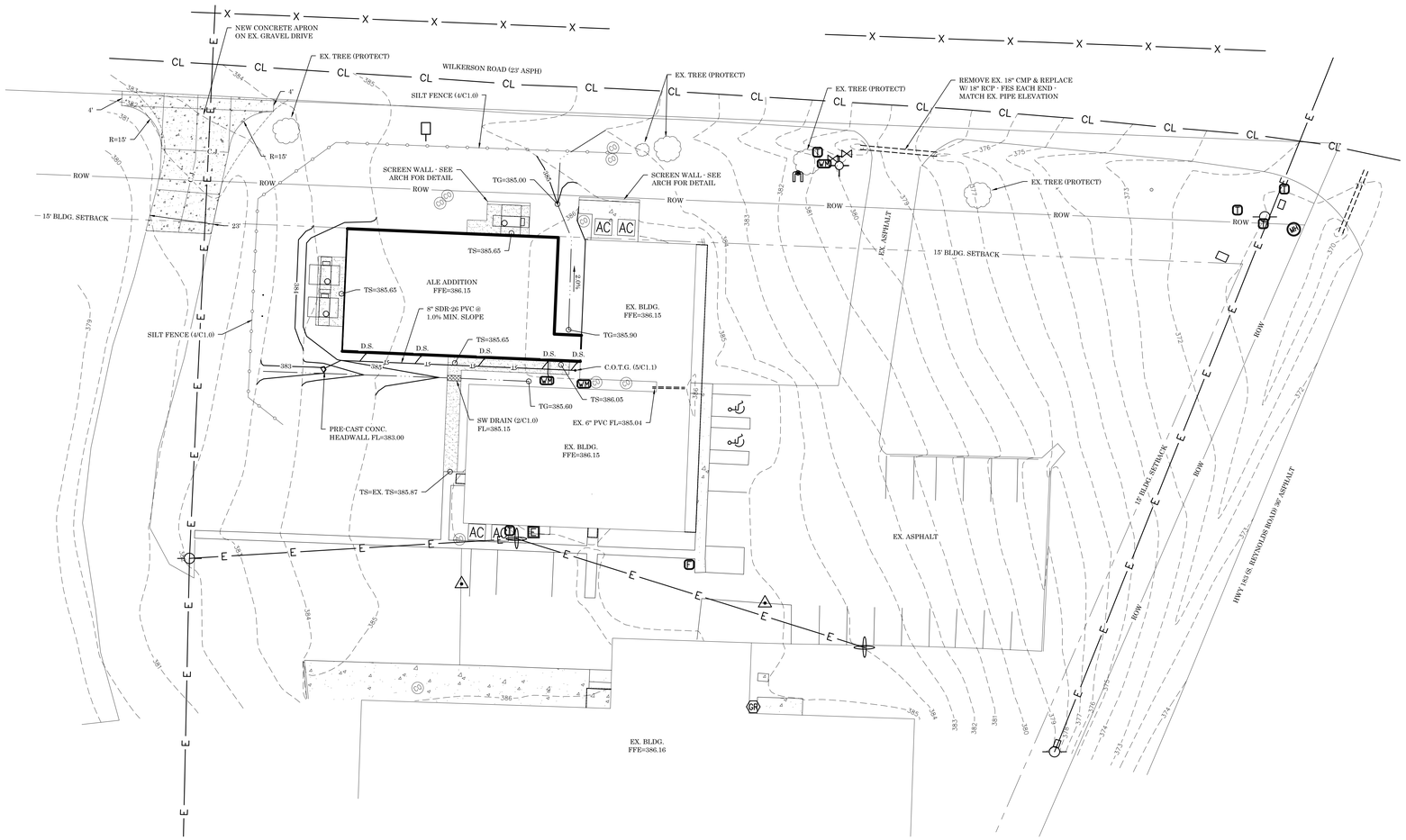
T1.1




2 C1.0 CONCRETE WALK TRENCH DRAIN DETAIL
NOT TO SCALE

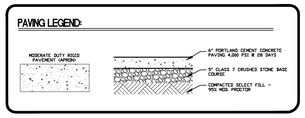



3 C1.0 DOWNSPOUT (D.S.) CONNECTION DETAIL
NOT TO SCALE




NORTH 1 C1.0 SITE GRADING & STORM DRAINAGE PLAN
SCALE: 1" = 20'
0 20 40

**PAVING LEGEND:**

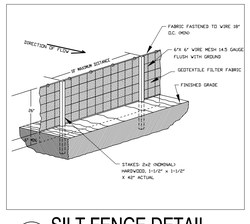



## GENERAL SITE GRADING NOTES:

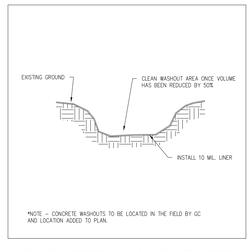
1. ALL BIDDERS SHALL FIELD VERIFY EXIST SITE CONDITIONS SO AS TO BE FAMILIAR WITH PROJECT PRIOR TO BIDDING WORK INCLUDED IN THIS CONTRACT. ANY DISCREPANCIES SHALL BE ADDRESSED PRIOR TO BIDDING.
2. CONTRACTOR TO VERIFY AND MARK ALL EXISTING UTILITIES PRIOR BEFORE ANY DEMOLITION OR NEW CONSTRUCTION WORK COMMENCES.
3. ALL WORK SHALL CONFORM TO LOCAL & STATE CODES; ELECTRICAL & PLUMBING LINES SHALL BE INSTALLED BY PROFESSIONALS LICENSED BY THE STATE OF ARKANSAS.
4. FIELD VERIFY EXACT LOCATION OF ALL EXISTING TREES; EXIST TREES NOT IN CONSTRUCTION AREA TO BE PROTECTED WITH 2x WOOD PLANKS CONT. IN LINE WITH DRIP EDGE OF TREE, SECURED TOGETHER & FLAGGED W/ORANGE TAPE; HEAVY EQUIPMENT TO WORK AS FAR AS POSSIBLE FROM EXIST TREES TO PREVENT DAMAGE TO FEEDER ROOTS; CONTRACTOR WILL BE REQUIRED TO COMPENSATE OWNER FOR ANY EXISTING TREES WHICH ARE DAMAGED OR DIE DUE TO CONSTRUCTION WORK.
5. THE GENERAL CONTRACTOR SHALL HAVE THE GEOTECHNICAL ENGINEER EMPLOYED TO OBSERVE SITE WORK MEET WITH THE GEOTECHNICAL ENGINEER THAT PROVIDED THE SOIL'S REPORT. THIS MEETING SHOULD OCCUR AT OR BEFORE THE PRE-CONSTRUCTION MEETING TO INSURE THE AMOUNT OF UNDERCUT THAT MAY BE REQUIRED FOR THE PROJECT. RECOMMENDATIONS BY GEO-TECHNICAL ENGINEER SHALL NOT BE IMPLEMENTED INTO WORK WITHOUT AUTHORIZATION FROM OWNER & ARCHITECT. NOTIFY ARCHITECT IMMEDIATELY IF UNEXPECTED SUBSURFACE CONDITIONS ARE ENCOUNTERED. THE CONTRACTOR WILL REFERENCE THE GEOTECHNICAL REPORT FOR A MORE DETAILED DESCRIPTION OF EARTHWORK AND COMPACTION REQUIREMENTS.
6. SEQUENCE OF DIRTWORK ACTIVITIES (REFERENCE GEOTECH REPORT):
   1)THE SITE WILL BE CLEARED OF ALL TREES NECESSARY FOR SITE CONSTRUCTION, SEE CLEARING LIMITS.
   2)THE TOP 1.0' OF SOIL WILL BE STRIPPED UNDER ALL STRUCTURAL ELEMENTS (BUILDINGS, PARKING & DRIVE AREAS). THIS MATERIAL CAN BE USED ON SITE AS UNCLASSIFIED FILL (GREEN SPACES).
   3)SEE GEOTECH REPORT FOR UNDERCUT RECOMMENDATIONS. SELECT FILL WILL BE PLACED TO 10' OUTSIDE BUILDING, 3' OUTSIDE THE EDGE OF PAVEMENT FOR DRIVES AND PARKING.
   4)PROOF ROLL ALL SUBGRADE PRIOR TO PLACING FILL, REMOVE AND REPLACE WITH COMPACTED SELECT FILL AS DIRECTED BY GEOTECH.
   5)SELECT FILL WILL BE PLACED IN LOOSE 8" LIFTS AND COMPACTED TO 95% MODIFIED PROCTOR WITHIN 2% OPTIMUM MOISTURE CONTENT. SEE GEOTECH REPORT FOR SELECT FILL REQUIREMENTS.
7. THE CONTRACTOR WILL VERIFY THE LOCATION AND ELEVATION OF ALL ROOF, CONDENSATE AND FOUNDATION DRAIN CONNECTIONS WITH THE PLUMBING AND FOUNDATION SHEETS PRIOR TO INSTILLATION.

## GENERAL EROSION CONTROL NOTES:

1. THE CONTRACTOR WILL PRODUCE A STORM WATER POLLUTION PREVENTION PLAN (SWPPP) THAT MEETS THE REQUIREMENTS SET FORTH BY THE ARKANSAS DEPARTMENT OF ENVIRONMENTAL QUALITY.
2. THE CONTRACTOR WILL FILL OUT INSPECTION REPORTS AND LOG RAINFALL DATA AS REQUIRED BY THE SWPPP.
3. THE CONTRACTOR WILL INSTALL ALL EROSION CONTROL MEASURES PRIOR TO COMMENCING DIRTWORK ACTIVITIES ON THIS SITE.
4. THE CONTRACTOR WILL IMMEDIATELY CLEAN UP ANY SEDIMENT THAT LEAVES THIS SITE.
5. THE CONTRACTOR WILL RE-ESTABLISH ALL DISTURBED AREAS IN ACCORDANCE WITH THE SWPPP.
6. THE CONTRACTOR WILL REMOVE ALL EROSION CONTROL MEASURES ONCE THE SITE HAS BEEN RE-ESTABLISHED.




4 C1.0 SILT FENCE DETAIL
SCALE: N.T.S.




5 C1.0 CONCRETE WASHOUT DETAIL
SCALE: N.T.S.

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SITE GRADING & STORM DRAINAGE PLAN

BRYANT ALE CLASSROOM ADDITION
BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

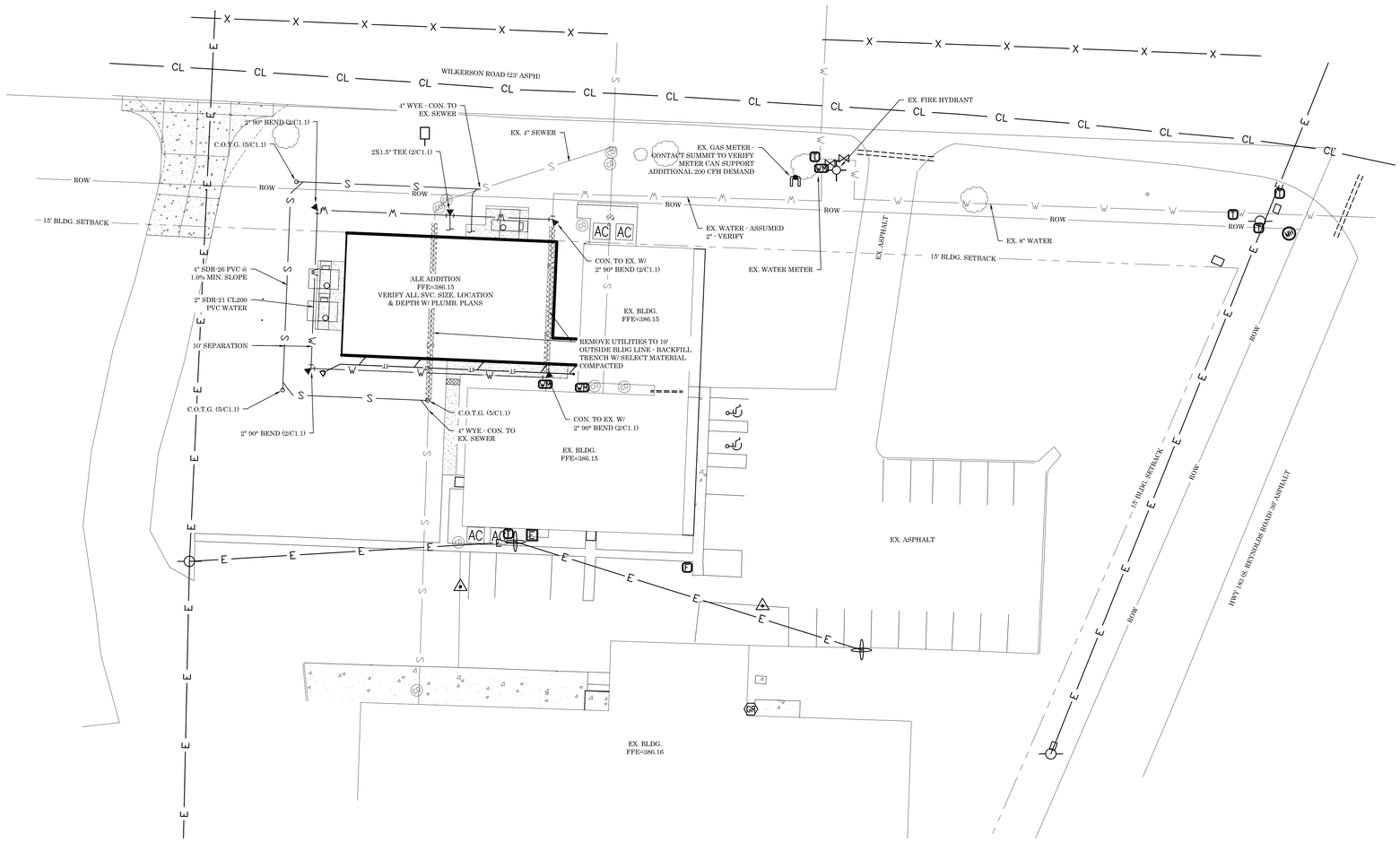
STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 12742
JOSH WILSON
6/9/25

CERTIFICATE OF AUTHORIZATION
MINTON ENGINEERING, INC.
NO. 1584
ARKANSAS ENGINEER

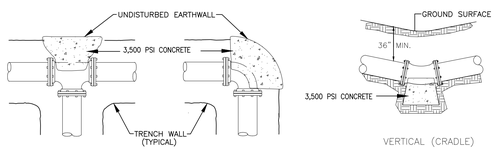
DATE: 2025.06.09
PROJECT NO: 23034
DRAWN BY: JM
REV:

ARKANSAS ONE-CALL SYSTEM, INC.
811 ARKANSAS ONE-CALL BEFORE YOU DIG

C1.0
2 of 3




NORTH 1/C1.1 SITE UTILITY PLAN
SCALE: 1" = 20'
0 20 40



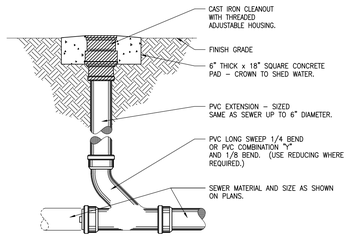

90° BEND
45° BEND (SIMILAR)
22 1/2° BEND (SIMILAR)
11 1/4° BEND (SIMILAR)

45° BEND
22 1/2° BEND (SIMILAR)
11 1/4° BEND (SIMILAR)

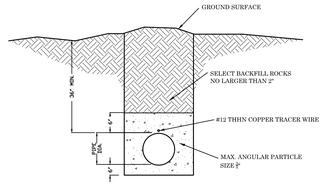
NOTES:
1. All fittings shall be mechanical joint with retainer glands.
2. Do not cover bells or flanges with concrete.
3. Wrap all fittings with visqueen.
4. Back all tees according to size of branch.
5. Backing future line extensions shall be such that later removal is possible.
6. All bends where fittings are used, both horizontal and vertical, shall be backed.
7. Reaction backing table is based on 150 p.s.i. and soil bearing pressure of 2,500 lb./sq. ft. Additional backing may be required in some areas as directed by engineer.

| REACTION BACKING TABLE | | | | | |
|---|---|---|---|---|---|
| REQUIRED SQ. FT. OF UNDISTURBED EARTHWALL FOR REACTION BACKING | | | | | |
| SIZE | TYPE OF FITTINGS | | | | |
| | TEE OR PLUG/CAP | 90° | 45° | 22 1/2° | 11 1/4° |
| 2"-4" | 2 | 2 | 1 | 1 | 1 |
| 6" | 3 | 3 | 2 | 1 | 1 |
| 8" | 4 | 4 | 3 | 2 | 2 |
| 12" | 10 | 10 | 5 | 3 | 2 |
| 18" | 26 | 26 | 14 | 7 | 4 |
| 24" | 38 | 38 | 20 | 10 | 7 |
| 30" | 59 | 59 | 32 | 16 | 10 |

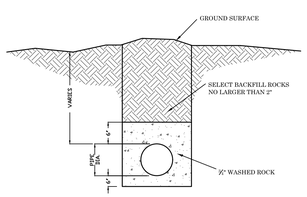
2/C1.1 WATERLINE BLOCKING DETAIL
NOT TO SCALE




5/C1.1 CLEANOUT TO GRADE (C.O.T.G.) DETAIL
NOT TO SCALE




3/C1.1 WATER BEDDING DETAIL
NOT TO SCALE




4/C1.1 SEWER BEDDING DETAIL
NOT TO SCALE

## GENERAL UTILITY NOTES:

1. ALL BIDDERS SHALL FIELD VERIFY EXIST SITE CONDITIONS SO AS TO BE FAMILIAR WITH PROJECT PRIOR TO BIDDING WORK INCLUDED IN THIS CONTRACT. ANY DISCREPANCIES SHALL BE ADDRESSED PRIOR TO BIDDING.
2. CONTRACTOR TO VERIFY AND MARK ALL EXISTING UTILITIES PRIOR BEFORE ANY DEMOLITION OR NEW CONSTRUCTION WORK COMMENCES.
3. ALL WORK SHALL CONFORM TO LOCAL & STATE CODES; ELECTRICAL & PLUMBING LINES SHALL BE INSTALLED BY PROFESSIONALS LICENSED BY THE STATE OF ARKANSAS.
4. ALL WORK SHALL CONFORM TO THE SPECIFICATIONS SET FORTH BY THE ARKANSAS DEPARTMENT OF HEALTH AND BRYANT WATER DEPARTMENT. THE CONTRACTOR WILL BE RESPONSIBLE FOR ANY CONNECTION FEES AND AS-BUILTS REQUIRED.
5. CONTRACTOR TO VERIFY UTILITY CONNECTION LOCATIONS TO THE BUILDING WITH THE PLUMBING SHEETS.
6. SEWER MANHOLES SET IN GREEN SPACE AREAS WILL HAVE A RIM ELEVATION OF AT LEAST 3" BUT NO MORE THAN 5" ABOVE ADJACENT GRADE.
7. ALL WATER AND SEWER LINES SHALL MAINTAIN 10' OF HORIZONTAL SEPARATION AND 18" OF VERTICAL SEPARATION, WATER OVER SEWER. WATERTIGHT CASING WILL BE REQUIRED IF THESE DIMENSIONS CAN NOT BE ACHIEVED. SEPARATION REQUIREMENTS B/T WATER AND SEWER WILL FULLY COMPLY WITH THE ARKANSAS RULES PERTAINING TO PUBLIC WATER SYSTEMS SECTION XIV A.

## GRADATION PLAN NOTE

PRIOR TO INSTALLING ANY SANITARY, STORM, GAS OR WATER LINES BELOW GRADE, THE PLUMBING CONTRACTOR SHALL FURNISH TO THE ARCHITECT TWO COPIES OF A GRADATION PLAN OF THE BUILDING DRAINS AND SEWER LINES WITH PROPOSED ELEVATION GRADES SHOWN AT EACH MAJOR GROUP OF PLUMBING FIXTURES, AT EACH PIPE LINE INTERSECTION, AT EACH PIPE LINE CROSSING, AT EACH GRADE BEAM OR FOOTING PENETRATION/INTERSECTION AND AT ANY EXISTING PIPE LINE CONNECTIONS. THE PLAN SHALL ALSO INCLUDE ALL THOSE PIPE INTERSECTIONS AND/OR PIPE CROSSINGS THAT ARE EXTERIOR OF BUILDING/ADDITION INCLUDING ANY MANHOLES, CONNECTION TO EXISTING MAINS AND CLEANOUTS TO GRADE.

ARKANSAS ONE CALL SYSTEM INC. DIAL 811 BEFORE YOU DIG

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501.223.9302 • FAX 501.223.9909 • WWW.LEWVRW.COM

SITE UTILITY PLAN

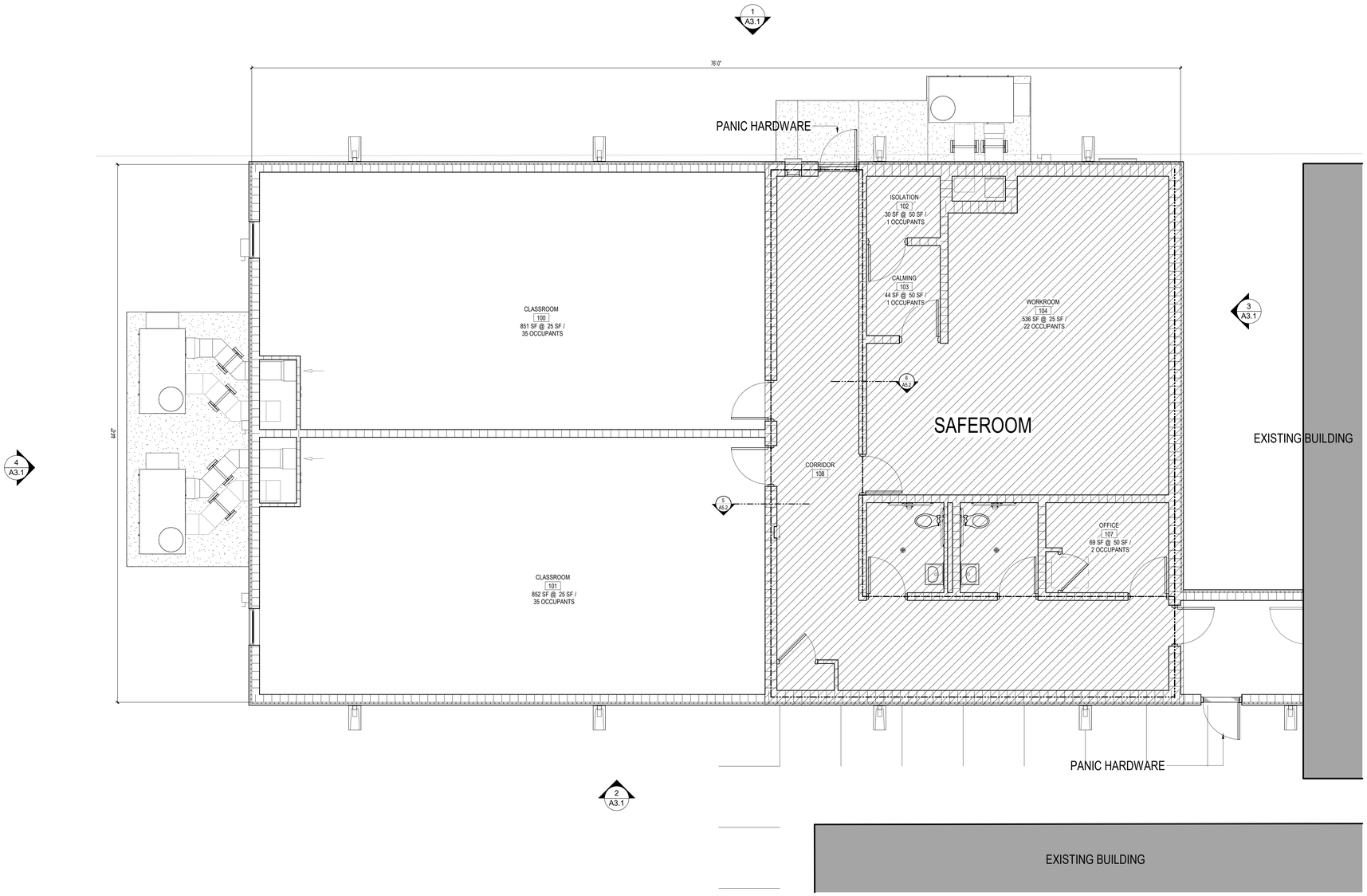
BRYANT ALE CLASSROOM ADDITION
BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 12742
6/9/25

CERTIFICATE OF AUTHORIZATION
WINTON ENGINEERING, INC.
NO. 1564
ARKANSAS ENGINEER

DATE: 2025-06-09
PROJECT NO: 23034
DRAWN BY: JM
REV:

C1.1
3 OF 3




NORTH

1 A1.0 LIFE SAFETY PLAN
1/4" = 1'-0"

## IBC TABLE 601
## FIRE-RESISTANCE RATING REQUIREMENTS FOR BUILDING ELEMENTS

| BUILDING ELEMENT | TYPE I | | TYPE II | | TYPE III | | TYPE IV | TYPE V | |
|---|---|---|---|---|---|---|---|---|---|
| | A | B | A | B | A | B | HT | A | B |
| PRIMARY STRUCTURAL FRAME | 3 | 2 | 1 | 0 | 1 | 0 | HT | 1 | 0 |
| BEARING WALLS | | | | | | | | | |
| EXTERIOR | 3 | 2 | 1 | 0 | 2 | 2 | 2 | 1 | 0 |
| INTERIOR | 3 | 2 | 1 | 0 | 1 | 0 | 1/HT | 1 | 0 |
| NONBEARING INTERIOR WALLS | | | | | | | | | |
| FLOOR CONSTRUCTION AND ASSOCIATED SECONDARY MEMBERS | 2 | 2 | 1 | 0 | 1 | 0 | HT | 1 | 0 |
| ROOF CONSTRUCTION AND ASSOCIATED SECONDARY MEMBERS | 1.5 | 1 | 1 | 0 | 1 | 0 | HT | 1 | 0 |

## FIREPROOFING NOTES: TYPE V-B CONSTRUCTION

| BUILDING ELEMENT | RATING | APPLICATION/PRODUCT |
|---|---|---|

NOTES: ALL STRUCTURAL STEEL SHALL BE UNPAINTED/UNPRIMED UNLESS NOTED OTHERWISE.
ALL METAL FLOOR AND ROOF DECK SHALL BE GALVANIZED OR UL CLASSIFIED PAINTED DECK

## LIFE SAFETY: STORM SHELTER

**FIRE AREA EDUCATION, NS,TYPE VB**

ALLOWABLE AREA FACTOR NS, VB (TABLE 506.2):
9,500 SF PER FLOOR

FRONTAGE INCREASE:
240' BUILDING PERIMETER
168' OF PERIMETER FACE 30+' OF OPEN SPACE
68% OF BUILDING PERIMETER

9,500 (NS AREA FACTOR)
x .68 INCREASE FACTOR
6,460 SF INCREASE

TOTAL ALLOWABLE AREA:
**15,960 SF PER FLOOR**

ACTUAL AREA (MEASURED WITHIN EXTERIOR WALLS):
**3,035 SF LOWER LEVEL**

ALLOWABLE HEIGHT (TABLE 504.3):
40 FEET

ACTUAL HEIGHT
16' 10" FEET

ALLOWABLE STORIES (TABLE 504.4):
ONE STORY

ACTUAL STORIES:
ONE STORY

**FIRE AREA MAIN LEVEL OCCUPANT LOAD:**

TOTAL: 168 OCCUPANTS
EXITS REQUIRED: 2 (2 PROVIDED)
EGRESS REQUIRED: 168 OCCUPANTS/2 EXITS = 84 OCCUPANTS PER EXIT

DOORS = 84 OCCUPANTS TRANSLATES TO 55" PER EXIT DOOR MIN.

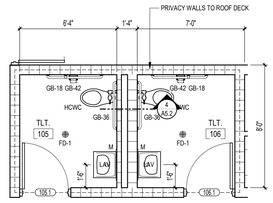
**FIRE AREA STORM SHELTER OCCUPANT LOAD CONTRIBUTION: IBC 423.5**

CLASSROOMS: 2
OFFICES: 1 OCCUPANTS
TOTAL: 168 OCCUPANTS

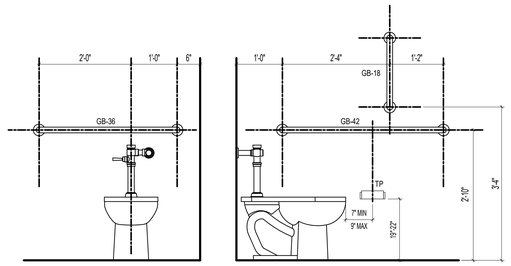
TOTAL LOAD CONTRIBUTION TO STORM SHELTER:
168 OCC. - (168 OCC. x .25 NET SF REDUCTION FACTOR) = **126 OCCUPANTS**

## FIRE WALL LEGEND

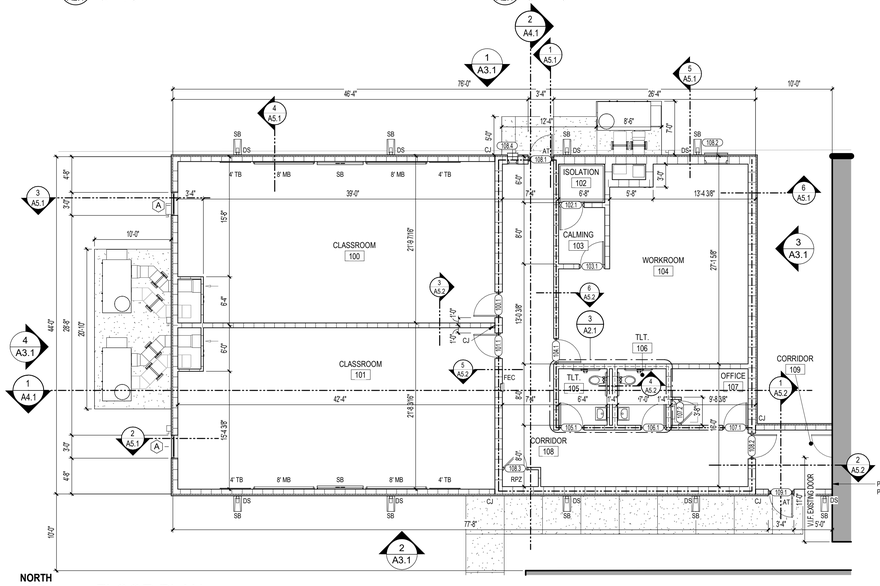
**2-HR FIRE WALL** — ·—·—·—



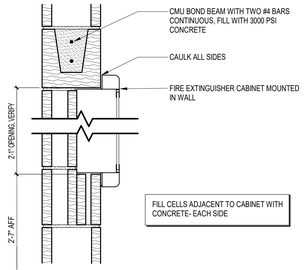

3 A2.1 ENLARGED PLAN
1/4" = 1'-0"



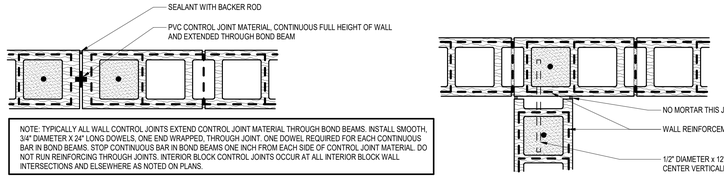

6 A2.1 GRAB BAR ELEVATIONS
3/4" = 1'-0"




NORTH
1 A2.1 FLOOR PLAN
1/8" = 1'-0"

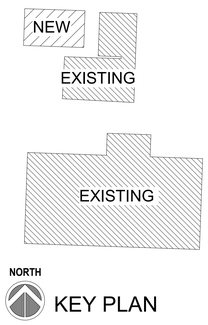



5 A2.1 FIRE EXTINGUISHER CABINET-CMU
1 1/2" = 1'-0"




NOTE: TYPICALLY ALL WALL CONTROL JOINTS EXTEND CONTROL JOINT MATERIAL THROUGH BOND BEAMS. INSTALL SMOOTH, 3/4" DIAMETER X 24" LONG DOWELS, ONE END WRAPPED, THROUGH JOINT. ONE DOWEL REQUIRED FOR EACH CONTINUOUS BAR IN BOND BEAMS. STOP CONTINUOUS BAR IN BOND BEAMS ONE INCH FROM EACH SIDE OF CONTROL JOINT MATERIAL. DO NOT RUN REINFORCING THROUGH JOINTS. INTERIOR BLOCK CONTROL JOINTS OCCUR AT ALL INTERIOR BLOCK WALL INTERSECTIONS AND ELSEWHERE AS NOTED ON PLANS.

7 A2.1 INTERIOR MASONRY CONTROL JOINT - CMU
1 1/2" = 1'-0"




NORTH
KEY PLAN

## GENERAL SITE NOTES

1. ALL WORK AND MATERIALS SHALL COMPLY WITH ALL CITY/COUNTY REGULATIONS AND CODES AND O.S.H.A. STANDARDS.
2. THE SITE WORK FOR THIS PROJECT SHALL MEET OR EXCEED THE "PROJECT SPECIFICATIONS".
3. CONTRACTOR SHALL REFER TO THE ARCHITECTURAL PLANS FOR EXACT LOCATIONS AND DIMENSIONS OF VESTIBULES, SLOPE PAVING, SIDEWALKS, EXIT PORCHES, PRECISE BUILDING DIMENSIONS, EXACT BUILDING UTILITY ENTRANCE LOCATIONS, ETC.
4. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL RELOCATIONS, (UNLESS OTHERWISE NOTED ON PLANS) INCLUDING BUT NOT LIMITED TO, ALL UTILITIES, STORM DRAINAGE, SIGNS, ETC. AS REQUIRED. ALL WORK SHALL BE IN ACCORDANCE WITH GOVERNING AUTHORITIES REQUIREMENTS AND PROJECT SPECIFICATIONS AND SHALL BE APPROVED BY SUCH. ALL COSTS SHALL BE INCLUDED IN BASE BID.
5. ALL DIMENSIONS ARE TO THE FACE OF CURB UNLESS OTHERWISE NOTED.
6. ALL PAVING TO BE STANDARD DUTY ASPHALTIC CONCRETE PAVING UNLESS OTHERWISE NOTED.
7. ALL CURB/HANDICAP RAMP DESIGN SHALL CONFORM TO ADA STANDARDS.
8. ALL NEW PARKING SPACES ARE TO BE PAINTED WITH 4" SINGLE WHITE SOLID LINES UNLESS OTHERWISE NOTED.
9. ALL HANDICAP SPACES ARE TO RECEIVE A HANDICAP SIGN (SIGN R7-8 PER FEDERAL MANUAL ON TRAFFIC CONTROL DEVICES). PAINTED ACCESSIBLE SYMBOLS SHALL BE INSTALLED IN ALL HANDICAP SPACES AS SHOWN ON THE PLANS. HANDICAP SPACES AND SYMBOLS SHALL BE PAINTED BLUE OR PER LOCAL CODE.
10. ALL TRAFFIC SIGNAGE, PAVEMENT MARKINGS, AND PARKING LOT STRIPING SHALL CONFORM TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD) REQUIREMENTS.
11. ALL DISTURBED AREAS ARE TO RECEIVE FOUR (4) INCHES OF TOPSOIL, SEED, MULCH AND WATER UNTIL A HEALTHY STAND OF GRASS IS ESTABLISHED.
12. PATCH AND REPAIR EXISTING PAVING WHERE DISTURBED BY NEW CONSTRUCTION BEYOND SAW-CUT JOINT FOR NEW CONSTRUCTION
13. SITE BOUNDARY, TOPOGRAPHY, UTILITY AND ROAD INFORMATION WAS TAKEN FROM A SURVEY BY JOHNSTON SURVEYING OF ROLAND, ARKANSAS.

## FIRE WALL LEGEND

**2-HR FIRE WALL** — 12" CONCRETE MASONRY UNITS TO BOTTOM OF ROOF DECK (UL #U905). FIRE STOP AT DECK AND ALL PENETRATIONS. DO NOT TIE PARALLEL FIRE WALLS TOGETHER

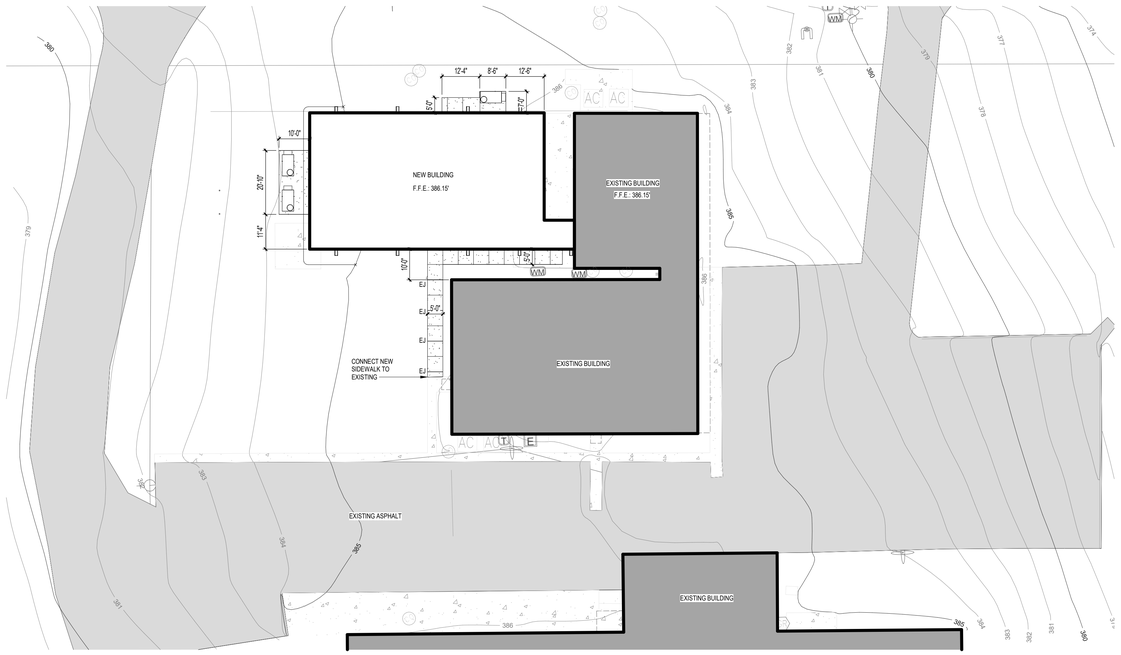
**1-HR FIRE WALL** — 8" CONCRETE MASONRY UNITS TO BOTTOM OF ROOF DECK. (UL #U905). FIRE STOP AT DECK AND ALL PENETRATIONS. DO NOT TIE PARALLEL FIRE WALLS TOGETHER

**NOTE:**
ALL FIRE WALLS AND BARRIERS SHALL BE MARKED WITH SIGNAGE READING, "FIRE AND/OR SMOKE BARRIER- PROTECT ALL OPENINGS" ACCORDING TO 2012 ARKANSAS FIRE PREVENTION CODE SECTION 703.7

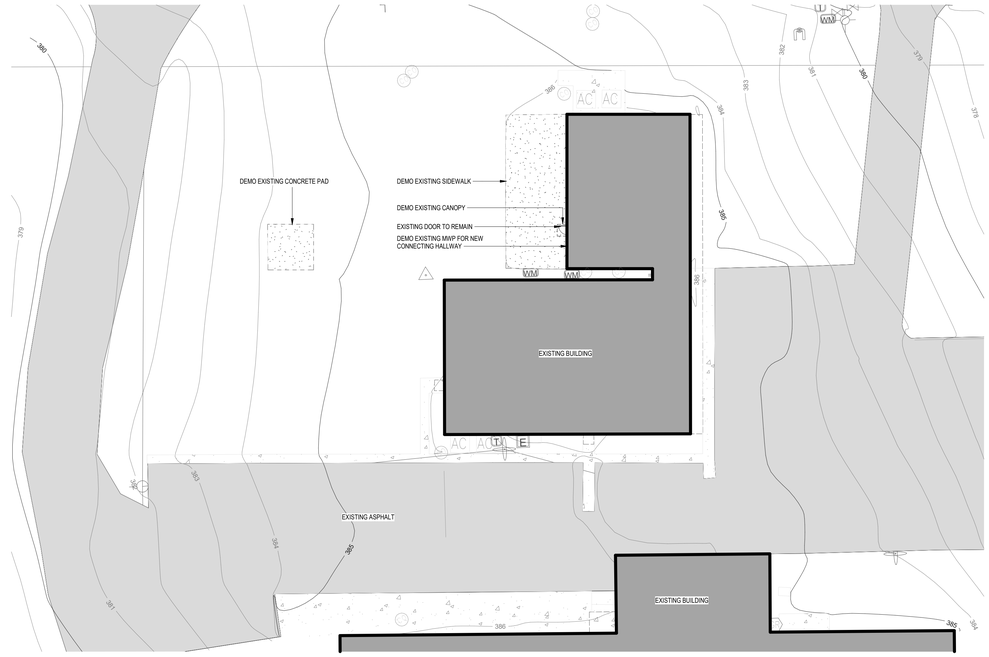
ALL PENETRATIONS SHALL BE PROTECTED BY AN APPROVED THROUGH-PENETRATION FIRESTOP SYSTEM IN ACCORDANCE WITH UL 1479

## GENERAL NOTES

1. SEE OVERALL PLAN SHEET A1.1 FOR CODE DATA AND FIRE PROTECTION REQUIRMENTS AND METHODS
2. CONTRACTOR TO VISIT SITE TO BECOME FAMILIAR WITH EXISTING CONDITIONS PRIOR TO BIDDING PROJECT. BRING ANY DISCREPANCIES TO THE ATTENTION OF THE ARCHITECT PRIOR TO BID.
3. INTERIOR LIGHT GAUGE METAL STUD WALLS
   1. WALLS SHALL BE FRAMED WITH 3 5/8" OR 6" (SEE PLAN) MEMBERS AT 16" O.C. w/ CONTINUOUS TRACK TOP AND BOTTOM, UNLESS NOTED OTHERWISE.
   2. EXTEND ALL WALLS 8" MIN. ABOVE CEILING
   3. WALLS WITHOUT AN ADJACENT FINISHED CEILING SHALL EXTEND TO DECK ABOVE
   4. LIGHT GAUGE FRAMING NOT SUFFICIENTLY BRACED BY INTERSECTING FRAMING OR REQUIRED BY HEIGHT OF FRAMING SHALL BE BRACED TO STRUCTURE WITH METAL STUD KICKERS (APPROXIMATELY 45 DEGREES) AT 48" ON CENTER MAXIMUM.
4. INTERIOR CONCRETE BLOCK WALLS
   1. WALLS SHALL BE 8" CMU (4" CMU AT CHASE WALLS, TOILET PARTITIONS, AND COLUMN WRAPS)
   2. WALL SHALL EXTEND TO 8" ABOVE HIGHEST ADJACENT CEILING
   3. WALLS WITHOUT AN ADJACENT FINISHED CEILING SHALL EXTEND TO 10'-8" AFF AND EXTEND TO DECK WITH METAL STUD FRAMING WITH 5/8" GYPSUM (EXPOSED SIDE(S)
   4. SEE STRUCTURAL DRAWINGS FOR REINFORCING
5. PRIVACY WALLS (BLOCK OR STUD) SHALL EXTEND TO CONCRETE CAP. PRIVACY WALLS SHALL BE MARKED THUS:
6. INTERIOR DOORS NOT DIMENSIONS SHALL BE LOCATED AS FOLLOWS:
   1. HINGE SIDE ADJACENT TO INTERSECTING WALL (CMU)
   2. LATCH SIDE 1'-4" OFF INTERSECTING WALL (STUD/CMU)
   3. CENTERED BETWEEN INTERSECTING WALLS (STUD/CMU)
7. PROVIDE HOUSEKEEPING PADS FOR ELECTRICAL AND MECHANICAL EQUIPMENT. VERIFY SIZE AND LOCATION WITH ELECTRICAL, PLUMBING, AND HVAC INSTALLERS AND MANUFACTURERS.
8. FOR SOUND TRANSFER CONTROL, FILL STUD WALLS WITH SOUND ATTENUATION BLANKETS. INSTALL BATT INSULATION ON ALL CEILING AROUND PERIMETER OF ROOMS EXTENDING 2'-0" FROM ALL INTERIOR WALLS UNLESS NOTED OTHERWISE IN REFLECTED CEILING PLAN NOTES.
9. GYPSUM BOARD EXPANSION JOINTS SHALL BE LOCATED 30'-0" O.C. MAXIMUM. VERIFY LOCATIONS WITH ARCHITECT. LOCATE ABOVE DOOR HEADS WHERE POSSIBLE.
10. FIELD VERIFY ALL DIMENSIONS FOR HANDRAILS, EQUIPMENT, ETC. PRIOR TO FABRICATION AND INSTALLATION
11. PROVIDE WOOD FOR BLOCKING WHERE BLOCKING IS REQUIRED. WHERE BLOCKING CONTACTS METAL FRAME, STUDS, ETC. SEPARATE WITH BUILDING FELT TO AVOID REACTIONS BETWEEN WOOD AND METALS.
12. ALL FIRE WALLS AND BARRIERS SHALL BE MARKED WITH SIGNAGE READING, "FIRE AND/OR SMOKE BARRIER- PROTECT ALL OPENINGS" ACCORDING TO 2021 ARKANSAS FIRE PREVENTION CODE SECTION 703.7. ALL PENETRATIONS SHALL BE PROTECTED BY AN APPROVED THROUGH-PENETRATION FIRESTOP SYSTEM IN ACCORDANCE WITH UL 1479




NORTH
2 A2.1 SITE PLAN
1" = 20'-0"




NORTH
4 A2.1 DEMO PLAN
1" = 20'-0"

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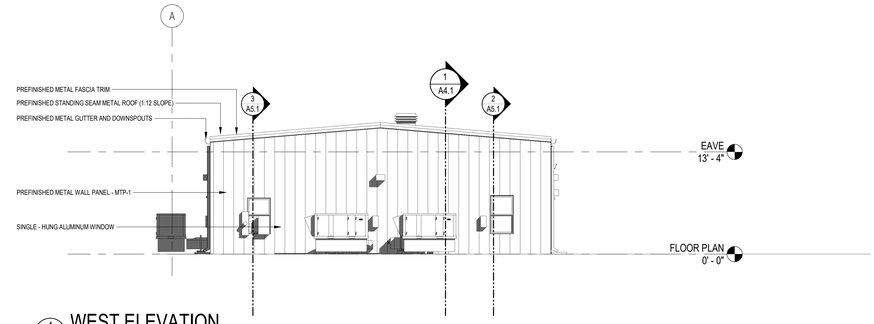
DEMO, SITE, & FLOOR PLAN

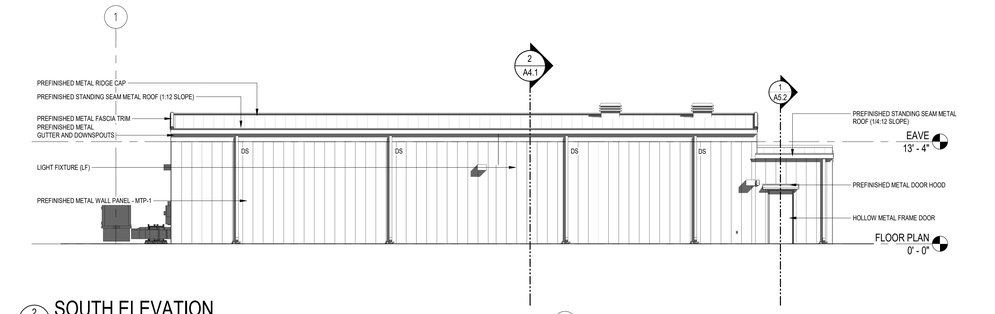
BRYANT ALE CLASSROOM ADDITION
BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

DATE: 2025 06-09
PROJECT NO: 25034
DRAWN BY: BGA
REV:

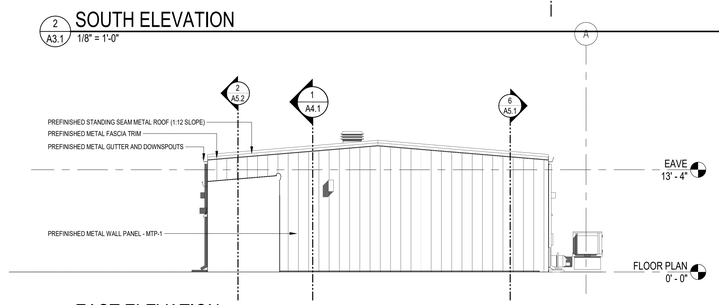
A2.1



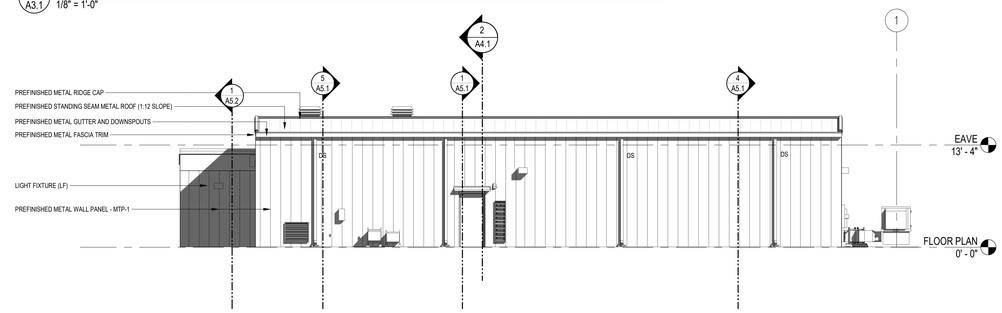

4 A3.1 WEST ELEVATION
1/8" = 1'-0"




2 A3.1 SOUTH ELEVATION
1/8" = 1'-0"




3 A3.1 EAST ELEVATION
1/8" = 1'-0"




1 A3.1 NORTH ELEVATION
1/8" = 1'-0"

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BUILDING ELEVATIONS

BRYANT ALE CLASSROOM ADDITION
BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

DATE: 2025 06-09
PROJECT NO: 25034
DRAWN BY: BGA
REV:

A3.1

minton engineering
300 North Port Drive
Cabot, AR 72023
(501) 941-5559

July 9, 2025

Mr. Colton Leonard
City of Bryant - Planning
210 S.W. 3rd St.
Bryant, AR 72022

Re: Site Plan Review, ALE Addition, Bryant School District, Bryant, AR

Mr. Leonard:

Below is our response to the DRC comments:

Public Works:

1. The existing 4" sewer service line is adequate to serve the existing buildings as well as the addition.
2. Concrete apron has been added to this drive.
3. Will comply w/ impact fees.

Stormwater:

1. Stormwater report is attached.
2. It is my understanding that Terry Harper (Bryant Schools) worked out that no detention will be required.
3. Erosion control has been added to sheet C1.0.

Engineering:

1. Sheet titles fixed.
2. Stormwater report is attached.
3. There is an adequate # of ADA spaces for this facility.
4. Pipe under the existing east drive is shown to be replaced.

5. A waiver has been requested for the non-conforming building standards.

Planning:

1. Here is the explanation from the mechanical engineer concerning the HVAC units on the north side of the addition: The gas package unit serving the protected area of the building was strategically positioned to optimize available space and provide service to the area in the most efficient and cost-effective way. Its current location allows for a dedicated duct chase within the protected area, minimizing complexity and expense. Relocating the unit would place it farther from the area it serves, requiring additional duct chases and potentially increasing the building's square footage to meet POR requirements where the ducts would enter. This would result in potential higher construction costs and a less efficient design.

2. Screen walls are added for the HVAC units on the north side of the addition as well as for the existing HVAC units on the north side of the existing building.

3. See attached Site Plan for fencing limits.

4. Handicap accessibility will come from the connection to the existing building.

Fire:

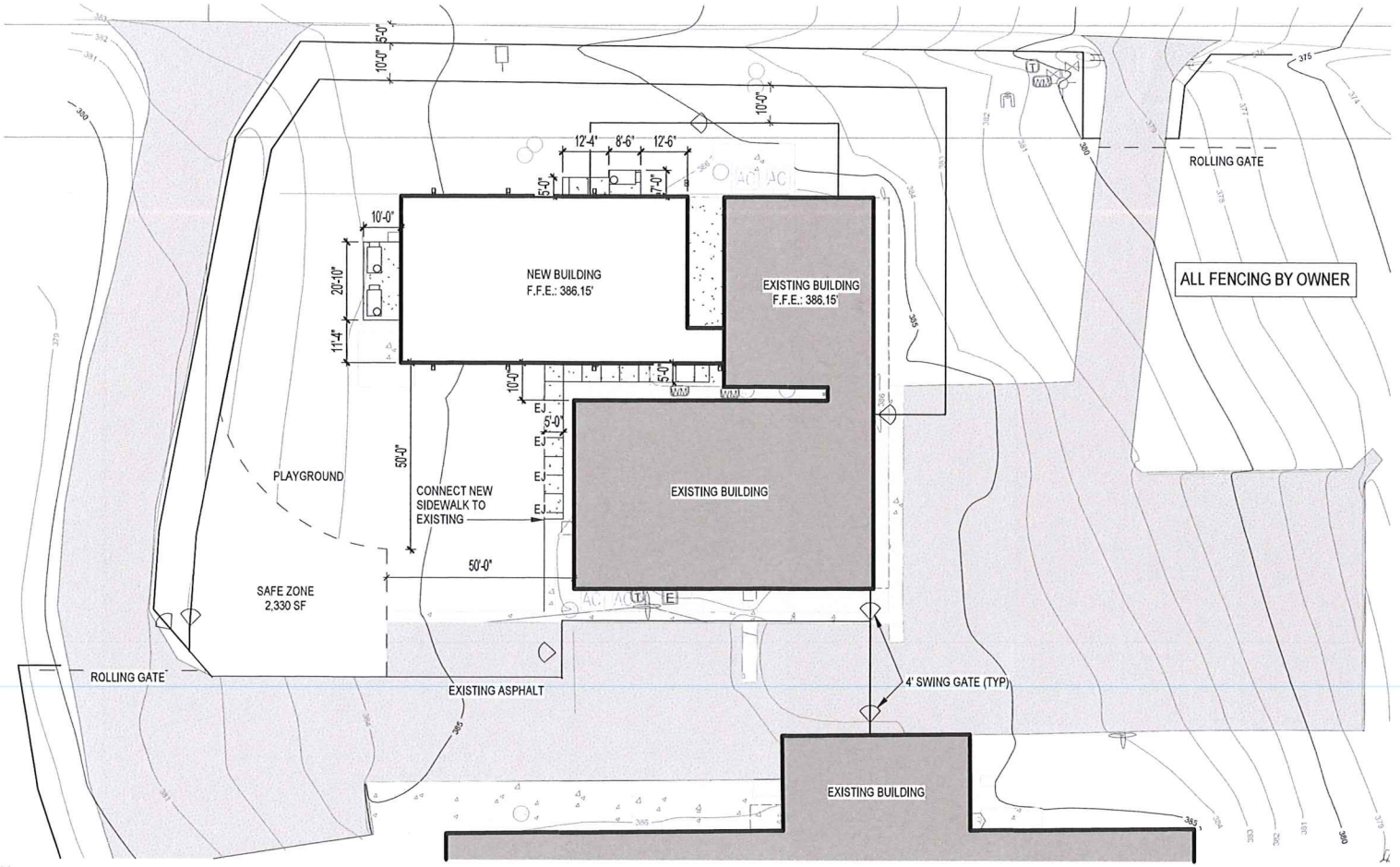
1. See attached Site Plan for fencing limits and Safe Zone requirements.

2. The Safe Room occupant load capacity is 305 based on the square footage.

Sincerely,

Josh Minton, PE
Project Engineer

Cc: Randy Wolf, AIA – Lewis Architects




NORTH

1 / A9.0 SITE PLAN

1" = 30'-0"

# BRYANT ALE CLASSROOM ADDITION

BRYANT PUBLIC SCHOOLS
BRYANT, ARKANSAS

## SITE PLAN

FOR REVIEW

LEWIS ARCHITECTS ENGINEERS
ELLIOTT • MCMORRAN • VADEN
RAGSDALE • WOODWARD • INCORPORATED
501.223.8702 • WWW.LEMVRW.COM

| JOB NO: | DATE: | SCALE: | DRAWING NO: |
|---|---|---|---|
| 25034 | 2025 07-01 | 1" = 30'-0" | A9.0 |

RICHARDSON ENGINEERING
Planning ▪ Engineering ▪ Development Consulting

June 26, 2025

City of Bryant
Development & Review Committee
Attn: Mr. Truett Smith
Director of Community Development

RE: Letter of Request for approval of Commercial Replat for The Shoppes at Dogwood Springs, Saline County, Arkansas

Dear Mr. Smith:

Please accept this letter as a request to approve the Commercial Replat for The Shoppes at Dogwood Springs.

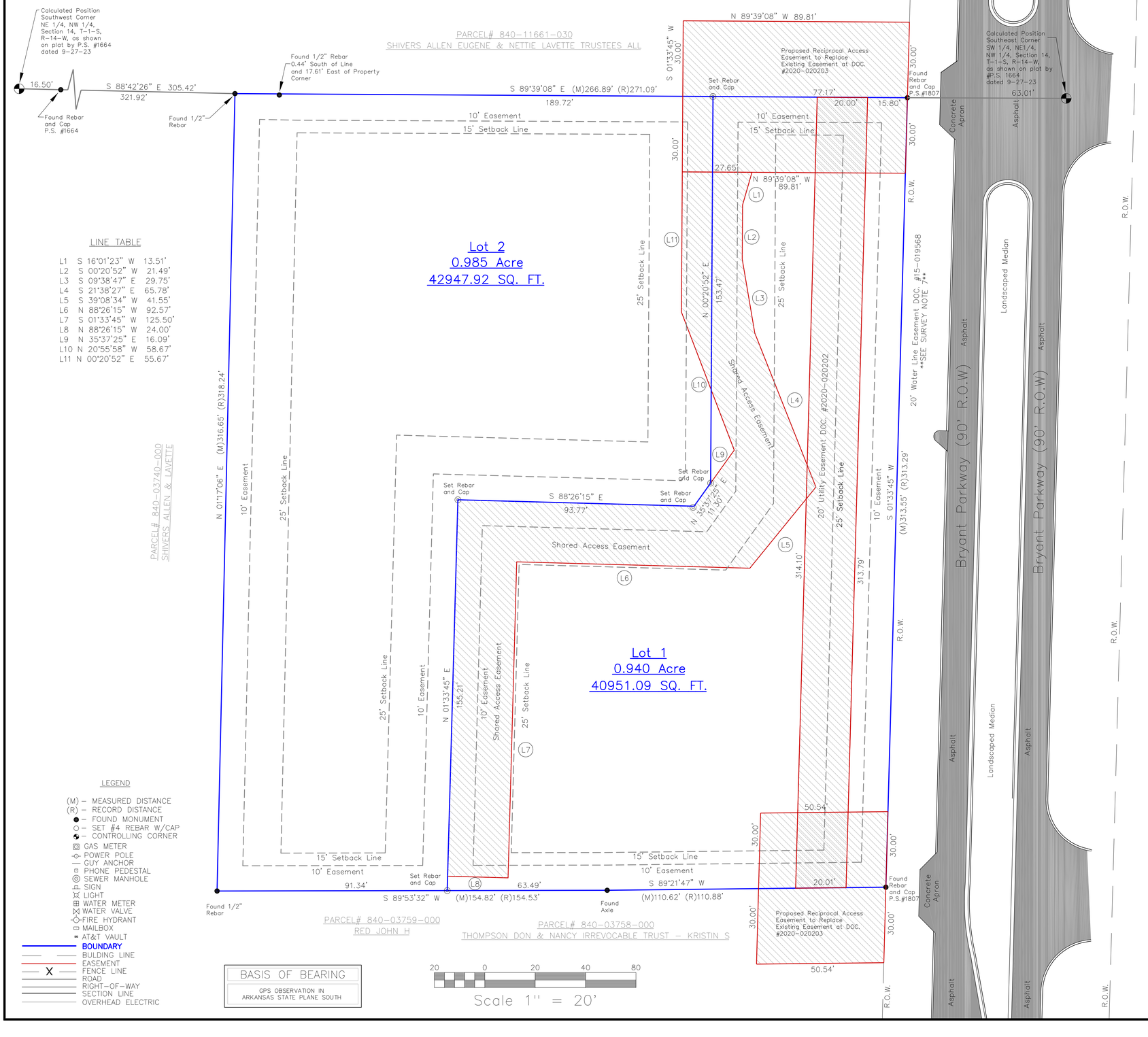
**Engineer's Information:**
Tristin Phillips, PE
Richardson Engineering, PLLC
P.O. Box 192
Benton, AR 72018
Tristin@Richardson-Engrs.com
(501) 315-7225

Sincerely,

Tristin Phillips, PE

Encl.

# FINAL PLAT OF
# THE SHOPPES AT DOGWOOD SPRINGS, CITY OF BRYANT, SALINE COUNTY, ARKANSAS




## LINE TABLE

| | | |
|---|---|---|
| L1 | S 16°01'23" W | 13.51' |
| L2 | S 00°20'52" W | 21.49' |
| L3 | S 09°38'47" E | 29.75' |
| L4 | S 21°38'27" E | 65.78' |
| L5 | S 39°08'34" W | 41.55' |
| L6 | N 88°26'15" W | 92.57' |
| L7 | S 01°33'45" W | 125.50' |
| L8 | N 88°26'15" W | 24.00' |
| L9 | N 35°37'25" E | 16.09' |
| L10 | N 20°55'58" W | 58.67' |
| L11 | N 00°20'52" E | 55.67' |

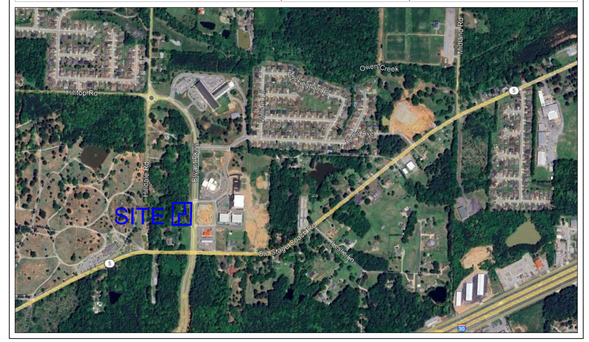
## LEGEND

- (M) – MEASURED DISTANCE
- (R) – RECORD DISTANCE
- ● – FOUND MONUMENT
- ○ – SET #4 REBAR W/CAP
- ◆ – CONTROLLING CORNER
- GAS METER
- POWER POLE
- GUY ANCHOR
- PHONE PEDESTAL
- SEWER MANHOLE
- SIGN
- LIGHT
- WATER METER
- WATER VALVE
- FIRE HYDRANT
- MAILBOX
- AT&T VAULT
- BOUNDARY
- BULDING LINE
- EASEMENT
- FENCE LINE
- ROAD
- RIGHT-OF-WAY
- SECTION LINE
- OVERHEAD ELECTRIC

BASIS OF BEARING
GPS OBSERVATION IN ARKANSAS STATE PLANE SOUTH

20 0 20 40 80
Scale 1" = 20'

VICINITY MAP (NOT TO SCALE)




## SURVEY DESCRIPTION

ALL OF BLOCK 4, THE EAST HALF OF BLOCK 5, LOT 1 OF BLOCK 8, AND LOTS 1 AND 2 OF BLOCK 9, TOGETHER WITH A PORTION OF NORTHERN AVENUE, NORTH STREET, AND LIBERTY STREET RIGHT OF WAYS ADJACENT TO SAID BLOCKS, AS SHOWN ON THE PLAT OF THE TOWN OF COLLEGEVILLE AS FILIED IN THE SALINE COUNTY RECORDS AT BOOK 11, PAGE 327; ALSO BEING A PART OF THE SOUTHEAST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14, TOWNSHIP 1 SOUTH, RANGE 14 WEST, SALINE COUNTY ARKANSAS, MORE PARTICULARLY DESCRIBED AS FOLLOWS: COMMENCING AT THE NORTHWEST CORNER OF THE SAID SE1/4, NW1/4, AND RUN THENCE ALONG THE NORTH LINE THEREOF S 88°42'26" E A DISTANCE OF 321.92' TO A FOUND 1/2" REBAR AT THE POINT OF BEGINNING; THENCE S 89°39'08" E A DISTANCE OF 266.89' TO A FOUND REBAR AND CAP ON THE WEST RIGHT OF WAY OF BRYANT PARKWAY; THENCE ALONG SAID WEST RIGHT OF WAY S 01°33'45" W A DISTANCE OF 313.55' TO A FOUND REBAR AND CAP; THENCE LEAVING SAID RIGHT OF WAY S 89°21'47" W A DISTANCE OF 110.62' TO A FOUND AXLE; THENCE S 89°53'32" W A DISTANCE OF 154.82' TO A FOUND 1/2" REBAR; THENCE N 01°17'06" E A DISTANCE OF 316.65' TO THE POINT OF BEGINNING CONTAINING 1.898 ACRES MORE OR LESS.

## CERTIFICATE OF PROPERTY OWNERSHIP

WE THE UNDERSIGNED, OWNERS OF THE REAL ESTATE SHOWN AND DESCRIBED HEREIN, DO HEREBY CERTIFY THAT WE HAVE LAID OFF, PLATTED AND SUBDIVIDED, AND DO HEREBY LAYOFF, PLAT AND SUBDIVIDE SAID REAL ESTATE IN ACCORDANCE WITH THIS PLAT.

SIGNED_____DATE_____

BOOK_____PAGE_____

INSTRUMENT NO._____

## CERTIFICATE OF FINAL PLAT APPROVAL

PURSUANT TO THE CITY OF BRYANT SUBDIVISION RULES AND REGULATIONS, AND ALL OF THE CONDITIONS OF APPROVAL HAVING BEEN COMPLETED, THIS DOCUMENT IS HEREBY ACCEPTED. THIS CERTIFICATE IS HEREBY EXECUTED UNDER THE AUTHORITY OF SAID RULES AND REGULATIONS.

_____

SIGNED: DATE:
BRYANT PLANNING

## CERTIFICATE OF SURVEYING ACCURACY

I, KIRT SLEDGE, HEREBY CERTIFY THAT THIS PLAT CORRECTLY REPRESENTS A BOUNDARY SURVEY COMPLETED BY ME, OR UNDER MY SUPERVISION ON JUNE 17, 2025, THAT ALL MONUMENTS SHOWN HEREON ACTUALLY EXIST AND THEIR LOCATION, SIZE, TYPE AND MATERIAL ARE CORRECTLY SHOWN; AND THAT ALL SURVEY REQUIREMENTS OF THE CITY OF BRYANT SUBDIVISION RULES AND REGULATIONS HAVE BEEN COMPLIED WITH.

Kirt Sledge 6-22-25

KIRT SLEDGE DATE OF EXECUTION
REGISTERED PROFESSIONAL SURVEYOR
NO.1665, ARKANSAS

## CERTIFICATE OF ENGINEERING ACCURACY

I, TRISTIN PHILLIPS, HEREBY CERTIFY THAT I AM THE ENGINEER OF RECORD FOR THIS SUBDIVISION, AND THAT I OR THOSE MADE BY ME UNDER MY SUPERVISION WILL DESIGN AND MONITOR THE CONSTRUCTION OF THE IMPROVEMENTS REQUIRED IN ACCORD WITH THE CITY OF BRYANT SUBDIVISION REGULATION ORDINANCE.

_____

TRISTIN PHILLIPS DATE OF EXECUTION
REGISTERED PROFESSIONAL ENGINEER
NO. 21954, ARKANSAS

## CERTIFICATE OF RECORDING

THIS DOCUMENT, NUMBER _____, FILED FOR RECORD _____, 2025,
IN PLAT BOOK _____, PAGE _____.

_____
NAME (CLERK)
FOR BILL OF ASSURANCE SEE DEED RECORD

BOOK_____, PAGE ____

## SURVEYOR'S NOTES

1. Source of Title: Book 2020, Page 020202.
2. No statement is made as to the existence, correctness, or location, except where shown, of any property corner monument.
3. All easements known to South Point Surveying at the time of the survey are shown on the drawing, but no statement is made as to the completeness of the easements shown. Tract is subject to easements, restrictive covenants, subdivision restrictions, and planning and zoning regulations of record, if any, and is subject to such facts as an accurate and current title search may disclose.
4. Error of Closure: this survey meets the State of Arkansas Minimum Standards for Error of Closure in Urban Surveys of 1 part in 10,000.
5. As shown on Flood Insurance Rate Map Number 05125C0240E dated June 5, 2020, this property lies in Zone X and is not in a Special Flood Hazard Area.
6. According to the City of Bryant Zoning Map, this property is zoned as C-2.
7. A Water and Sewer Easement recorded at Saline County Document #15-019568 is described as being 20' in width along the west side of Snooks Lane, a road that no longer exists and appears to have originally been somewhere in the vicinity of what is now Bryant Parkway.

STATE PLAT CODE; 500-01S-14W-0-14- 400-62-1665


SOUTH POINT SURVEYING, PLLC
P.O. Box 400 Sheridan, AR 72150
southpointsurveying@yahoo.com
501-285-5958 501-837-2342


| Drawing: | Date: | Page: | Drawn by: |
|---|---|---|---|
| BRYANT PARKWAY | 6/22/24 | 1/1 | MRO |

THE SHOPPES AT DOGWOOD SPRINGS
BRYANT, ARKANSAS

GAS METER
WATER METER
GUY WIRE
POWER/UTILITY POLE
TELEPHONE PEDESTAL
SEWER MANHOLE
WATER VALVE
FIRE HYDRANT
SIGNS
LIGHT POLE
TELEPHONE MANHOLE
SS SANITARY SEWER LINE
W WATER LINE
STORM SEWER PIPE
ROADWAY CENTERLINE
UTILITY EASEMENT
BUILDING SETBACK LINE
R/W ROADWAY RIGHT-OF-WAY
OHE OVERHEAD ELECTRIC LINES
UGT UNDERGROUND TELEPHONE
G UNDERGROUND GAS
F.O. UNDERGROUND FIBER OPTIC

STORM DRAIN MANHOLE
SEWER CLEANOUT
N NORTH
S SOUTH
E EAST
W WEST
(M) AS MEASURED
(D) PER DEED
(R) RECORDED
R/W RIGHT-OF-WAY
L.A. LANDSCAPED AREA
CR4 CAPPED 1/2" REBAR
CONC. CONCRETE
P.O.C. POINT OF COMMENCEMENT
P.O.B. POINT OF BEGINNING
CMP CORRUGATED METAL PIPE
RCP REINFORCED CONCRETE PIPE
ESMT EASEMENT
HDPE HIGH DENSITY POLYETHYLENE
SUBD SUBDIVISION
FDC FIRE DEPARTMENT CONNECTION
CPS COTTON PICKER SPINDLE
P5 5/8" PIPE

ASPHALT
CONCRETE

SET 1/2" REBAR w/ CAP #1853
SET COTTON-PICKER SPINDLE
FOUND MONUMENT (DESC. NOTED)
COMPUTED CORNER (NOT SET)
CORRESPONDS TO DRAWING NOTE

## SHEET INDEX


| SHEET NUMBER | SHEET TITLE |
|---|---|
| C1.0 | COVER SHEET |
| C1.1 | OVERALL SITE PLAN |
| C1.2 | ENLARGED SITE PLAN |
| C1.3 | SITE DETAILS |
| C1.4 | OVERALL GRADING PLAN |
| C1.5 | ENLARGED GRADING PLAN |
| C1.6 | UTILITY PLAN |
| C1.7 | UTILITY PROFILE |
| C1.8 | UTILITY DETAILS |
| C1.9 | UTILITY DETAILS |
| C1.10 | PRE DRAINAGE MAP |
| C1.11 | POST DRAINAGE MAP |
| C1.12 | LANDSCAPE PLAN |
| C1.13 | STORM WATER POLLUTION PREVENTION PLAN |


# NEW BEGINNINGS

HIGHWAY 5
BRYANT, AR

## GENERAL CONSTRUCTION NOTES

A. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGES OCCURRING TO ANY PROPERTY DURING THE CONSTRUCTION OF THIS PROJECT. SAID CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT PROPERTY DAMAGE.

B. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL SOLELY AND COMPLETELY BE RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND WILL NOT BE LIMITED TO NORMAL WORKING HOURS.

C. THE DUTY OF THE LOCAL UTILITY PROVIDER TO CONDUCT CONSTRUCTION INSPECTION REVIEWS OF THE CONTRACTOR'S PERFORMANCE IS NOT AN INSPECTION OR REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES IN, ON, OR NEAR THE CONSTRUCTION SITE.

D. ALL WATER AND SEWER IMPROVEMENTS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE LATEST REVISION TO THE LOCAL PROVIDER'S WATER AND WASTEWATER (SANITARY SEWER) STANDARD SPECIFICATIONS.

E. THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF ALL UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLAN.

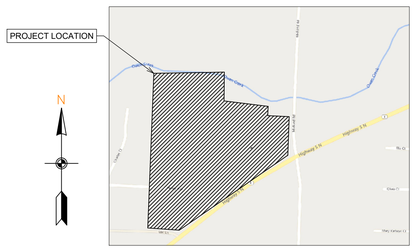
F. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH, AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.

G. PRIOR TO INSTALLATION OF ANY UTILITIES, THE CONTRACTOR IS TO EXCAVATE, VERIFY AND CALCULATE ALL CROSSINGS AND INFORM ANY AND ALL UTILITIES OF ANY CONFLICTS PRIOR TO CONSTRUCTION.

H. CONSTRUCTION SHALL NOT START ON ANY WATER UTILITY TIE-INS UNTIL APPROVAL IS GIVEN BY THE LOCAL UTILITY PROVIDER. SAID CONTRACTOR SHALL NOT OPERATE ANY VALVE, HYDRANT, OR WATER UTILITY APPURTENANCE NOR SHALL HE ATTACH TO OR TAP ANY WATER UTILITY MAIN WITHOUT APPROVAL. THE CONTRACTOR SHALL BEAR THE COST AND CONSEQUENCE OF ANY DISRUPTION OF UTILITY OPERATION CAUSED BY CONSTRUCTION.

I. FIBER OPTIC CABLE ON AND/OR ADJACENT TO THIS SITE WERE NOT LOCATED BY THE SURVEY AND ARE NOT SHOWN. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ANY FIBER OPTIC CABLES ASSOCIATED WITH THIS SITE AND TAKE ALL NECESSARY AND REQUIRED PRECAUTIONS TO PROTECT ANY EXISTING FIBER OPTIC CABLES. CONTRACTORS SHALL COORDINATE ALL EFFORTS WITH OWNER OF FIBER OPTIC CABLES OR THEIR DESIGNATED REPRESENTATIVE.

J. THE CONTRACTOR IS RESPONSIBLE FOR CONTACTING "ONECALL" SERVICE TO MARK ALL UTILITIES PRIOR TO ANY DEMOLITION, EARTHWORK, OR UTILITY WORK ON THIS SITE.




Vicinity Map
SCALE 1" = 500'

Know what's **below.**
**Call** before you dig.

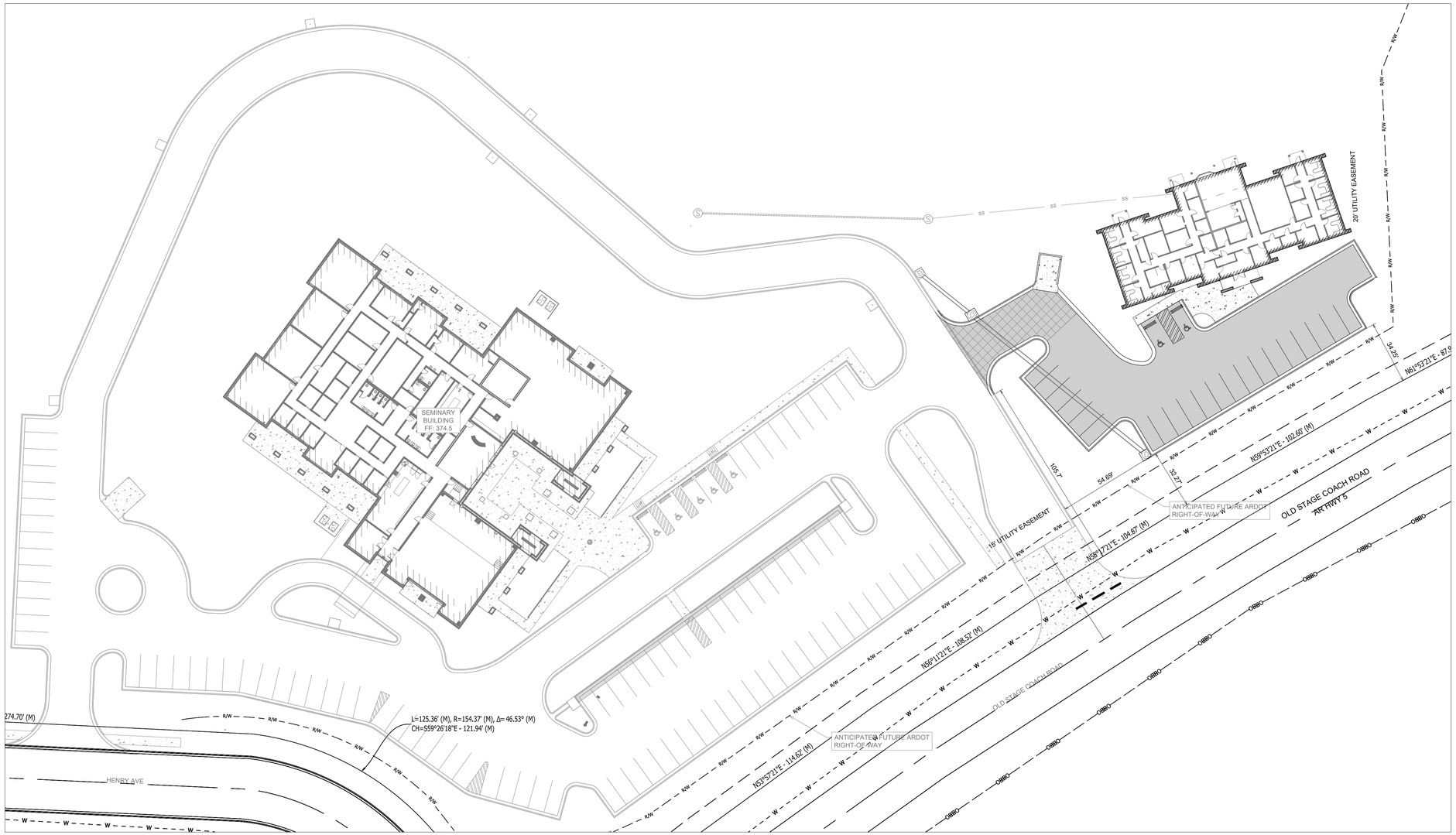
DEVIATIONS/VARIANCES

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS


PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants

23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840




# OVERALL SITE PLAN

SCALE 1" = 30'

## GENERAL CONSTRUCTION NOTES

A. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGES OCCURRING TO ANY PROPERTY DURING THE CONSTRUCTION OF THIS PROJECT. SAID CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT PROPERTY DAMAGE.

B. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL SOLELY AND COMPLETELY BE RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND WILL NOT BE LIMITED TO NORMAL WORKING HOURS.

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C. ALL WATER AND SEWER IMPROVEMENTS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE LATEST REVISION TO THE CITY OF BRYANT'S WATER AND WASTEWATER (SANITARY SEWER) STANDARD SPECIFICATIONS.

D. THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF ALL UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLAN.

E. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH, AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.

F. PRIOR TO INSTALLATION OF ANY UTILITIES, THE CONTRACTOR IS TO EXCAVATE, VERIFY AND CALCULATE ALL CROSSINGS AND INFORM ANY AND ALL UTILITIES OF ANY CONFLICTS PRIOR TO CONSTRUCTION.

G. CONSTRUCTION SHALL NOT START ON ANY WATER UTILITY TIE-INS UNTIL APPROVAL IS GIVEN BY BRYANT WATER. SAID CONTRACTOR SHALL NOT OPERATE ANY VALVE, HYDRANT, OR WATER UTILITY APPURTENANCE NOR SHALL HE ATTACH TO OR TAP ANY WATER UTILITY MAIN WITHOUT APPROVAL. THE CONTRACTOR SHALL BEAR THE COST AND CONSEQUENCE OF ANY DISRUPTION OF UTILITY OPERATION CAUSED BY CONSTRUCTION.

H. FIBER OPTIC CABLE ON AND/OR ADJACENT TO THIS SITE WERE NOT LOCATED BY THE SURVEY AND ARE NOT SHOWN. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ANY FIBER OPTIC CABLES ASSOCIATED WITH THIS SITE AND TAKE ALL NECESSARY AND REQUIRED PRECAUTIONS TO PROTECT ANY EXISTING FIBER OPTIC CABLES. CONTRACTORS SHALL COORDINATE ALL EFFORTS WITH OWNER OF FIBER OPTIC CABLES OR THEIR DESIGNATED REPRESENTATIVE.

J. THE CONTRACTOR IS RESPONSIBLE FOR CONTACTING "ONECALL" SERVICE TO MARK ALL UTILITIES PRIOR TO ANY DEMOLITION, EARTHWORK, OR UTILITY WORK ON THIS SITE.

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

N

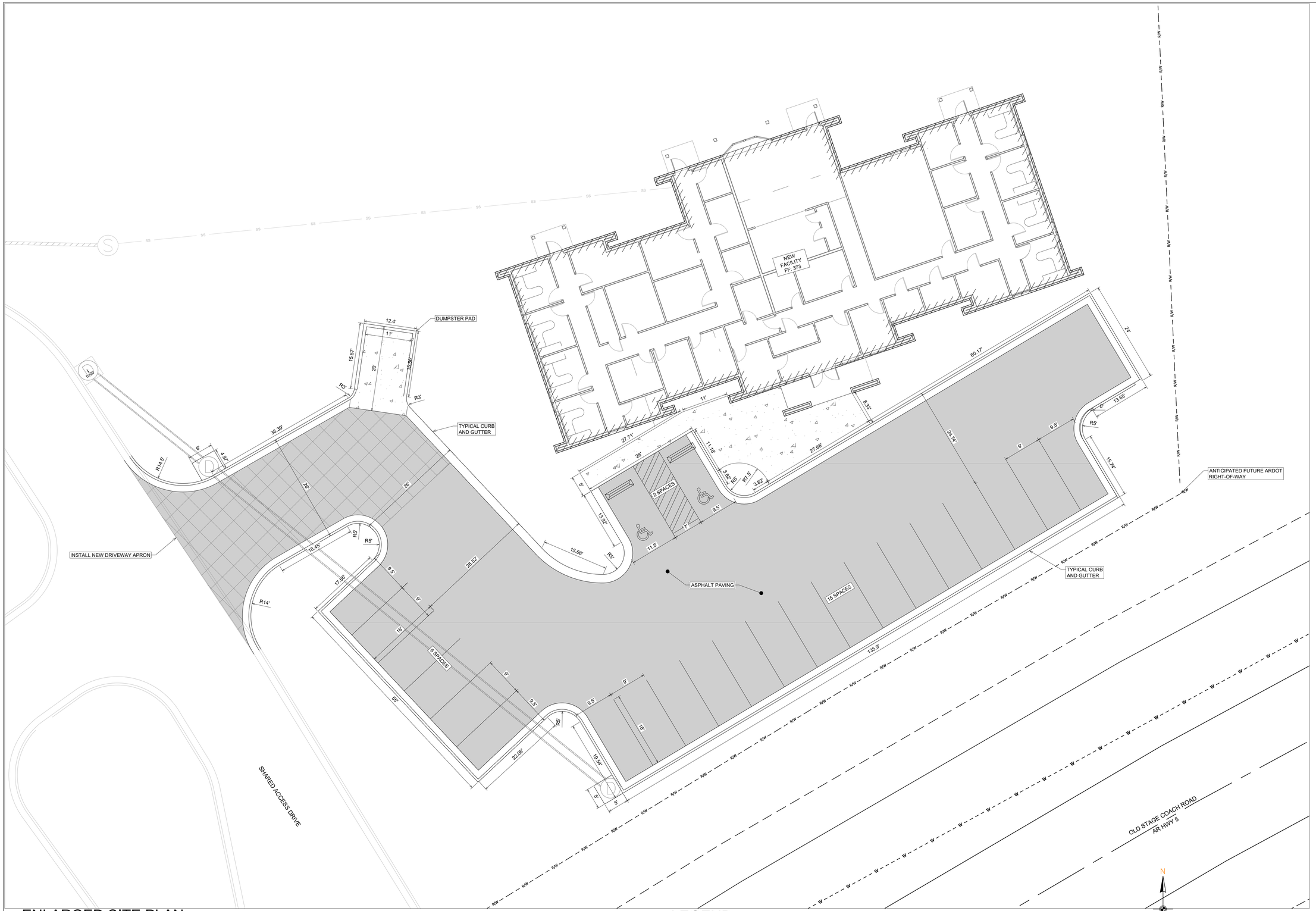
0 30'
1" = 30'-0"

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
OVERALL SITE PLAN

SHEET NUMBER:
C1.1




# ENLARGED SITE PLAN

SCALE 1" = 10'

1. TOTAL NEW DEVELOPMENT AREA = (+/-) 1.8 ACRES
2. PROPERTY IS ZONED C-2
3. 23 PARKING SPACES PROVIDED INCLUDING 2 ADA ACCESSIBLE PARKING SPACES
4. ALL DIMENSIONS ARE TO THE BACK OF CURB AND/OR EDGE OF PAVEMENT
5. DAMAGE TO PUBLIC AND PRIVATE PROPERTY DUE TO HAULING OPERATIONS OR OPERATIONS OF CONSTRUCTION RELATED EQUIPMENT FROM A CONSTRUCTION SITE SHALL BE REPAIRED BY THE THE RESPONSIBLE PARTY PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY.
6. REPAIR, REPLACE, OR EXTEND EXISTING DAMAGED OR MISSING CURB AND GUTTER, SIDEWALK OR RAMPS WITHIN THE PUBLIC RIGHT OF WAY.
7. ALL SIGNAGE, PAVEMENT MARKING AND PARKING LOT STRIPING SHALL CONFORM TO REQUIREMENTS GIVEN IN MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD). MUTCD REQUIRES THAT PARKING SPACES BE MARKED IN WHITE.

# LEGEND

- LIGHT DUTY HMAC ASPHALT SURFACE COURSE
- MEDIUM DUTY HMAC ASPHALT SURFACE COURSE

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGININGS**
HIGHWAY 5
BRYANT, ARKANSAS

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP LEWIS

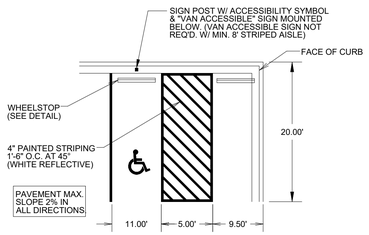
CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS-ENGINEER

PROJECT NUMBER:

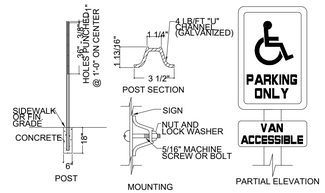
SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
ENLARGED SITE PLAN

SHEET NUMBER:
C1.2



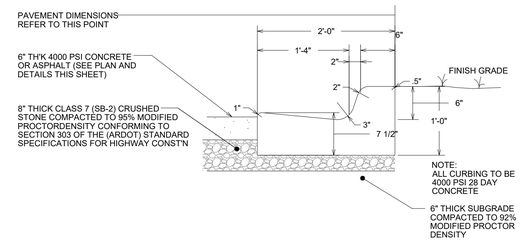

## TYPICAL ACCESSIBLE PARKING STALLS




## HANDICAP SIGN DETAIL

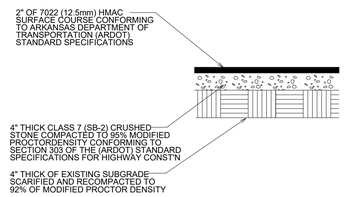
NOT TO SCALE

NOTE:
HANDICAP SIGNAGE SHALL BE IN STRICT COMPLIANCE WITH CURRENT FEDERAL AND LOCAL LAW REQUIREMENTS



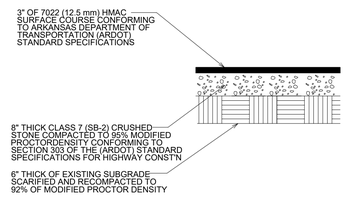

## 2'-0" CONCRETE CURB & GUTTER

NOT TO SCALE



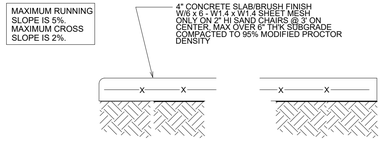

## LIGHT DUTY HMAC ASPHALT SURFACE COURSE

NOT TO SCALE




## MEDIUM DUTY HMAC ASPHALT SURFACE COURSE

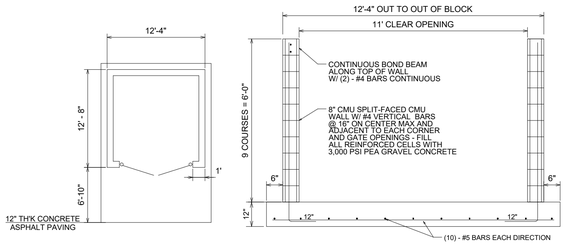
NOT TO SCALE




## CONCRETE WALK SECTION

NOT TO SCALE

NOTE:
ALL SIDEWALK JOINTS TO BE STEEL TROWELED. ALL JOINT EDGES AND SHALL BE SPACED AT 5 FEET ON CENTER MAXIMUM IN ALL DIRECTIONS AND SHALLBE STEEL TROWELED ON A RADIUS NOT TO EXCEED ONE-HALF INCH.




## DUMPSTER PAD/ENCLOSURE DETAIL

NOT TO SCALE

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION — PHILLIP LEWIS ENGINEERING, INC. — No. 566 — ARKANSAS ENGINEER

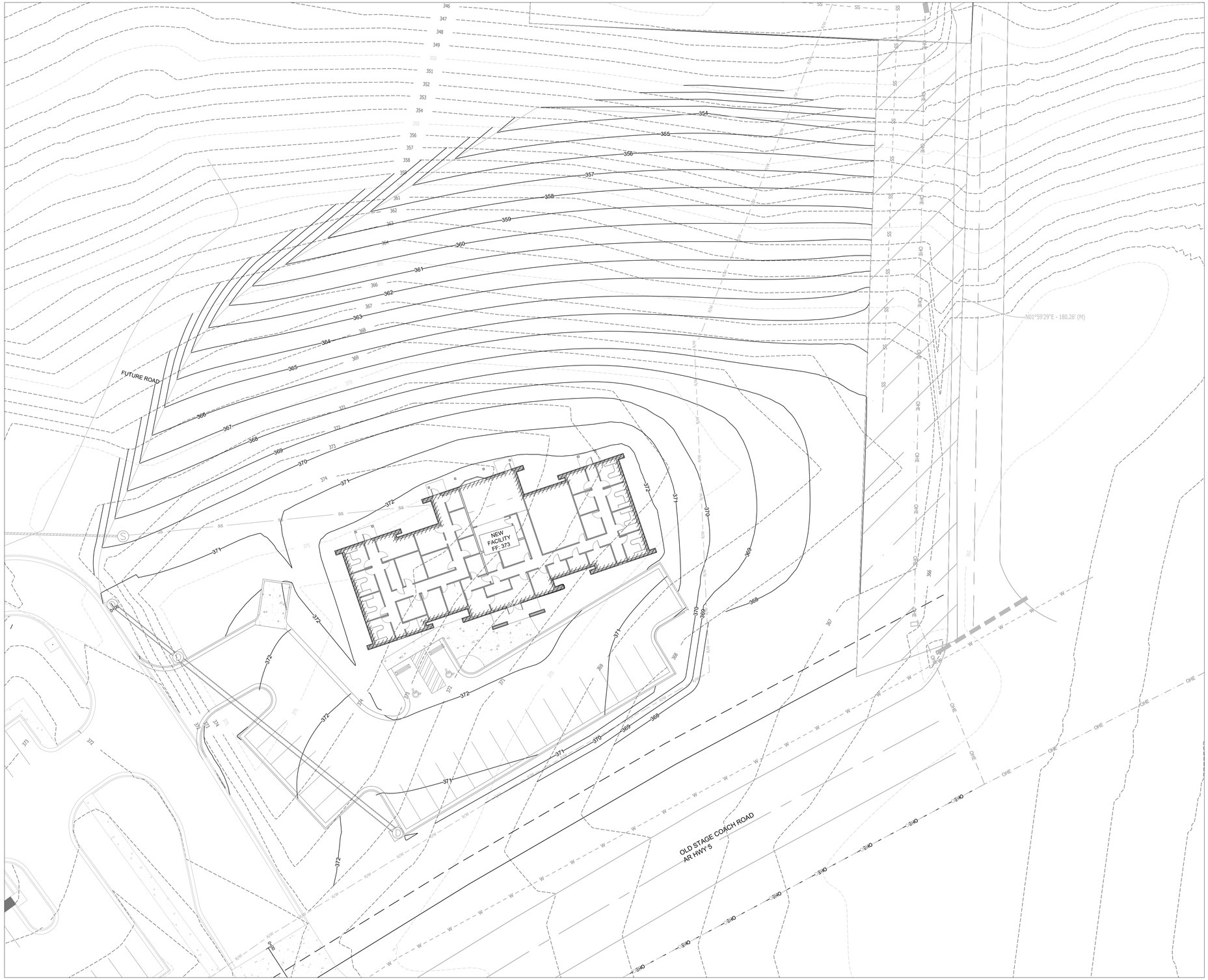
STATE OF ARKANSAS — REGISTERED PROFESSIONAL ENGINEER — No. 9540 — PHILLIP A. LEWIS

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
SITE DETAILS

SHEET NUMBER:
C1.3




OVERALL GRADING PLAN

SCALE 1" = 10'

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

PROJECT NUMBER:

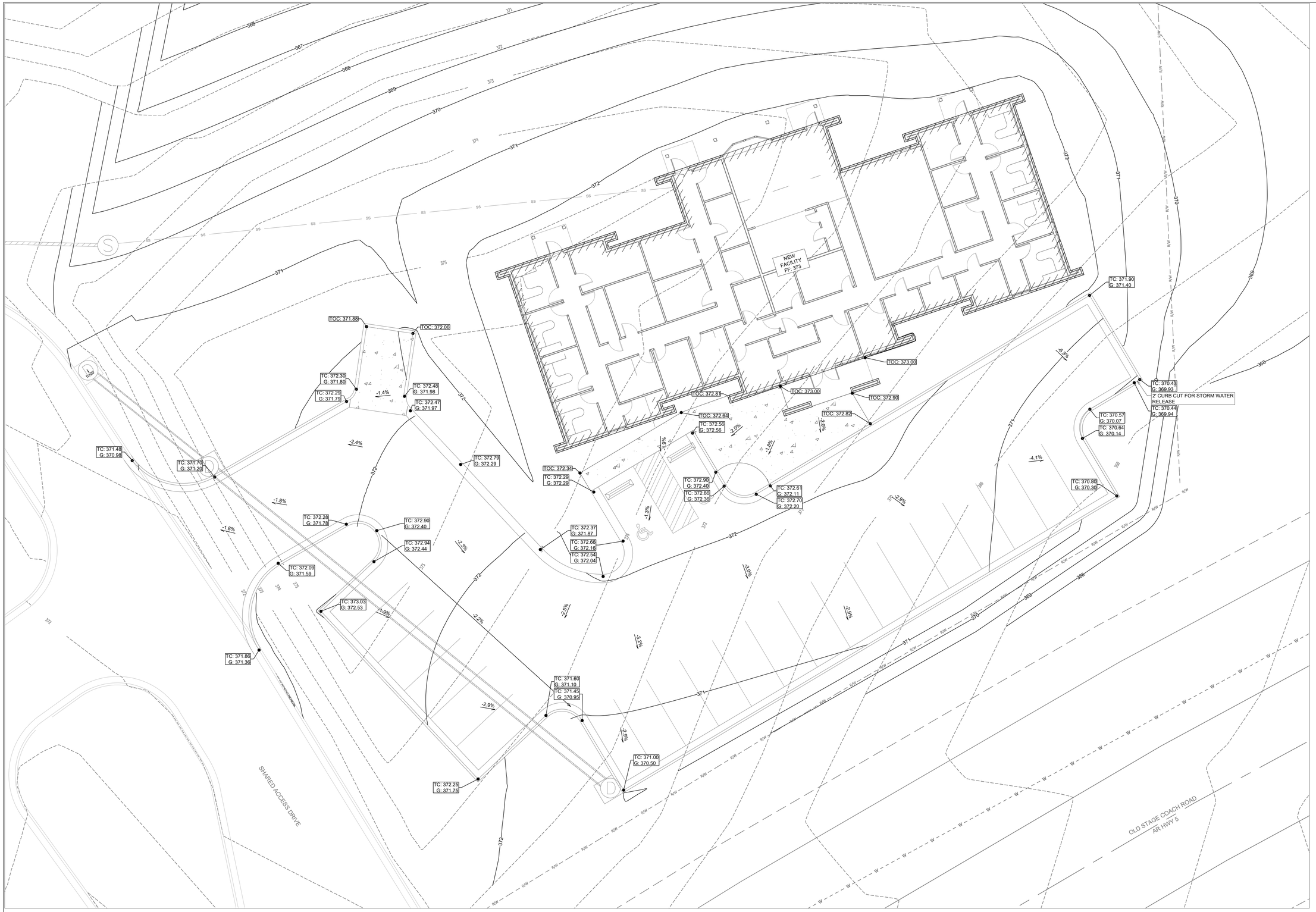
SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
OVERALL GRADING PLAN

SHEET NUMBER:
C1.4

N

0 10'
1" = 10'-0"




# ENLARGED GRADING PLAN

SCALE 1" = 10'

| |
|---|
| TC = TOP OF CURB ELEVATION |
| G = GUTTER ELEVATION |
| TOC = TOP OF CONCRETE ELEVATION |
| FG = FINAL GRADE ELEVATION |
| TP = TOP OF PAVEMENT ELEVATION |
| EG = EXISTING GRADE ELEVATION |

N

0 10'

1" = 10'-0"

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGININGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
ARKANSAS-ENGINEER
No. 566

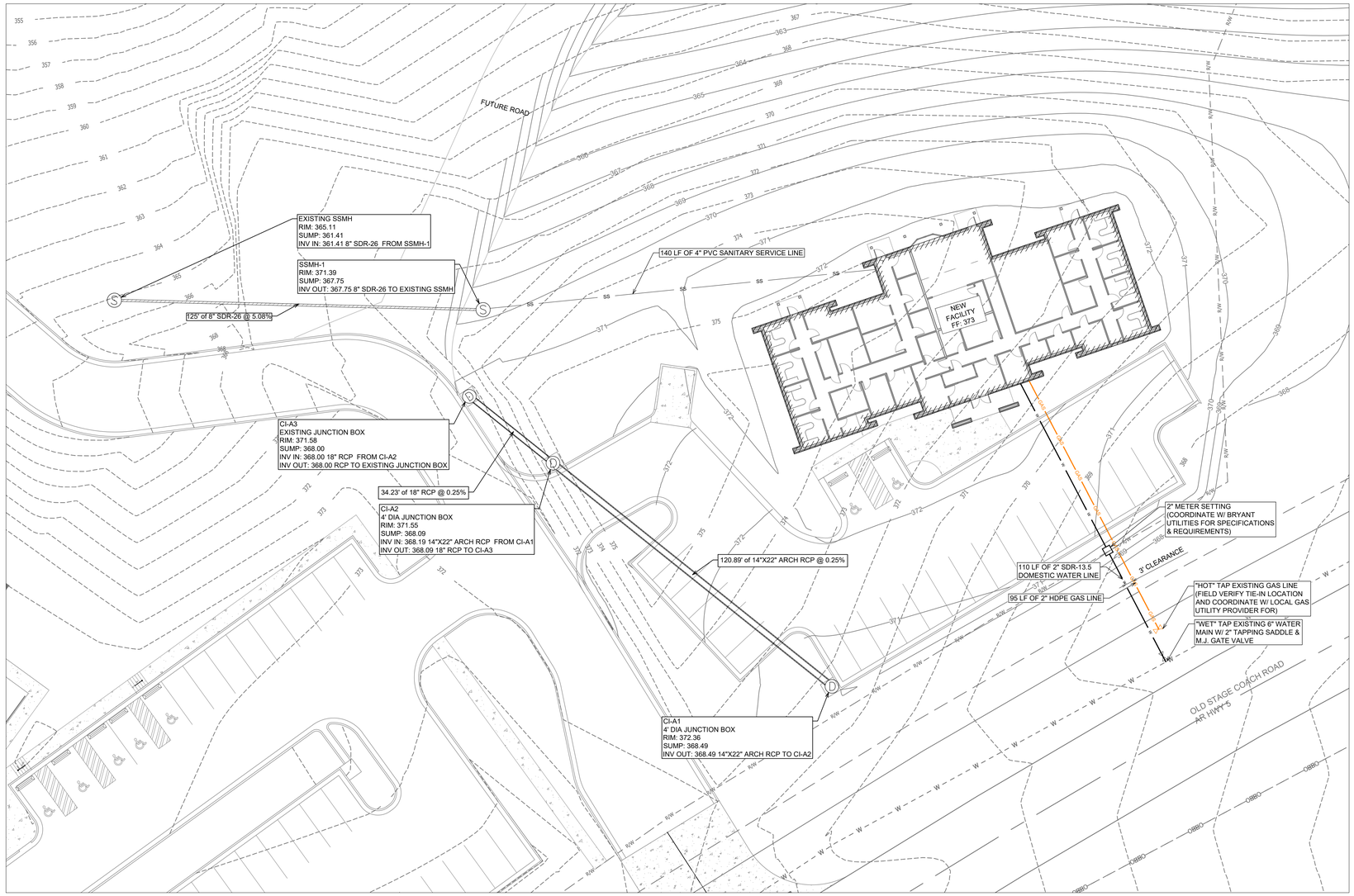
STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
ENLARGED GRADING PLAN

SHEET NUMBER:
C1.5




# UTILITY PLAN

SCALE 1" = 20'

## GENERAL CONSTRUCTION NOTES

A. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGES OCCURRING TO ANY PROPERTY DURING THE CONSTRUCTION OF THIS PROJECT. SAID CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT PROPERTY DAMAGE.

B. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL SOLELY AND COMPLETELY BE RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND WILL NOT BE LIMITED TO NORMAL WORKING HOURS.

THE DUTY OF BRYANT TO CONDUCT CONSTRUCTION INSPECTION REVIEWS OF THE CONTRACTOR'S PERFORMANCE IS NOT AN INSPECTION OR REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES IN, ON, OR NEAR THE CONSTRUCTION SITE.

C. ALL WATER AND SEWER IMPROVEMENTS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE LATEST REVISION TO THE CITY OF BRYANT'S WATER AND WASTEWATER (SANITARY SEWER) STANDARD SPECIFICATIONS.

D. THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF ALL UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLAN.

E. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH, AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.

F. PRIOR TO INSTALLATION OF ANY UTILITIES, THE CONTRACTOR IS TO EXCAVATE, VERIFY AND CALCULATE ALL CROSSINGS AND INFORM ANY AND ALL UTILITIES OF ANY CONFLICTS PRIOR TO CONSTRUCTION.

G. CONSTRUCTION SHALL NOT START ON ANY WATER UTILITY TIE-INS UNTIL APPROVAL IS GIVEN BY BRYANT WATER. SAID CONTRACTOR SHALL NOT OPERATE ANY VALVE, HYDRANT, OR WATER UTILITY APPURTENANCE NOR SHALL HE ATTACH TO OR TAP ANY WATER UTILITY MAIN WITHOUT APPROVAL. THE CONTRACTOR SHALL BEAR THE COST AND CONSEQUENCE OF ANY DISRUPTION OF UTILITY OPERATION CAUSED BY CONSTRUCTION.

H. FIBER OPTIC CABLE ON AND/OR ADJACENT TO THIS SITE WERE NOT LOCATED BY THE SURVEY AND ARE NOT SHOWN. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ANY FIBER OPTIC CABLES ASSOCIATED WITH THIS SITE AND TAKE ALL NECESSARY AND REQUIRED PRECAUTIONS TO PROTECT ANY EXISTING FIBER OPTIC CABLES. CONTRACTORS SHALL COORDINATE ALL EFFORTS WITH OWNER OF FIBER OPTIC CABLES OR THEIR DESIGNATED REPRESENTATIVE.

J. THE CONTRACTOR IS RESPONSIBLE FOR CONTACTING "ONECALL" SERVICE TO MARK ALL UTILITIES PRIOR TO ANY DEMOLITION, EARTHWORK, OR UTILITY WORK ON THIS SITE.

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGININGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
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No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP W. LEWIS

Know what's **below.**
**Call** before you dig.

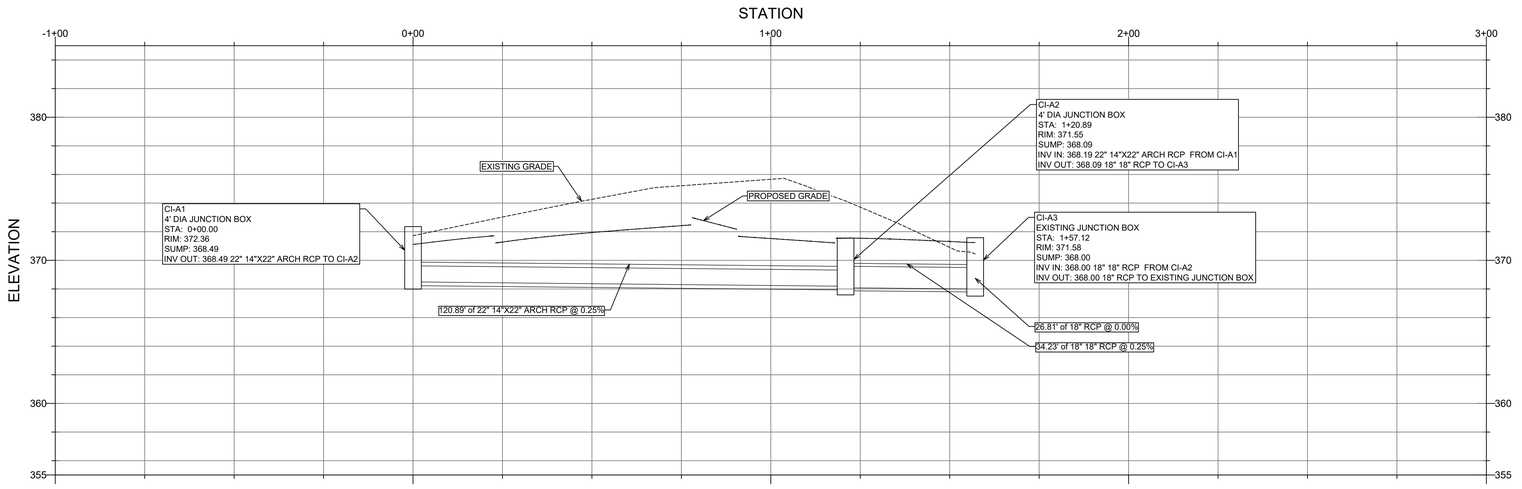
PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

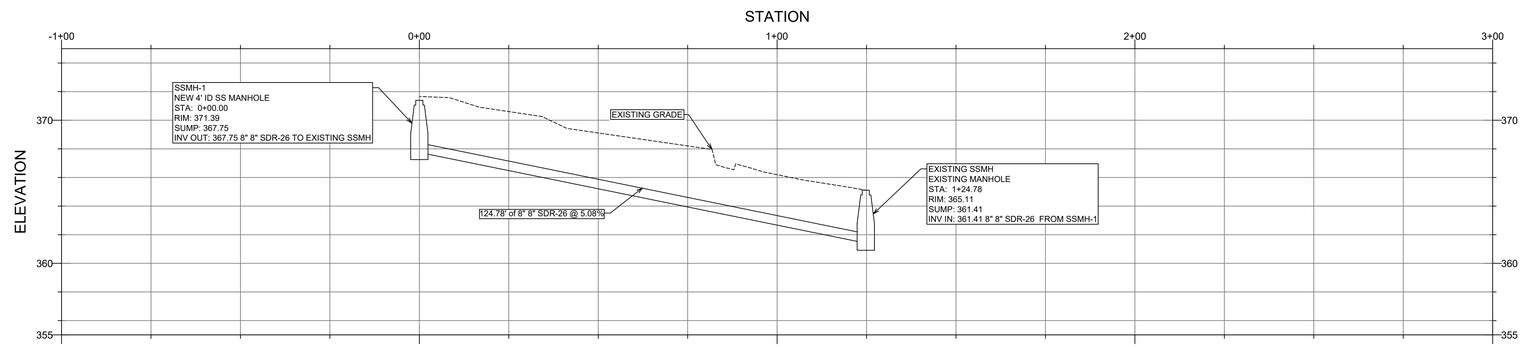
PAGE TITLE:
UTILITY PLAN

SHEET NUMBER:
C1.6

# STORM SEWER




# SANITARY SEWER




PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINGS**
HIGHWAY 5
BRYANT, ARKANSAS

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PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

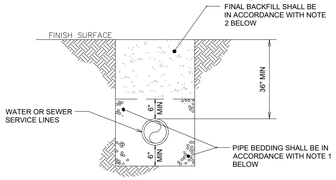
STATE OF ARKANSAS
PHILLIP A. LEWIS
REGISTERED PROFESSIONAL ENGINEER
No. 9540

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

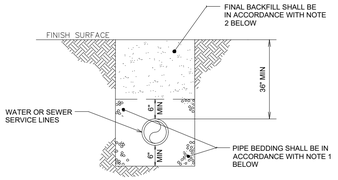
PAGE TITLE:
UTILITY PROFILES

SHEET NUMBER:
C1.7



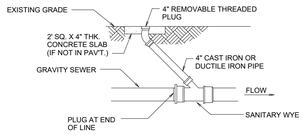

## GAS LINE BEDDING DETAIL

NOT TO SCALE



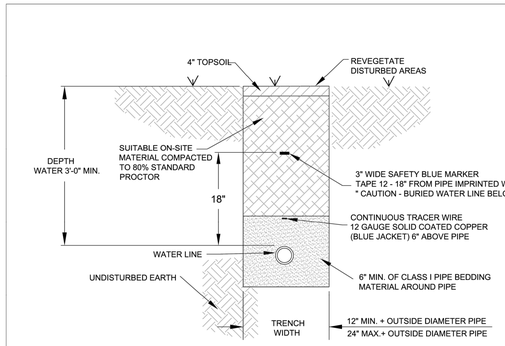

## WATER AND SEWER LINES BEDDING DETAIL

NOT TO SCALE




## THROUGH FLOW CLEANOUT

NOT TO SCALE




NOTES:

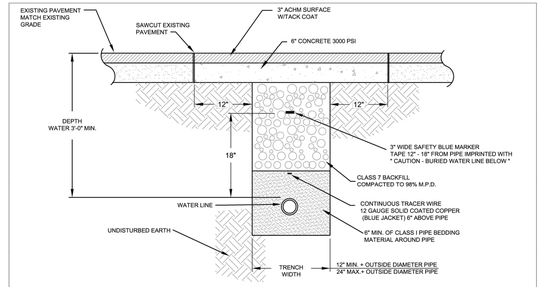
1. ALL VALVES, BENDS, ETC. SHALL BE RESTRAINED.
2. THE CONTRACTOR SHALL PROVIDE ALL ITEMS NECESSARY TO CONNECT WITH ANY PART OF THE EXISTING WATER SYSTEM THAT WILL REMAIN IN ORDER TO ESTABLISH A SATISFACTORY AND ACCEPTABLE WATER SYSTEM.
3. CONTRACTOR TO CONSTRUCT ALL TRENCH EXCAVATION IN ACCORDANCE WITH ALL OSHA REGULATIONS (29 CFR CH.XVII, SUBPART B)
4. TRENCH SHALL BE EXCAVATED BELOW GRADE REQUIRED TO PROVIDE A MINIMUM 36" OF PIPE COVER.
5. MAXIMUM PIPE COVER SHALL BE 60" UNDER NORMAL CONDITIONS. COVER GREATER THAN 60" MAY BE ALLOWED FOR SHORT DISTANCES WHERE REQUIRED BY FIELD CONDITIONS. NO HYDRANT SHALL BE ALLOWED WHERE LINES ARE GREATER THAN 60" DEEP.

## WATER MAIN TRENCH

(NON-PAVED AREA)

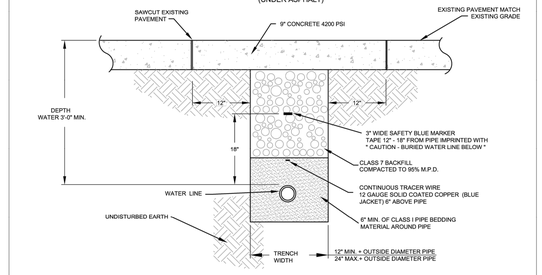
CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | WATER MAIN TRENCH (NON-PAVED AREA) | REVISED ----- ----- ----- ----- ----- | W1 |
| DRAWN BY: | CHECKED BY: | FILE: W1-Water Trench (Non-Paved Area).dwg | |




## WATER MAIN TRENCH

(UNDER ASPHALT)




## WATER MAIN TRENCH

(UNDER CONCRETE)

NOTES:

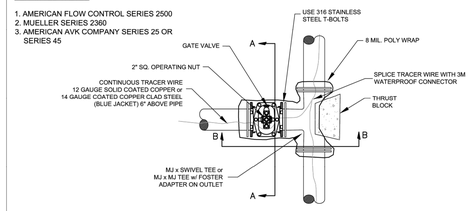
1. ALL VALVES, BENDS, ETC. SHALL BE RESTRAINED.
2. THE CONTRACTOR SHALL PROVIDE ALL ITEMS NECESSARY TO CONNECT WITH ANY PART OF THE EXISTING WATER SYSTEM THAT WILL REMAIN IN ORDER TO ESTABLISH A SATISFACTORY AND ACCEPTABLE WATER SYSTEM.
3. CONTRACTOR TO CONSTRUCT ALL TRENCH EXCAVATION IN ACCORDANCE WITH ALL OSHA REGULATIONS (29 CFR CH.XVII, SUBPART B)
4. TRENCH SHALL BE EXCAVATED BELOW GRADE REQUIRED TO PROVIDE A MINIMUM 36" OF PIPE COVER.
5. MAXIMUM PIPE COVER SHALL BE 60" UNDER NORMAL CONDITIONS. COVER GREATER THAN 60" MAY BE ALLOWED FOR SHORT DISTANCES WHERE REQUIRED BY FIELD CONDITIONS. NO HYDRANT SHALL BE ALLOWED WHERE LINES ARE GREATER THAN 60" DEEP.

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

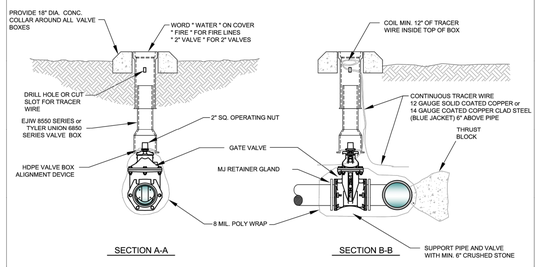
| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | WATER MAIN TRENCH (UNDER PAVEMENT) | REVISED ----- ----- ----- ----- ----- | W2 |
| DRAWN BY: | CHECKED BY: | FILE: W2-Water Trench (Under Pavement).dwg | |

PERMITTED VALVES

1. AMERICAN FLOW CONTROL SERIES 2500
2. MUELLER SERIES 2360
3. AMERICAN AVK COMPANY SERIES 25 OR SERIES 45




PLAN




NOTES:

1. ALL VALVES SHALL BE SECURELY ANCHORED TO THE TEE.
2. ALL HARDWARE SHALL BE 316 STAINLESS STEEL.
3. IF DEPTH OF BURY EXCEEDS 4 FT., A VALVE STEM EXTENSION SHALL BE REQUIRED. THE VALVE STEM EXTENSION NUT SHALL BE WITHIN 24-INCHES TO 12-INCHES OF THE FINISHED SURFACE.

## GATE VALVE DETAIL

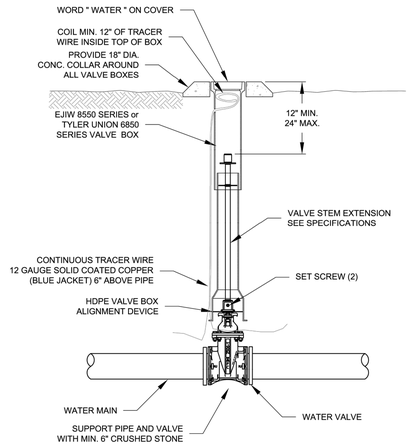
2" - 12"

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | GATE VALVE | REVISED ----- ----- ----- ----- ----- | W4 |
| DRAWN BY: | CHECKED BY: | FILE: W4-Gate Valve.dwg | |

NOTES:

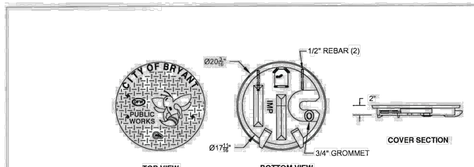
1. OPERATING NUT EXTENSIONS SHALL BE USED WHEN THE TOP OF THE OPERATING NUT IS GREATER THAN 4 FEET FROM THE TOP OF FINISHED SURFACE.
2. THE STEM EXTENSION SHALL BE OF ADEQUATE LENGTH TO REACH FROM THE VALVE OPERATING NUT TO A POINT WITHIN 24-INCHES TO 12-INCHES OF THE FINISHED SURFACE.



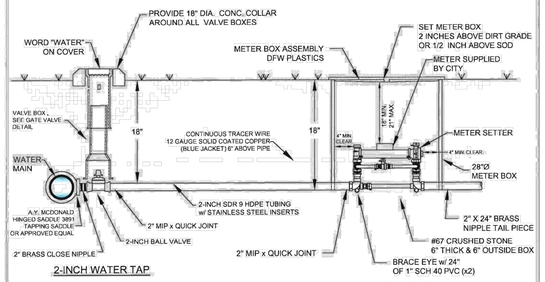

## VALVE WITH STEM EXTENSION

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | VALVE STEM EXTENSION | REVISED ----- ----- ----- ----- ----- | W7 |
| DRAWN BY: | CHECKED BY: | FILE: W7-Valve Stem Extension.dwg | |




## WATER METER LID




2-INCH WATER TAP

2-INCH METER SETTER

NOTES:

1. COORDINATE INSTALLATION AND CONFIGURATIONOF ALL 1-1/2" AND LARGER METER SETTINGS WITH THE CITY.
2. ALL METER BOXES SHALL BE INSTALLED IN NON-PAVED AREAS. ANY METER BOX THAT GETS PLACED IN A PAVED AREA SHALL BE RELOCATED AT THE OWNER'S EXPENSE BEFORE A WATER METER WILL BE INSTALLED.
3. SUPPORT METER INSTALLATION WITH 1"x24" SCH40 PVC THROUGH EACH BRACE EYE.

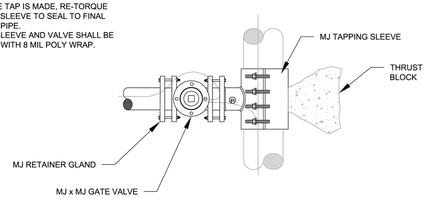
## 2" WATER SERVICE AND WATER METER

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

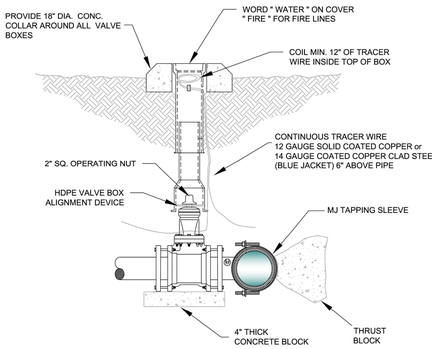
| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | 2" WATER METER | REVISED ----- ----- ----- ----- ----- | W12 |
| DRAWN BY: | CHECKED BY: | FILE: W12-2 Inch Water Meter.dwg | |

NOTES:

1. TAPPING SLEEVE SHALL BE SMITH-BLAIR 662 OR FORD FAST.
2. AFTER THE TAP IS MADE, RE-TORQUE BOLTS ON SLEEVE TO SEAL TO FINAL SHAPE OF PIPE.
3. TAPPING SLEEVE AND VALVE SHALL BE WRAPPED WITH 8 MIL POLY WRAP.



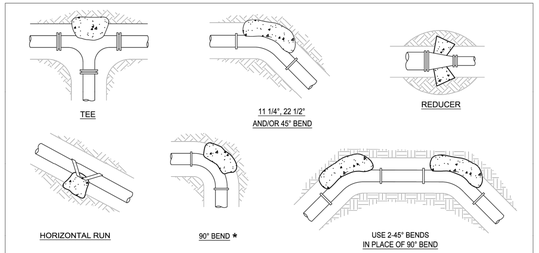

PLAN VIEW

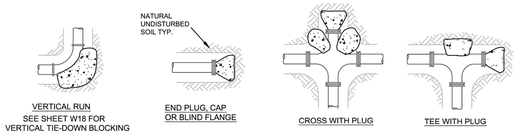



PROFILE VIEW

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | TAPPING SLEEVE AND VALVE | REVISED ----- ----- ----- ----- ----- | W13 |
| DRAWN BY: | CHECKED BY: | FILE: W13-Tapping Sleeve and Valve.dwg | |




SEE SHEET W18 FOR VERTICAL TIE-DOWN BLOCKING

THRUST BLOCK SCHEDULE

(2000 PSF SOIL, 200 PSI WATER PRESSURE, 100 PSI WATER HAMMER)

| BEARING AREA OF THRUST BLOCKS IN SQ. FT. (HORIZONTAL BENDS) | | | | | | VOLUME OF THRUST BLOCK IN CU. FEET (VERTICAL BENDS) | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| FITTING SIZE | PLUG TEE OR CAP | BEND ANGLE 90° | 45° | 22 1/2° | 11 1/4° | FITTING SIZE | BEND ANGLE 90° | 45° | 22 1/2° | 11 1/4° | ROD DIAM. | EMBED MENT |
| 2, 3 & 4 | 1.9 | 2.7 | 1.4 | 0.7 | 0.4 | 2, 3 & 4 | 35.5 | 19.2 | 9.9 | 4.9 | 50" | 30" |
| 6 | 5.6 | 7.9 | 4.3 | 2.2 | 1.1 | 6 | 105.8 | 57.2 | 29.2 | 14.7 | 75" | 30" |
| 8 | 9.6 | 13.6 | 7.4 | 3.8 | 1.9 | 8 | 181.9 | 98.5 | 50.2 | 25.2 | 75" | 30" |
| 12 | 20.5 | 29.0 | 15.7 | 8.0 | 4.0 | 12 | 387.1 | 209.5 | 106.8 | 53.7 | 1.0" | 30" |
| 16 | 35.7 | 50.4 | 27.3 | 13.9 | 7.0 | 16 | 672.6 | 364.0 | 185.6 | 93.2 | 1.0" | 36" |
| 18 | 44.8 | 63.4 | 34.3 | 17.5 | 18.8 | 18 | 844.7 | 457.2 | 233.1 | 117.1 | 1.0" | 36" |
| 24 | 78.4 | 110.9 | 60.0 | 30.6 | 15.4 | 24 | 1478.7 | 800.3 | 408.0 | 205.0 | 1.5" | 36" |

★ 90 DEGREE BENDS SHALL ONLY BE USED ON A BY-EXCEPTION BASIS, AND MUST EACH BE SPECIFICALLY APPROVED BY CITY.

THRUST BLOCK NOTES:

1. CONCRETE FOR THRUST BLOCKS - CLASS A CONCRETE SHALL DEVELOP NOT LESS THAN 3000 P.S.I. COMPRESSIVE STRENGTH AT 28 DAYS AND BE PLACED AGAINST UNDISTURBED SOIL.
2. ALL BENDS, BOTH HORIZONTAL AND VERTICAL, SHALL BE BACKED WITH CONCRETE. VERTICAL BENDS SHALL BE PLACED ON CONCRETE PADS WHERE BENDS TURN UP, OR LOADED WHERE BENDS TURN DOWN.
3. WRAP PIPE JOINTS IN 8 MIL "POLYETHLENE" BEFORE PLACING CONCRETE.
4. BEARING AREA SHOWN IN TABLE IS BASED UPON A 2000 LBS/F SOIL BEARING, AND UPON A PIPELINE PRESSURE OF 200 psi. PLUS 100 psi. WATER HAMMER. AREAS SHOWN SHALL BE ADJUSTED, SHOULD FIELD CONDITIONS VARY.
5. MJ RESTRAINTS ARE REQUIRED FOR ALL FITTINGS.
6. USE LONG-RADIUS FITTINGS WHEREVER POSSIBLE.
7. ALL BOLTS FOR FITTINGS SHALL BE 316 STAINLESS STEEL.
8. ALL DUCTILE IRON FITTINGS SHALL BE FUSION-BONDED EPOXY COATED INSIDE AND OUTSIDE IN ACCORDANCE WITH ANSI/AWWA C116/A21.16.
9. UNIT WEIGHT OF CONCRETE FOR VERTICAL THRUST BLOCKS IS 150 LBS/CU. FT.

## THRUST BLOCKING

CITY OF BRYANT, AR
WATER UTILITIES
210 S.W. 3rd. STREET
BRYANT, AR
PHONE: (501) 943-0468

| TITLE: | WATER DETAILS | DATE: APRIL 2015 | SHEET: |
|---|---|---|---|
| DESCRIPTION: | THRUST BLOCKING | REVISED ----- ----- ----- ----- ----- | W16 |
| DRAWN BY: | CHECKED BY: | FILE: W16-Thrust Blocking.dwg | |

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

STATE OF ARKANSAS
PHILLIP A. LEWIS
REGISTERED PROFESSIONAL ENGINEER
No. 9540

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

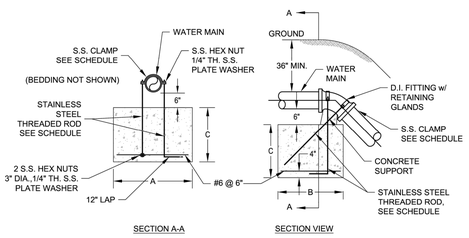
PAGE TITLE:
UTILITY DETAILS

SHEET NUMBER:
C1.8

| BLOCKING SCHEDULE | | | | | |
|---|---|---|---|---|---|
| PIPE SIZE | BENDS | 45° | 22 1/2° | 11 1/4° | ROD DIA. |
| 8" | VOLUME REQ'D (CU. FT.) | 98.5 | 50.2 | 25.2 | 3/4 IN. |
| | A (FT.) | 5.00' | 4.00' | 3.00' | |
| | B (FT.) | 4.00' | 3.20' | 2.80' | |
| | C (FT.) | 5.00' | 4.00' | 3.00' | |
| | MIN. CLAMP (2 EA.) | 5/8 IN. x 2 IN. | | | |
| 12" | VOLUME REQ'D (CU. FT.) | 209.5 | 106.8 | 53.7 | 3/4 IN. |
| | A (FT.) | 6.00' | 5.00' | 4.00' | |
| | B (FT.) | 6.00' | 4.25' | 3.50' | |
| | C (FT.) | 6.00' | 5.00' | 4.00' | |
| | MIN. CLAMP (2 EA.) | 1/2 IN. x 2 IN. | | | |
| 18" | VOLUME REQ'D (CU. FT.) | 457.2 | 233.1 | 117.1 | 1 IN. |
| | A (FT.) | 8.00' | 6.50' | 5.00' | |
| | B (FT.) | 7.25' | 5.50' | 4.75' | |
| | C (FT.) | 8.00' | 6.50' | 5.00' | |
| | MIN. CLAMP (2 EA.) | 5/8 IN. x 3 IN. | | | |
| 24" | VOLUME REQ'D (CU. FT.) | 800.3 | 408.0 | 205.0 | 1 1/4 IN. |
| | A (FT.) | 9.50' | 7.50' | 6.00' | |
| | B (FT.) | 9.00' | 7.25' | 5.75' | |
| | C (FT.) | 9.50' | 7.50' | 6.00' | |
| | MIN. CLAMP (2 EA.) | 5/8 IN. x 3 IN. | | | |

VOLUME CALCULATED ON THE BASIS OF CONCRETE REACTING THRUST ON THE RESPECTIVE BENDS UNDER AN INTERNAL PRESSURE OF 250 PSI, 50 PSI SURGE AND THE WEIGHT OF CONCRETE IS 150 POUNDS PER CU. FT.

ALL FITTINGS SHALL BE MECHANICAL JOINTS WITH RETAINING GLANDS. BEDDING NOT SHOWN

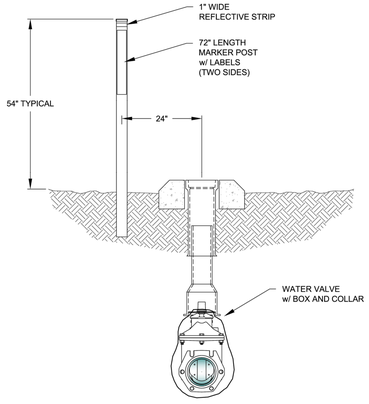



## VERTICAL TIE-DOWN BLOCKING



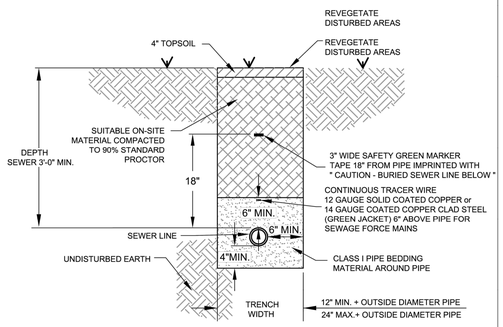
NOTES:

1. WATER LINE MARKERS SHALL BE TRI-VIEW MARKING SYSTEM BY RHINO MARKING AND PROTECTION SYSTEMS OR CARSONITE INTERNATIONAL DUAL-SIDED UTILITY MARKER (CIB-380).
2. THE UPPERMOST PORTION OF THE CARSONITE MARKER SHALL BE MADE OF VISIBILITY ENHANCER (CVE-360).
3. TRI-VIEW MARKERS DO NOT REQUIRE VISIBILITY ENHANCERS.
4. AN ADDITIONAL WHITE 1" WIDE REFLECTIVE TAPE (3M OR EQUAL) SHALL BE PLACED AROUND THE FULL CIRCUMFERENCE OF THE TOP OF THE MARKER.




## VALVE MARKER





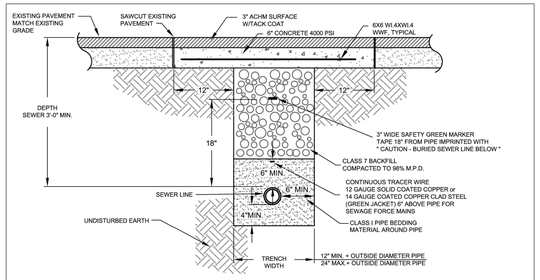

NOTES:

1. THE CONTRACTOR SHALL PROVIDE ALL ITEMS NECESSARY TO CONNECT WITH ANY PART OF THE EXISTING SEWER SYSTEM THAT WILL REMAIN IN ORDER TO ESTABLISH A SATISFACTORY AND ACCEPTABLE SEWER SYSTEM.
2. CONTRACTOR TO CONSTRUCT ALL TRENCH EXCAVATION IN ACCORDANCE WITH ALL OSHA REGULATIONS (29 CFR CH.XVII, SUBPART B)
3. TRENCH SHALL BE EXCAVATED BELOW GRADE REQUIRED TO PROVIDE A MINIMUM 36" OF PIPE COVER.

## SEWER TRENCH

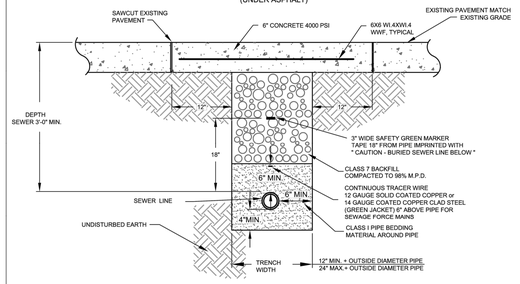
(NON-PAVED AREA)






## SEWER TRENCH

(UNDER ASPHALT)




## SEWER TRENCH

(UNDER CONCRETE)

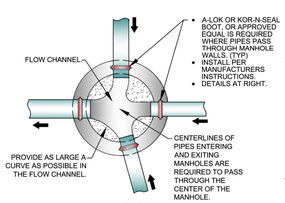
NOTES:

1. THE CONTRACTOR SHALL PROVIDE ALL ITEMS NECESSARY TO CONNECT WITH ANY PART OF THE EXISTING SEWER SYSTEM THAT WILL REMAIN IN ORDER TO ESTABLISH A SATISFACTORY AND ACCEPTABLE SEWER SYSTEM.
2. CONTRACTOR TO CONSTRUCT ALL TRENCH EXCAVATION IN ACCORDANCE WITH ALL OSHA REGULATIONS (29 CFR CH.XVII, SUBPART B)
3. TRENCH SHALL BE EXCAVATED BELOW GRADE REQUIRED TO PROVIDE A MINIMUM 36" OF PIPE COVER.

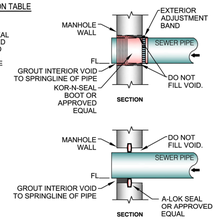


| Inside Diameter of Manhole | Minimum Wall Thickness | Base Thickness | Minimum Ring & Cover Size |
|---|---|---|---|
| 4' DIA | 5" | 6" | 24" (< or Equal to 24' Pipes) |
| 5' DIA | 7" | 8" | |
| 6' DIA | 7" | 8" | 36" (> 24' Pipes) |

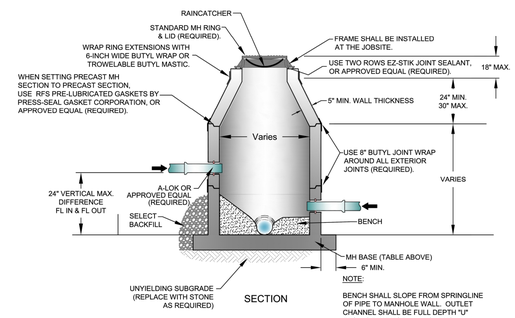
MANHOLE INFORMATION TABLE




MANHOLE FLOW CHANNEL




CONNECTION DETAILS



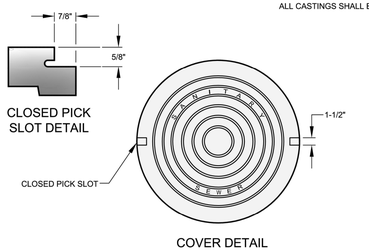

NOTE:

BENCH SHALL SLOPE FROM SPRINGLINE OF PIPE TO MANHOLE WALL. OUTLET CHANNEL SHALL BE FULL DEPTH "U" FROM CENTER OF MANHOLE TO WALL.

## PRECAST MANHOLE



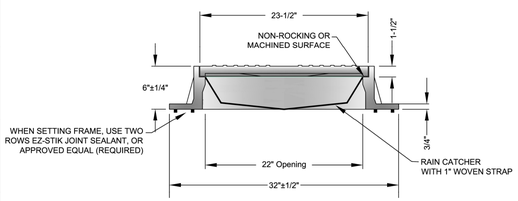
ALL CASTINGS SHALL BE "MADE IN USA"




COVER DETAIL

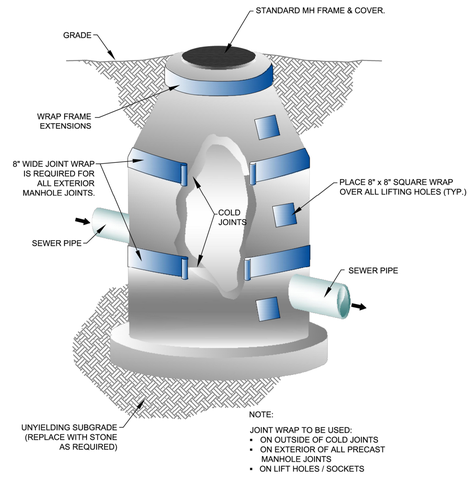
1. MINIMUM WEIGHT OF RING: 100 POUNDS
2. MINIMUM WEIGHT OF COVER: 110 POUNDS
3. COVERS ARE FURNISHED WITH TWO CLOSED PICK SLOTS.
4. CASTINGS SHALL BE "MADE IN USA"

* DIMENSIONAL TOLERANCES SHALL NOT EXCEED 1/16 INCH PER FOOT




## FRAME AND COVER DETAIL






NOTE:

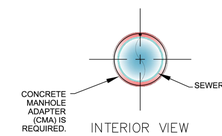
JOINT WRAP TO BE USED:

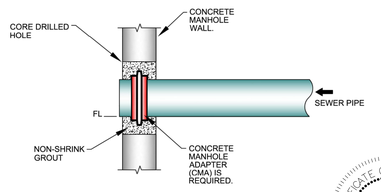
- ON OUTSIDE OF COLD JOINTS
- ON EXTERIOR OF ALL PRECAST MANHOLE JOINTS
- ON LIFT HOLES / SOCKETS

## MANHOLE JOINT WRAP



THE INSTALLATION SHALL BE DYE TESTED FOR ACCEPTANCE.




## MANHOLE CORING DETAILS




PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840


REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

STATE OF ARKANSAS — REGISTERED PROFESSIONAL ENGINEER — No. 9540 — PHILLIP LEWIS

CERTIFICATE OF AUTHORIZATION — PHILLIP LEWIS ENGINEERING, INC. — No. 566 — ARKANSAS ENGINEER

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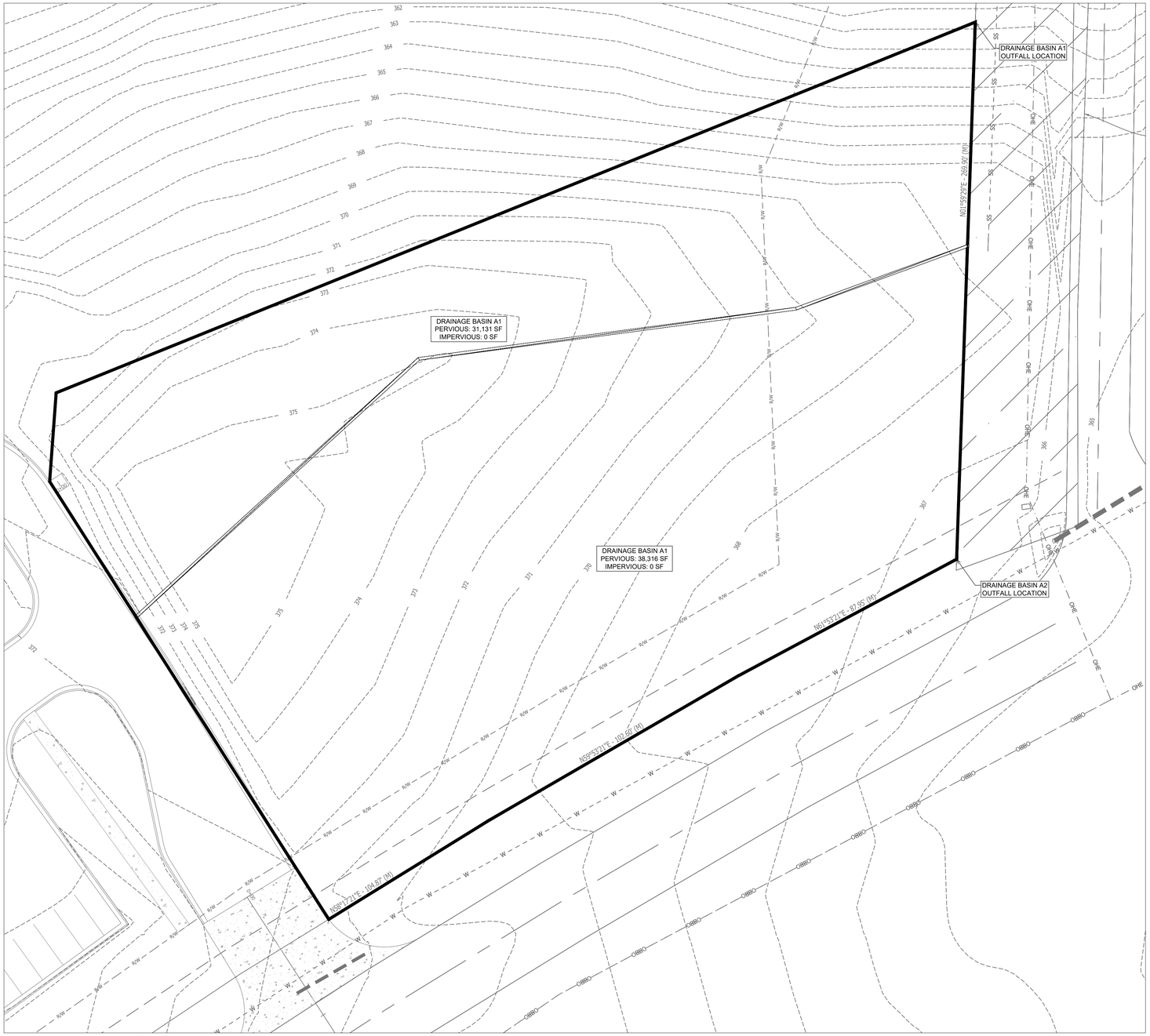


PRE-DEVELOPMENT DRAINAGE BASIN PLAN

SCALE 1" = 20'

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Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

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HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
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No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

N

0 20'

1" = 20'-0"

PROJECT NUMBER:

SHEET ISSUE DATE:
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PAGE TITLE:
PRE-DEV DRAINAGE

SHEET NUMBER:
C1.10

# POST-DEV DRAINAGE

SCALE 1" = 20'

## GENERAL SITE NOTES

1. TOTAL NEW DEVELOPMENT AREA = (+/-) 1.4 ACRES
2. PROPERTY IS ZONED C-2
3. 21 PARKING SPACES PROVIDED INCLUDING 2 ADA ACCESSIBLE PARKING SPACES
4. ALL DIMENSIONS ARE TO THE BACK OF CURB AND/OR EDGE OF PAVEMENT
5. DAMAGE TO PUBLIC AND PRIVATE PROPERTY DUE TO HAULING OPERATIONS OR OPERATIONS OF CONSTRUCTION RELATED EQUIPMENT FROM A CONSTRUCTION SITE SHALL BE REPAIRED BY THE THE RESPONSIBLE PARTY PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY.
6. REPAIR, REPLACE, OR EXTEND EXISTING DAMAGED OR MISSING CURB AND GUTTER, SIDEWALK OR RAMPS WITHIN THE PUBLIC RIGHT OF WAY.
7. ALL SIGNAGE, PAVEMENT MARKING AND PARKING LOT STRIPING SHALL CONFORM TO REQUIREMENTS GIVEN IN MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD). MUTCD REQUIRES THAT PARKING SPACES BE MARKED IN WHITE.

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ARKANSAS ENGINEERS

N

0 10'
1" = 10'-0"

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23620 Interstate 30 | Bryant, Arkansas
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BRYANT, ARKANSAS

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PHILLIP A. LEWIS

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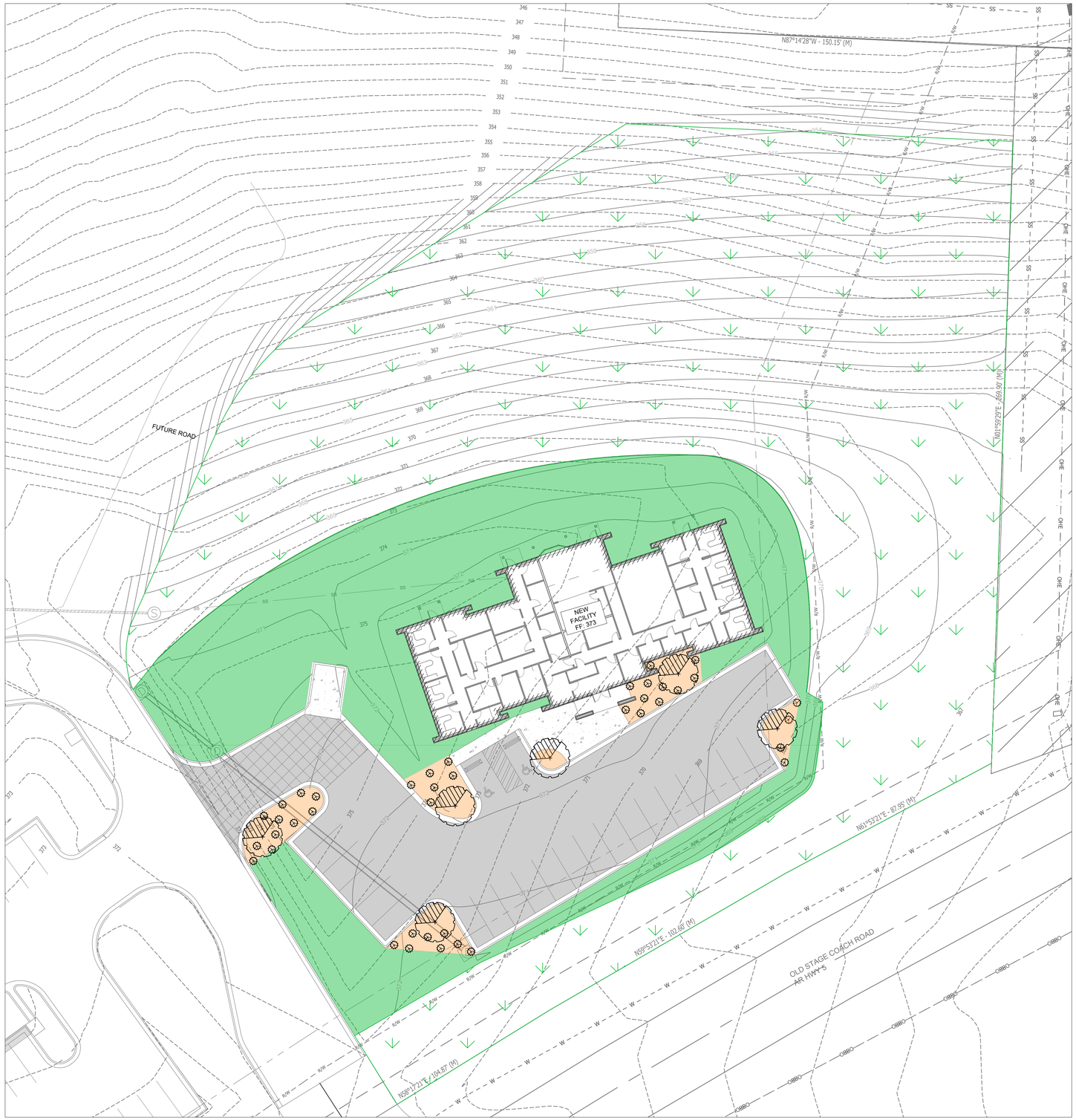
PAGE TITLE:
POST-DEV DRAINAGE

SHEET NUMBER:
C1.11




# LANDSCAPE PLAN

SCALE 1" = 60'

NOTES:
1. LANDSCAPED AREAS TO BE AMENDED WITH 4" OF TOPSOIL, SCARIFY SOIL 3" PRIOR TO APPLICATION. ALL TOP SOIL SHALL BE PLACED IN COORDINATION WITH GRADING AND DRAINAGE PLANS TO ENSURE THAT THE GRADING AND DRAINAGE DESIGN FOR THE SITE IS MAINTAINED AFTER BEING SODDED OR SEEDED. EXISTING SOIL FROM THE SITE CAN BE STOCK PILED AND REUSED AS LONG AS IT IS OF QUALITY THAT ENCOURAGES ADEQUATE GROWTH OF PLANTING MATERIAL. THE CONTRACTOR IS RESPONSIBLE FOR ANY SOIL TESTING THAT MAY BE REQUIRED.
2. LANDSCAPE PLAN REPRESENTS RECOMMENDED SPECIES, SIZES, & LOCATIONS. OWNER SHALL CHANGE THE ITEMS TO EQUAL OR GREATER VALUE.

## GENERAL CONSTRUCTION NOTES

A. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGES OCCURRING TO ANY PROPERTY DURING THE CONSTRUCTION OF THIS PROJECT. SAID CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PREVENT PROPERTY DAMAGE.

B. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR WILL SOLELY AND COMPLETELY BE RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND WILL NOT BE LIMITED TO NORMAL WORKING HOURS.

THE DUTY OF BRYANT TO CONDUCT CONSTRUCTION INSPECTION REVIEWS OF THE CONTRACTOR'S PERFORMANCE IS NOT AN INSPECTION OR REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES IN, ON, OR NEAR THE CONSTRUCTION SITE.

C. ALL WATER AND SEWER IMPROVEMENTS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE LATEST REVISION TO THE CITY OF BRYANT'S WATER AND WASTEWATER (SANITARY SEWER) STANDARD SPECIFICATIONS.

D. THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR ELEVATION OF EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND, WHERE POSSIBLE, MEASUREMENTS TAKEN IN THE FIELD. THE INFORMATION IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR MUST CALL THE APPROPRIATE UTILITY COMPANY AT LEAST 48 HOURS BEFORE ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF ALL UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH PROPOSED IMPROVEMENTS SHOWN ON THE PLAN.

E. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH, AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.

F. PRIOR TO INSTALLATION OF ANY UTILITIES, THE CONTRACTOR IS TO EXCAVATE, VERIFY AND CALCULATE ALL CROSSINGS AND INFORM ANY AND ALL UTILITIES OF ANY CONFLICTS PRIOR TO CONSTRUCTION.

G. CONSTRUCTION SHALL NOT START ON ANY WATER UTILITY TIE-INS UNTIL APPROVAL IS GIVEN BY BRYANT WATER. SAID CONTRACTOR SHALL NOT OPERATE ANY VALVE, HYDRANT, OR WATER UTILITY APPURTENANCE NOR SHALL HE ATTACH TO OR TAP ANY WATER UTILITY MAIN WITHOUT APPROVAL. THE CONTRACTOR SHALL BEAR THE COST AND CONSEQUENCE OF ANY DISRUPTION OF UTILITY OPERATION CAUSED BY CONSTRUCTION.

H. FIBER OPTIC CABLE ON AND/OR ADJACENT TO THIS SITE WERE NOT LOCATED BY THE SURVEY AND ARE NOT SHOWN. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO LOCATE ANY FIBER OPTIC CABLES ASSOCIATED WITH THIS SITE AND TAKE ALL NECESSARY AND REQUIRED PRECAUTIONS TO PROTECT ANY EXISTING FIBER OPTIC CABLES. CONTRACTORS SHALL COORDINATE ALL EFFORTS WITH OWNER OF FIBER OPTIC CABLES OR THEIR DESIGNATED REPRESENTATIVE.

J. THE CONTRACTOR IS RESPONSIBLE FOR CONTACTING "ONECALL" SERVICE TO MARK ALL UTILITIES PRIOR TO ANY DEMOLITION, EARTHWORK, OR UTILITY WORK ON THIS SITE.

| PLANT SCHEDULE | | | | | | |
|---|---|---|---|---|---|---|
| PLANT TYPE | SYMBOL | CODE | QTY | COMMON SPECIES | SCIENTIFIC NAME | CAL / SIZE |
| TREES | | WO | 6 | WILLOW OAK | QUERCUS PHELLOS | MIN. 3" DIAMETER @ BASE AND 12' TALL |
| SHRUBS | | BW | 40 | DWARF NANDINA | N. DOMESTICA "HARBOUR DWARF" | 3 GAL |
| GROUND COVER | | SO | 16,501 SF | BERMUDA SOD | | |
| | | GS | 48,539 SF | GRASS SEED | | |
| | | | 1,828 SF | LANDSCAPE BEDDING (TBD BY OWNER) | | |

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No. 9540
PHILLIP A. LEWIS

N

0 20'
1" = 60'-0"

PROJECT NUMBER:

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PAGE TITLE:
LANDSCAPE PLAN

SHEET NUMBER:
C1.12

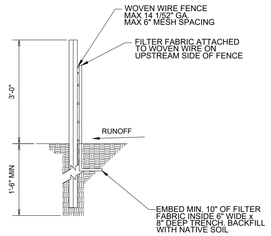
# STORMWATER POLLUTION PREVENTION PLAN

SCALE 1" = 60'

INSTALL FILTER SOCKS AT ALL INLETS; MAINTAIN THROUGHOUT CONSTRUCTION.
DISTURBED AREA: 85,405 AC.

## LEGEND

- DISTURBED AREA
- UNDISTURBED AREA
- SEDIMENT FENCE WITH WIRE BACKING
- DRAINAGE DIRECTION




## SILT FENCE

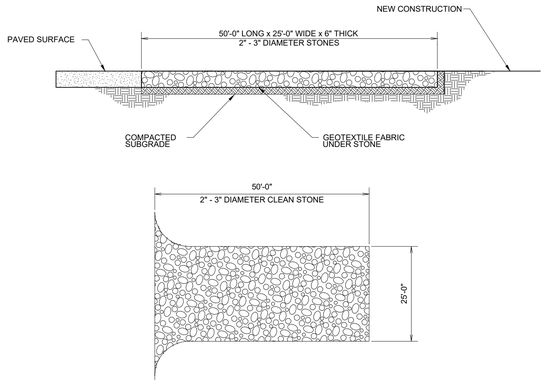
NOT TO SCALE

## NOTES AND SPECIFICATIONS:

1. POSTS SHALL BE A MINIMUM OF 36 INCHES CONSTRUCTED OF EITHER OF THE FOLLOWING MATERIALS: STEEL "T" OR "U" TYPE, OR 2" x 2" HARDWOOD.
2. WOVEN WIRE USED AS ADDITIONAL FENCE SUPPORT SHALL BE MINIMUM 14.5 GA. WITH 6" MAXIMUM SPACING.
3. WOVEN WIRE SHALL BE PLACED ALONG THE UPHILL SIDE OF THE FENCE AND FASTENED WITH WIRE TIES OR 1" STAPLES ALONG THE UPHILL SIDE OF THE POSTS.
4. FILTER FABRIC SHALL BE FASTENED TO WOVEN WIRE ACCORDING TO MANUFACTURER'S RECOMMENDATION, OR WITH TIES EVERY 24" AT THE TOP AND MID-SECTIONS.
5. WHERE TWO PIECES OF FILTER FABRIC ADJOIN EACH OTHER THEY SHALL BE OVERLAPPED BY 6 INCHES AND FOLDED TOGETHER.
6. WHERE TWO POSTS MEET TO JOIN FENCE SECTIONS, THE TOPS OF THE POSTS SHALL BE SECURED TOGETHER WITH WIRE.
7. THE FENCE SHALL BE CONSTRUCTED ALONG THE CONTOUR AS MUCH AS POSSIBLE.
8. ENDS OF FENCES SHALL BE EXTENDED UP THE SLOPE TO PRVENT RUNOFF FROM MIGRATING AROUND THE END OF THE FENCE.
9. INSPECTION OF THE FENCE SHALL BE PERFORMED WEEKLY, OR IMMEDIATELY AFTER A RAIN EVENT, OR WHEN BULGES APPEAR IN THE FENCE. ACCUMALTED SILT SHALL NOT BE ALLOWED TO EXCEED HALF THE HEIGHT OF THE FABRIC. REPAIR AND OR REPLACMENT OF DAMAGED FENCE SHALL BE COMPLETED PROMPTLY.
10. ACCUMULATED SILT SHALL BE REMOVED AND DISPOSED OF IN AN APPROVED SITE IN SUCH A MANNER THAT IT WILL NOT CONTRIBUTE TO OFF-SITE SILTATION.
11. ALL FENCING SHALL BE REMOVED WITH THE CONSTRUCTION SITE IS FULLY STABLIZED SO AS TO NOT IMPEDE STORM FLOW OR DRAINAGE.
12. PRE-FRABRICATED UNITS DO NOT REQUIRE THE USE OF WOVEN WIRE FENCE.

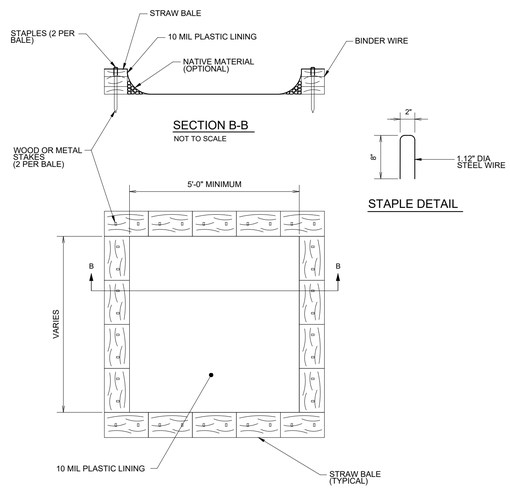
# NOTES (GENERAL):

1. SEE EROSION CONTROL DETAILS IN SWPPP FOR EROSION CONTROL FACILITIES.
2. SEE SWPPP FOR INSTALLATION, MAINTENANCE, INSPECTION, AND RECORD KEEPING REQUIREMENTS.
3. CONTRACTOR SHALL SHOW EROSION CONTROL MEASURE ON SITE MAP.
4. EROSION AND SEDIMENT CONTROL STRUCTURES TO MEET SWPPP DETAILS - APPENDIX D
5. INSTALL ROCK DITCH, CHECK, OR SAND BAG CHECKS AS NECESSARY TO PREVENT SCOUR UNTIL LANDSCAPING IS ESTABLISHED.
6. CONTRACTOR MUST PLACE SEDIMENT BASIN WITH SEDIMENT FENCE OUTLET FOR ANY SEDIMENT CONTAMINATED DEWATERING DISCHARGE.
7. FINAL SLOPE WILL BE SAME DIRECTION AS EXISTING SLOPE.
8. TEMPORARY STABILIZATION PRACTICES WILL NOT BE REQUIRED. WORK WILL BE CONTINUOUS AND DISTURBED AREA REVEGITATED IN A TIMELY MANNER. SEE SWPPP FOR SEEDING MIXES.
9. PERMANENT STABILIZATION OF ALL DISTURBED AREAS ARE TO BE SEEDED, FERTILIZED, WATERED AND COVERED WITH STRAW UNLESS OTHERWISE NOTED ON PLANS TO BE HYDROSEEDED.
10. CONTRACTOR TO SHOW CONCRETE WASH OUT SUMP, ENTRANCE/EXIT PAD AND OTHER CONTROLS AS REQUIRED/NEEDED AS SWPPP SITE MAP IS UPDATED THROUGHOUT THE DURATION OF THE PROJECT.
11. STOCKPILING OF CONSTRUCTION SPOIL MATERIAL AT PARTICULAR LOCATIONS SHALL ONLY BE ALLOWED FOR A LIMITED TIME PERIOD, NOT TO EXCEED (6) MONTHS. PRIOR TO A FINAL INSPECTION OF THE GRADING PERMIT, THE FOLLOWING STANDARDS SHALL BE ACHIEVED FOR COMPLETION OF CONSTRUCTION:
    a) DEVELOPMENT AND GRADING WITHIN THE DISTURBED AREA IS COMPLETE AND MATCHES PLANS AS APPROVED BY THE PLANNING COMMISSION, AND
    b) THE DISTURBED SOIL AREA IS OBSERVED TO HAVE 80% GRASS COVERAGE AND 100% STABILITY, AND
    c) NO SLOPES STEEPER THAN A 3:1 PITCH UNLESS OTHERWISE APPROVED IN WRITING BY THE DIRECTOR OF ENGINEERING, AND
    d) NOTICE OF VIOLATIONS ISSUED HAVE ALL CORRECTIVE ACTIONS APPROVED WITH AN INSPECTION REPORT SIGNED BY A REPRESENTATIVE OF THE DIRECTOR OF ENGINEERING, AND
    e) ALL HEAVY EQUIPMENT, STOCKPILES, AND CONSTRUCTION SITE MATERIALS HAVE BEEN REMOVED FROM THE CONSTRUCTION SITE.




## CONSTRUCTION ENTRANCE

NOT TO SCALE




## CONCRETE WASHOUT

NOT TO SCALE

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

N
0 60'
1" = 60'-0"

PROJECT NUMBER:

SHEET ISSUE DATE:
07/09/2025

PAGE TITLE:
SWPPP PLAN

SHEET NUMBER:
C1.13

# NEW BEGINNINGS

# PRELIMINARY DRAINAGE REPORT

***Date:*** **07-15-2025**

***Located in:*** **Bryant, Arkansas**

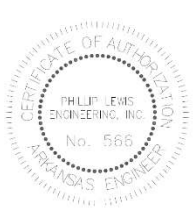
***Prepared for:***
**City of Bryant, Arkansas**

**Prepared by:**

PHILLIP LEWIS ENGINEERING
Structural + Civil Consultants
23620 Interstate 30 | Bryant, AR
PH: 501-350-9840

# *CERTIFICATION*

I hereby state that this Final Drainage has been prepared by me or under my supervision and meets the standard of care and expertise which is usual and customary in this community of professional engineers. The analysis has been prepared utilizing procedures and practices by the City of Bryant and within the standard accepted practices.



DATE: 07-15-2024

Phillip A. Lewis, PE.

# PROJECT LOCATION MAP

# DESCRIPTION OF PROPERTY

The proposed project is for the consruction of a new pregnancy center located along Highway 5, directly adjacent to the current ongoing seminary project. The proposed development is a 5,900 sq. ft. building and parking lot.

The intent of this drainage analysis is to adequately size the storm sewer system and summarize pre and post runoff conditions.

The existing ground coverage for the entire development drainage basin consists of and natural vegetation (2%-7% slope), hydrologic soil group B/C.

According to FEMA Flood Insurance Rate Map, Panel 05125C0240E, this property lies within Zone X, areas determined to be outside the 0.2% annual chance floodplain. A copy of the map can be found in the appendix.

# DRAINAGE CRITERIA

In accordance with the requirements of the City of Bryant, the proposed developments drainage plan and this drainage report were developed with the criteria established in the Bryant Stormwater Management & Drainage Manual provided on cityofbryant.com.

All drainage calculations were performed using HydroCAD software to determine and analyze the changes in stormrunoff volume, flow rates, and design the outlet release structure.  Hydraflow Express software was used to appropriately design and size all storm sewer inlets, pipes and channels.

Calculations were performed using the Rational Method, using NOAA rainfall data, Runoff Coefficient table (Bryant Stormwater Management & Drainage Manual, Table 400-2) and the pipe and intlet structure sizes were determined by the 25-year storm event.

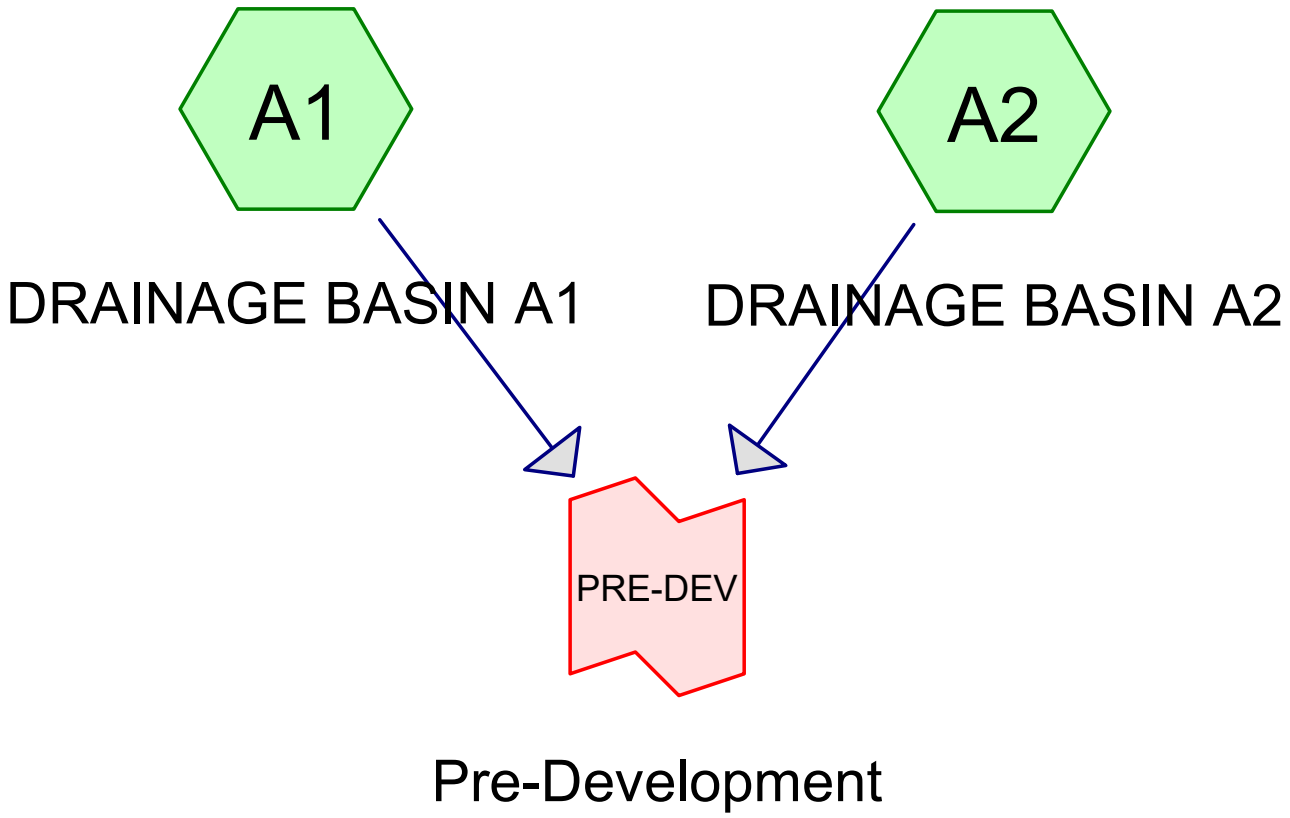
# PROPOSED DRAINAGE SYSTEM

This develompent is designed to capture the majority of runoff within the parking lot curb and gutter. The storm sewer system will consist of standard concrete curb inlets. These inlets were sized based on there independent drainage basin flow rate and the slope that the inlets will be placed at.

Overall Pre-development and Post-development runoff/discharge rates are compared below:

| Storm Event | Pre-development Discharge (cfs) | Post-development Discharge (cfs) |
|---|---|---|
| 2-yr | 1.30 | 3.94 |
| 5-yr | 1.54 | 4.73 |
| 10-yr | 1.74 | 5.28 |
| 25-yr | 2.01 | 6.08 |
| 100-yr | 2.38 | 7.24 |

# PRE DEVELOPMENT HYDROGRAPHS




Pre-Development

Subcat Reach Pond Link

**Routing Diagram for New Beginnings Drainage**
Prepared by Phillip Lewis Engineering, Printed 7/15/2025
HydroCAD® 10.20-5c s/n 12520 © 2023 HydroCAD Software Solutions LLC

## Summary for Subcatchment A1: DRAINAGE BASIN A1

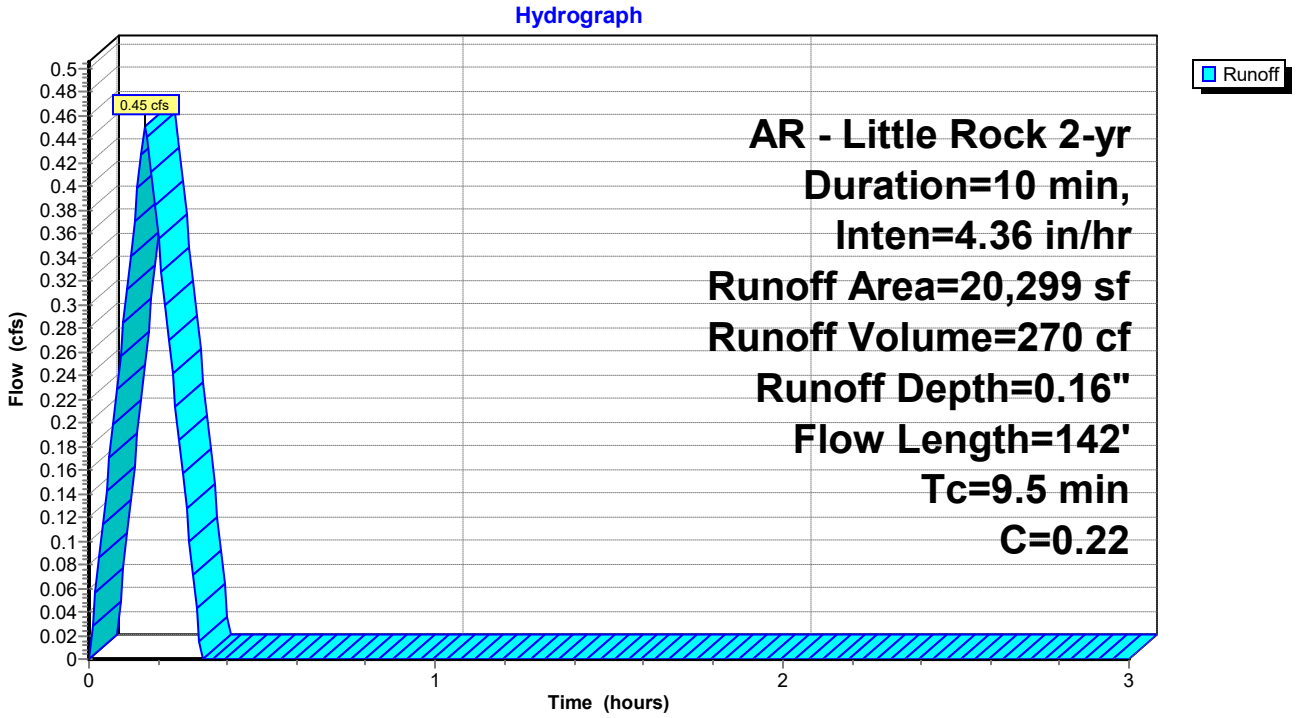
Runoff = 0.45 cfs @ 0.16 hrs, Volume= 270 cf, Depth= 0.16"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=10 min, Inten=4.36 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,299 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 20,299 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 9.2 | 100 | 0.0430 | 0.18 | | **Sheet Flow, Overland Sheet flow** Grass: Dense n= 0.240 P2= 4.20" |
| 0.3 | 42 | 0.1410 | 2.63 | | **Shallow Concentrated Flow, Overland Concentrated Flow** Short Grass Pasture Kv= 7.0 fps |
| 9.5 | 142 | Total | | | |

## Subcatchment A1: DRAINAGE BASIN A1



## Summary for Subcatchment A2: DRAINAGE BASIN A2

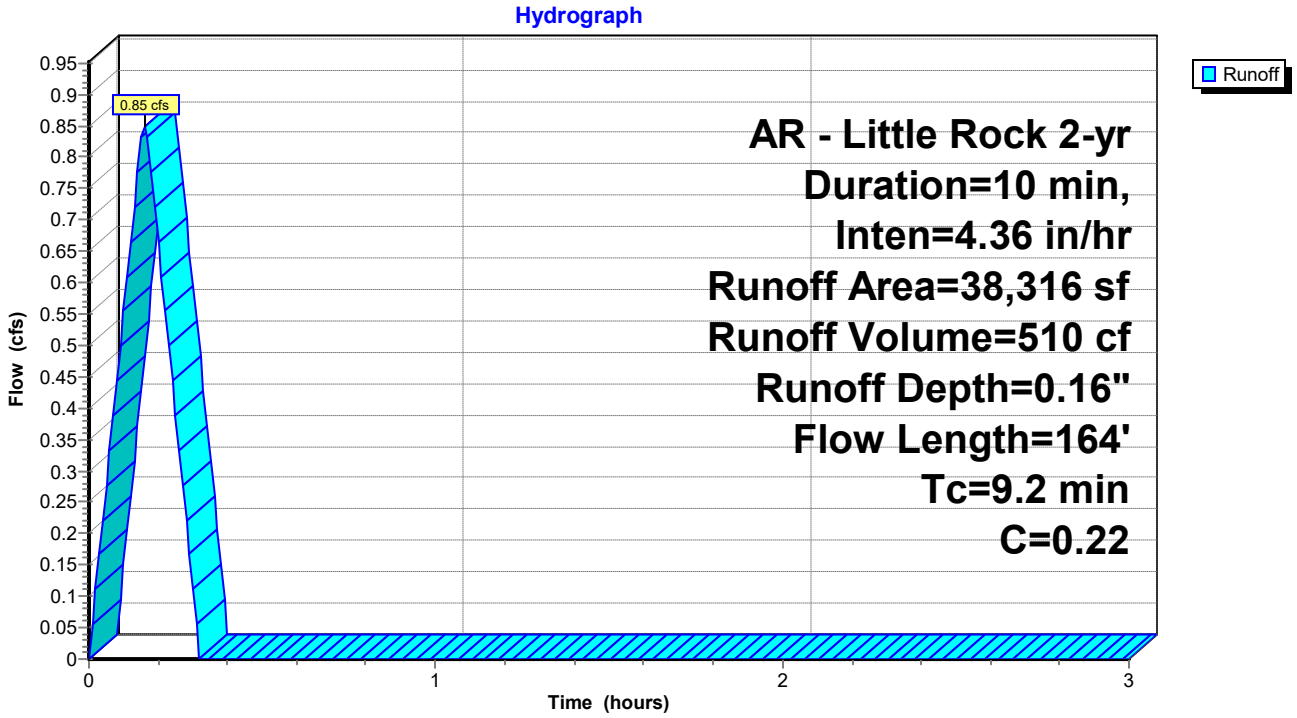
Runoff = 0.85 cfs @ 0.16 hrs, Volume= 510 cf, Depth= 0.16"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=10 min, Inten=4.36 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 38,316 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 38,316 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 8.3 | 100 | 0.0560 | 0.20 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.9 | 64 | 0.0320 | 1.25 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.2 | 164 | Total | | | |

## Subcatchment A2: DRAINAGE BASIN A2

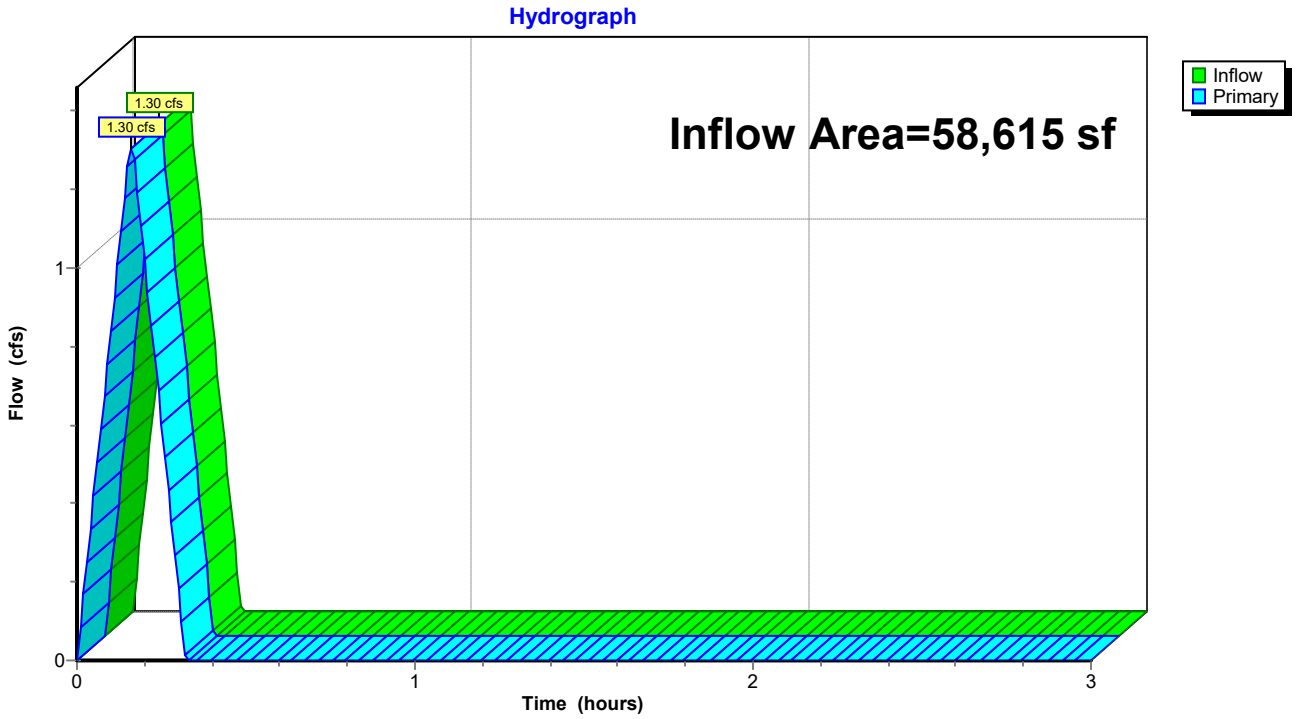


## Summary for Link PRE-DEV: Pre-Development

Inflow Area = 58,615 sf, 0.00% Impervious, Inflow Depth = 0.16" for 2-yr event
Inflow = 1.30 cfs @ 0.16 hrs, Volume= 780 cf
Primary = 1.30 cfs @ 0.16 hrs, Volume= 780 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link PRE-DEV: Pre-Development



## Summary for Subcatchment A1: DRAINAGE BASIN A1

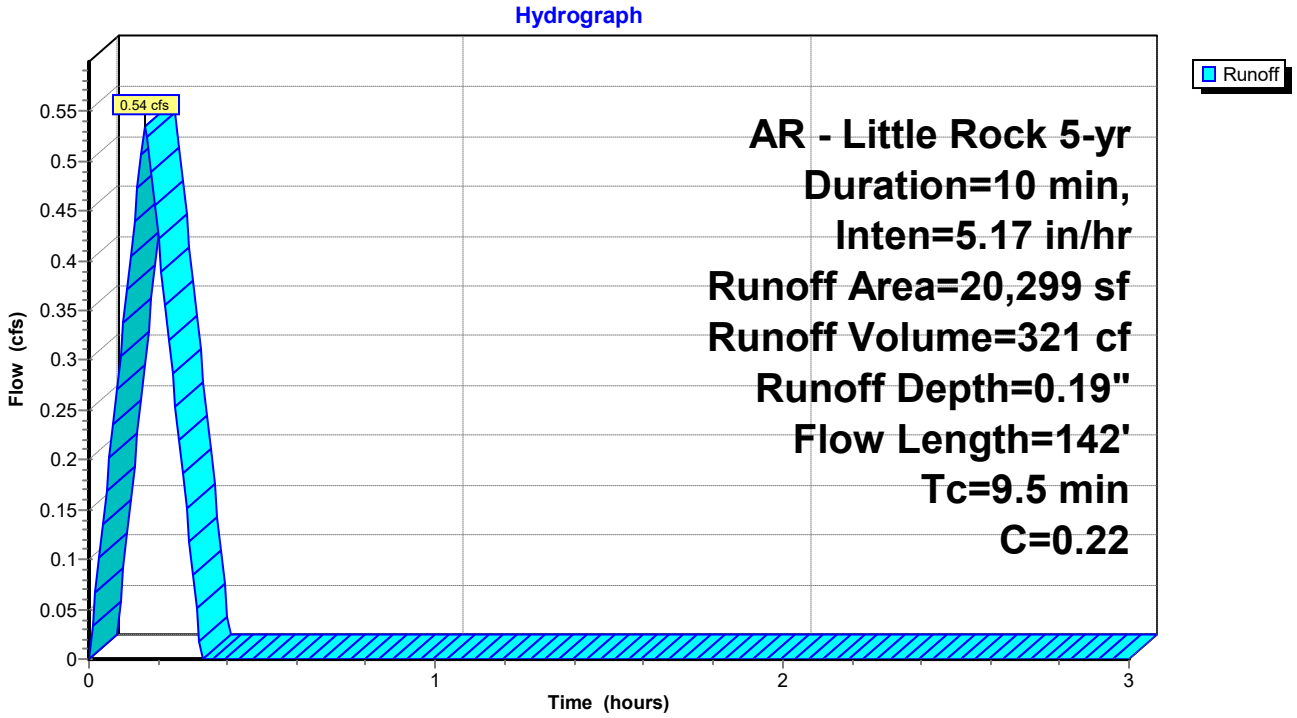
Runoff = 0.54 cfs @ 0.16 hrs, Volume= 321 cf, Depth= 0.19"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=10 min, Inten=5.17 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,299 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 20,299 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 9.2 | 100 | 0.0430 | 0.18 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.3 | 42 | 0.1410 | 2.63 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.5 | 142 | Total | | | |

## Subcatchment A1: DRAINAGE BASIN A1



## Summary for Subcatchment A2: DRAINAGE BASIN A2

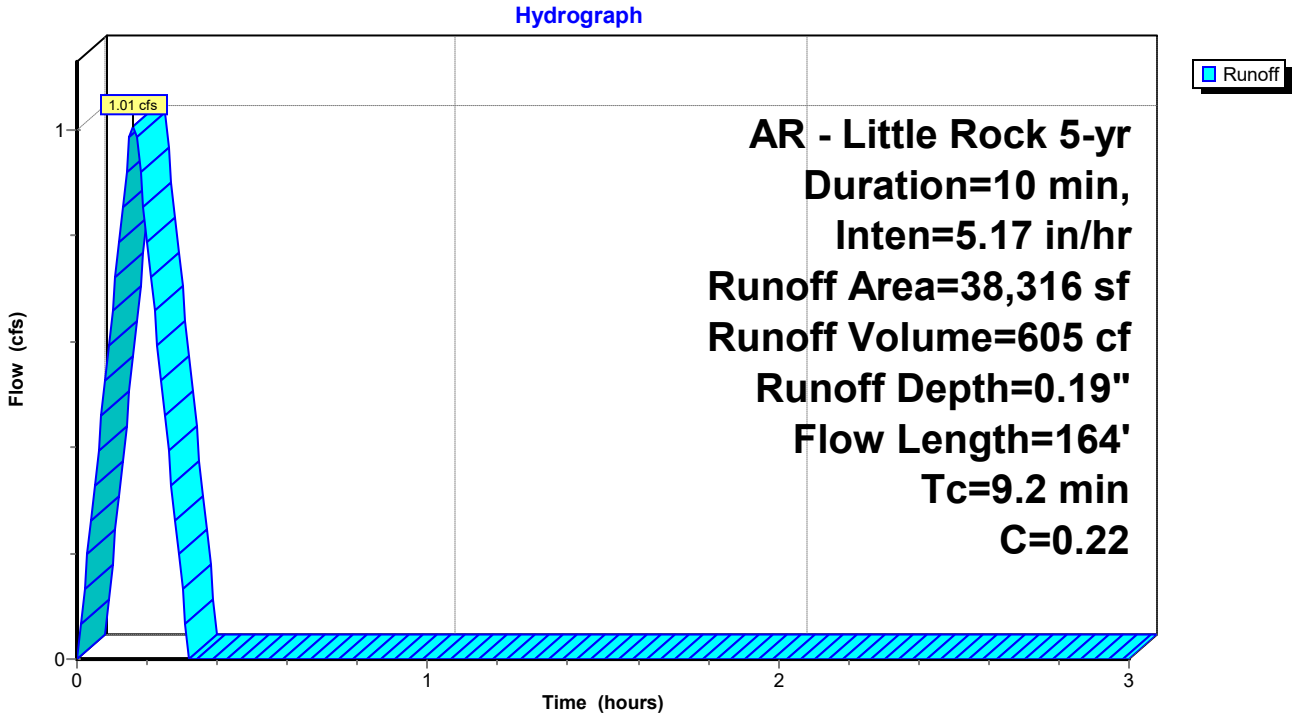
Runoff = 1.01 cfs @ 0.16 hrs, Volume= 605 cf, Depth= 0.19"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=10 min, Inten=5.17 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 38,316 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 38,316 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 8.3 | 100 | 0.0560 | 0.20 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.9 | 64 | 0.0320 | 1.25 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.2 | 164 | Total | | | |

## Subcatchment A2: DRAINAGE BASIN A2

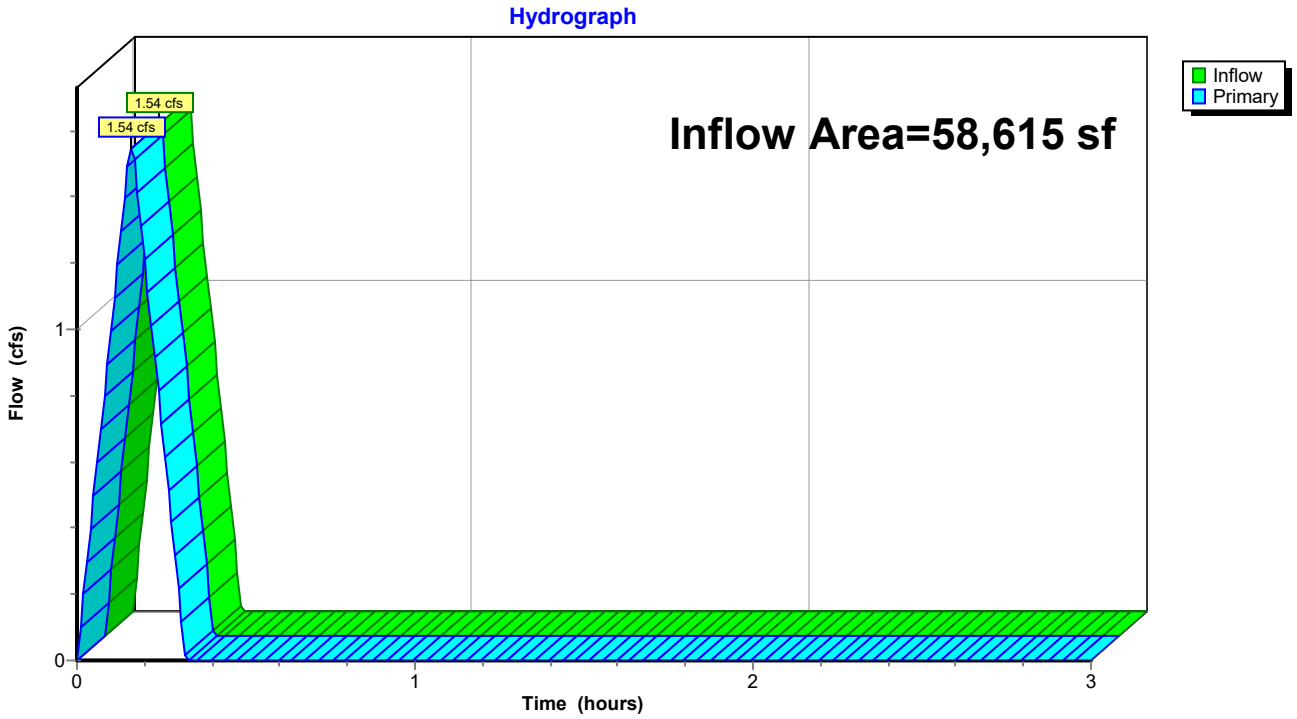


## Summary for Link PRE-DEV: Pre-Development

Inflow Area = 58,615 sf, 0.00% Impervious, Inflow Depth = 0.19" for 5-yr event
Inflow = 1.54 cfs @ 0.16 hrs, Volume= 926 cf
Primary = 1.54 cfs @ 0.16 hrs, Volume= 926 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link PRE-DEV: Pre-Development



## Summary for Subcatchment A1: DRAINAGE BASIN A1

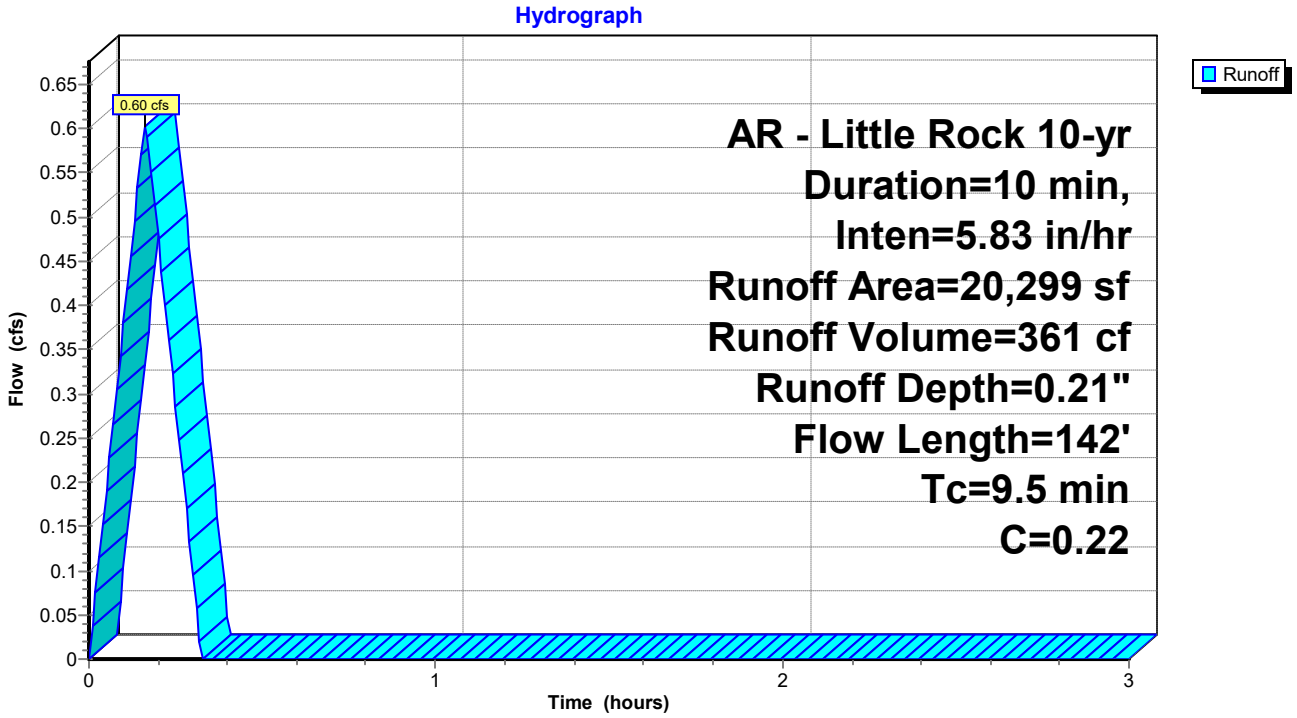
Runoff = 0.60 cfs @ 0.16 hrs, Volume= 361 cf, Depth= 0.21"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=10 min, Inten=5.83 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,299 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 20,299 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 9.2 | 100 | 0.0430 | 0.18 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.3 | 42 | 0.1410 | 2.63 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.5 | 142 | Total | | | |

## Subcatchment A1: DRAINAGE BASIN A1



## Summary for Subcatchment A2: DRAINAGE BASIN A2

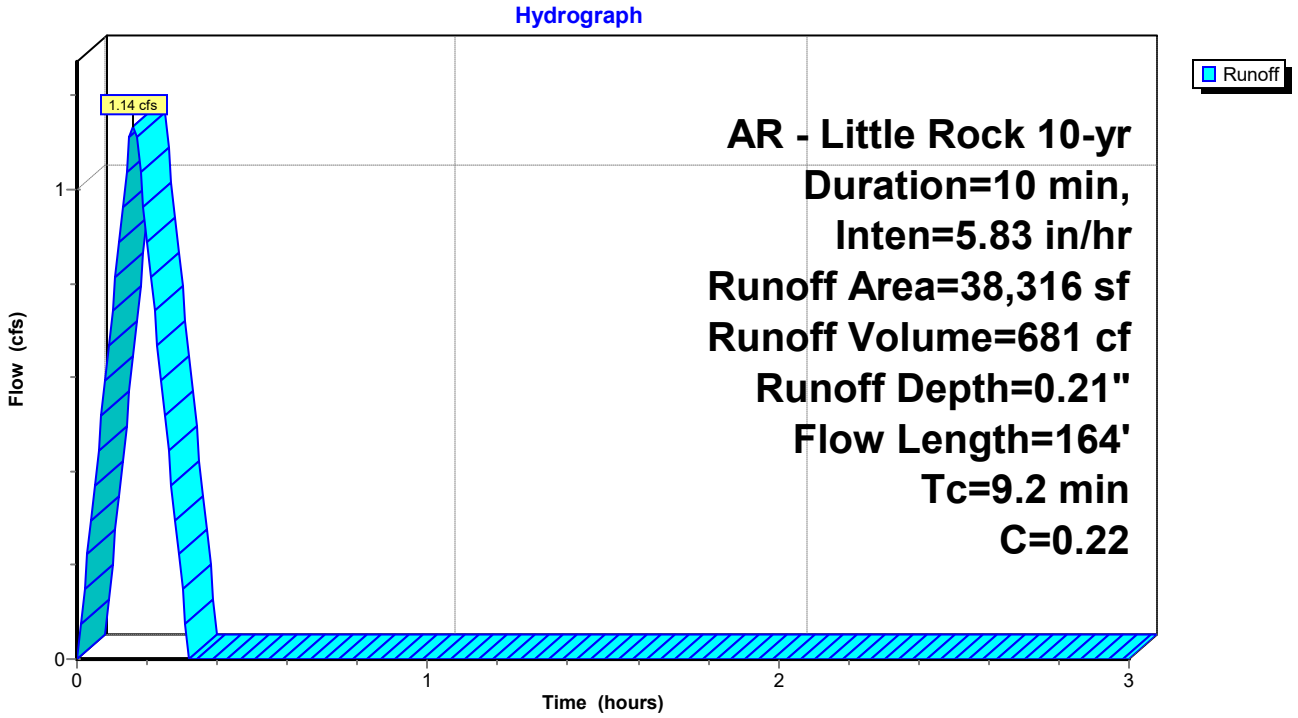
Runoff = 1.14 cfs @ 0.16 hrs, Volume= 681 cf, Depth= 0.21"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=10 min, Inten=5.83 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 38,316 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 38,316 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 8.3 | 100 | 0.0560 | 0.20 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.9 | 64 | 0.0320 | 1.25 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.2 | 164 | Total | | | |

## Subcatchment A2: DRAINAGE BASIN A2

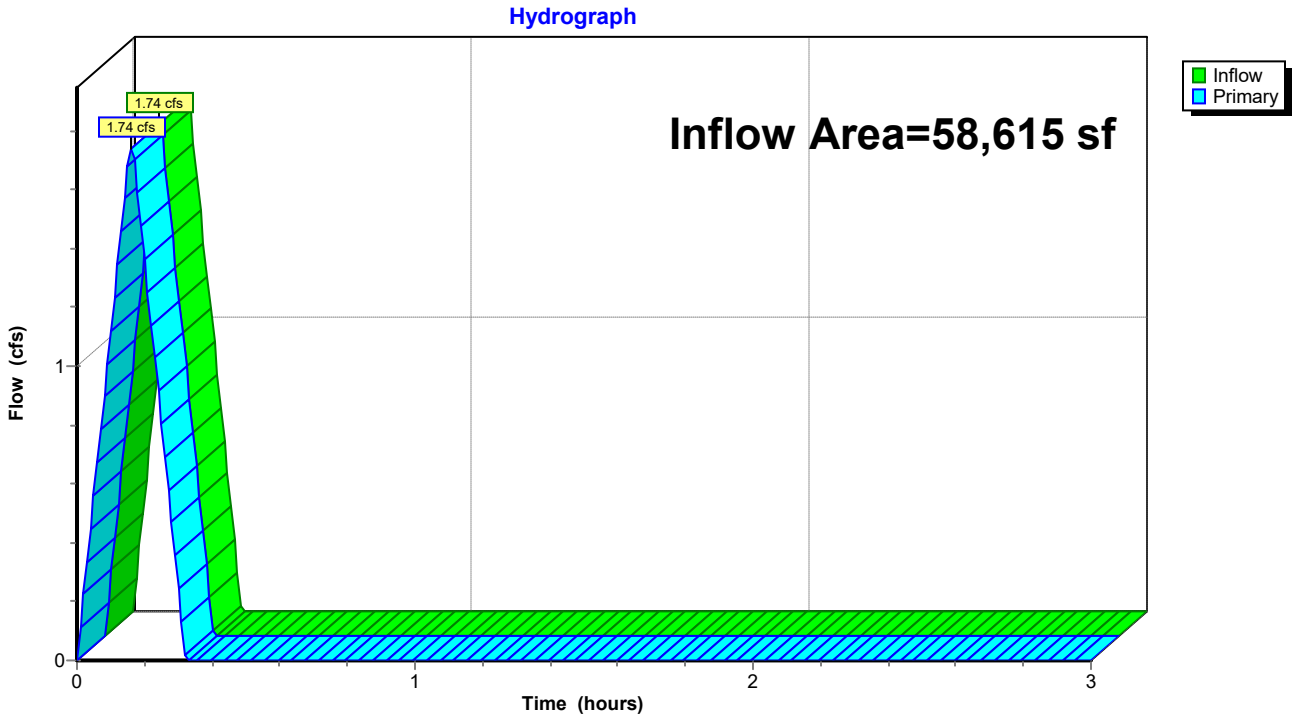


## Summary for Link PRE-DEV: Pre-Development

Inflow Area = 58,615 sf, 0.00% Impervious, Inflow Depth = 0.21" for 10-yr event
Inflow = 1.74 cfs @ 0.16 hrs, Volume= 1,043 cf
Primary = 1.74 cfs @ 0.16 hrs, Volume= 1,043 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link PRE-DEV: Pre-Development



## Summary for Subcatchment A1: DRAINAGE BASIN A1

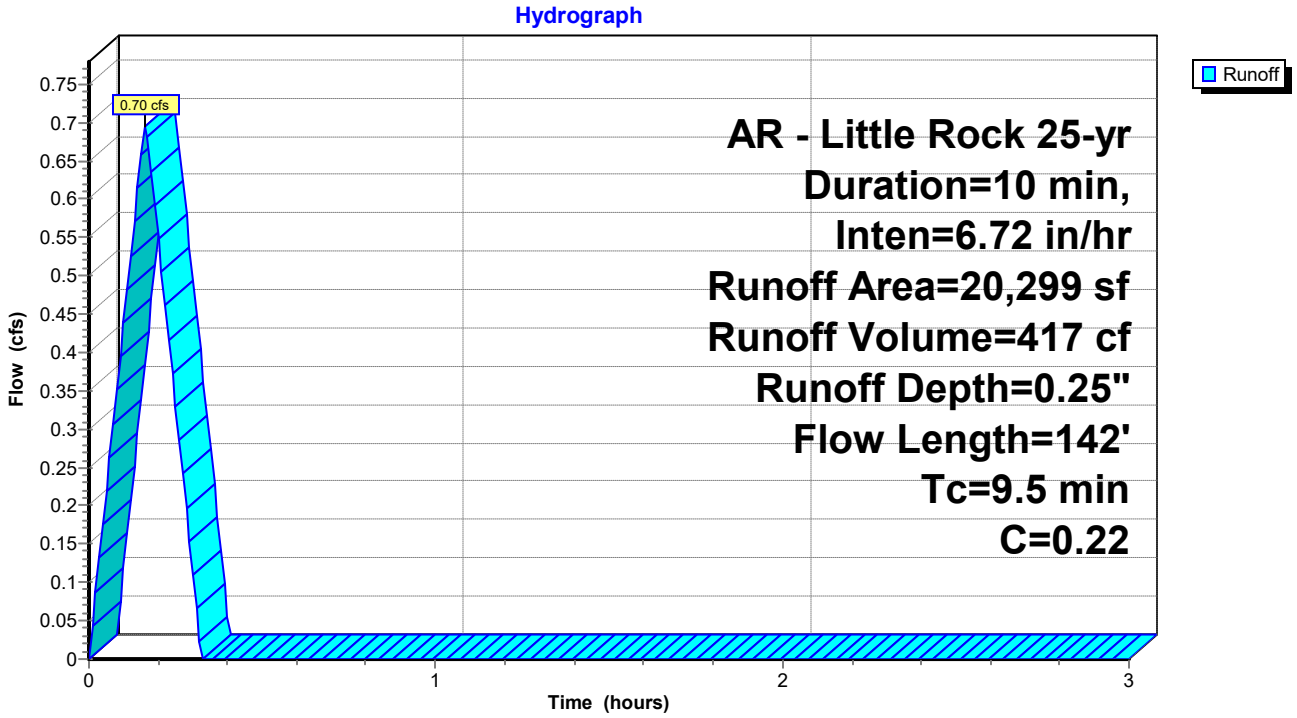
Runoff = 0.70 cfs @ 0.16 hrs, Volume= 417 cf, Depth= 0.25"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=10 min, Inten=6.72 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,299 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 20,299 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 9.2 | 100 | 0.0430 | 0.18 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.3 | 42 | 0.1410 | 2.63 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.5 | 142 | Total | | | |

## Subcatchment A1: DRAINAGE BASIN A1



## Summary for Subcatchment A2: DRAINAGE BASIN A2

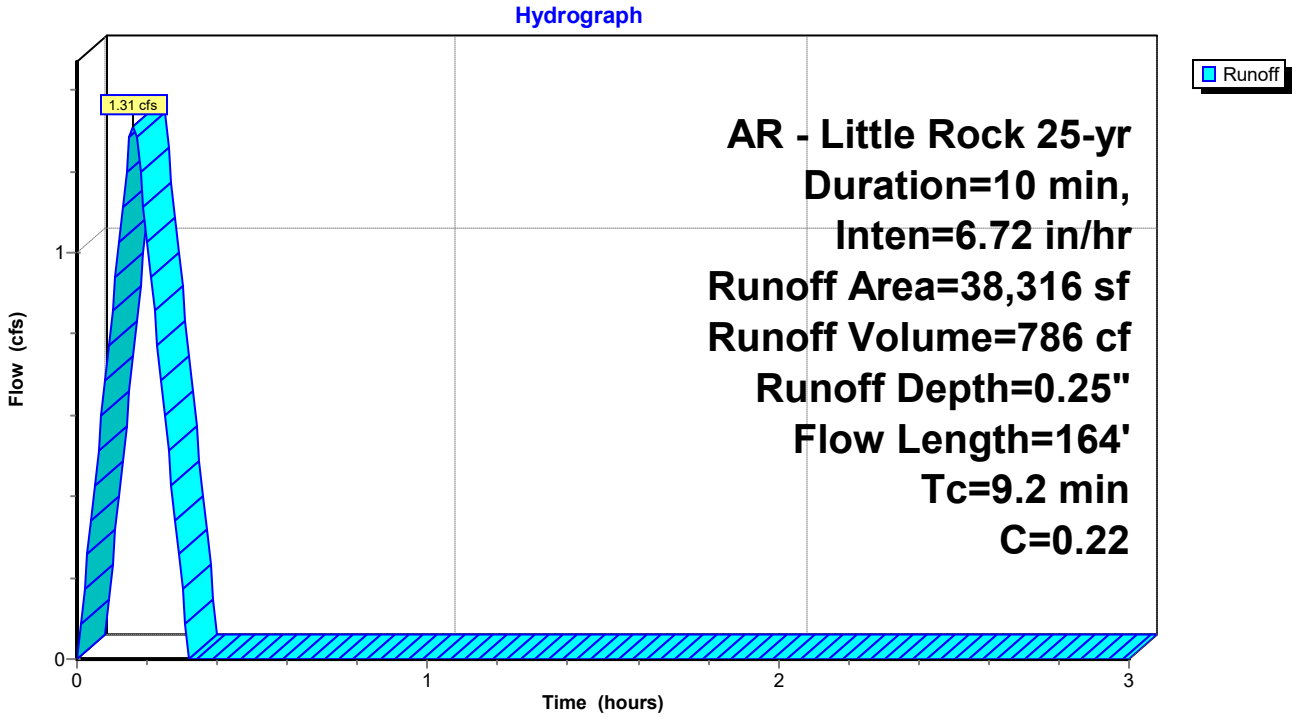
Runoff = 1.31 cfs @ 0.16 hrs, Volume= 786 cf, Depth= 0.25"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=10 min, Inten=6.72 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 38,316 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 38,316 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 8.3 | 100 | 0.0560 | 0.20 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.9 | 64 | 0.0320 | 1.25 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.2 | 164 | Total | | | |

## Subcatchment A2: DRAINAGE BASIN A2

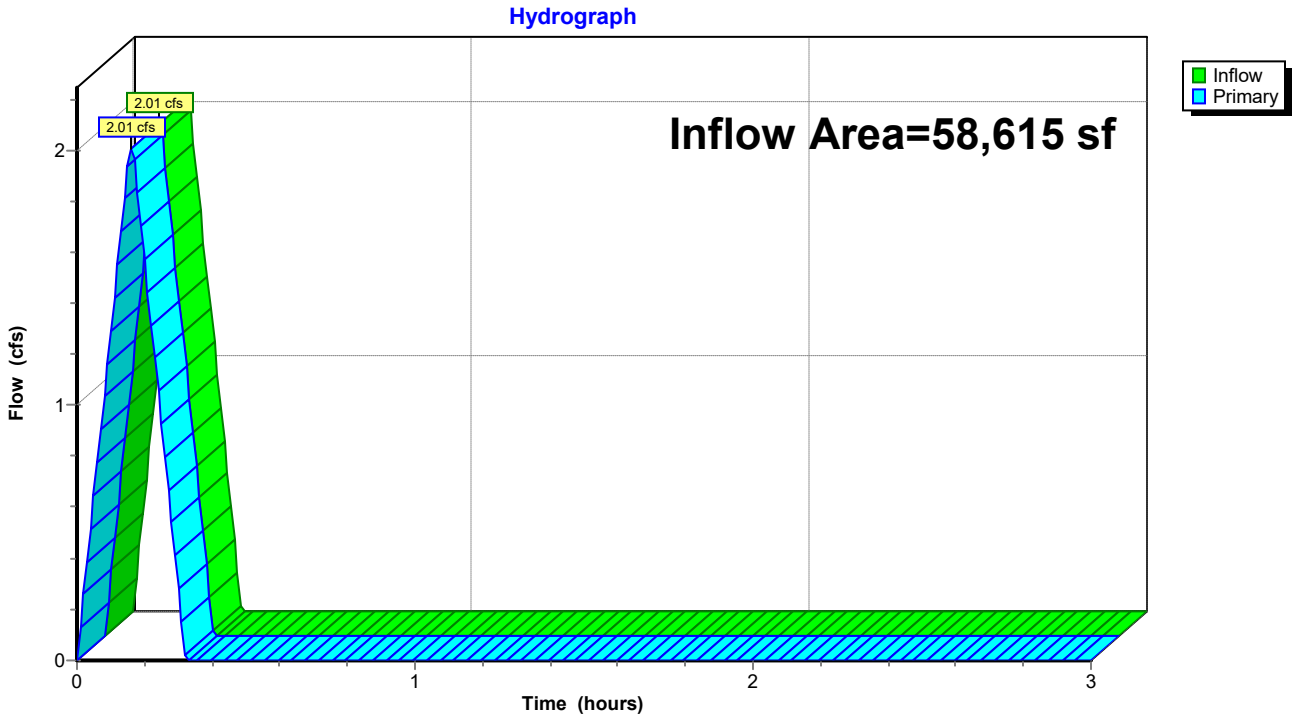


## Summary for Link PRE-DEV: Pre-Development

Inflow Area = 58,615 sf, 0.00% Impervious, Inflow Depth = 0.25" for 25-yr event
Inflow = 2.01 cfs @ 0.16 hrs, Volume= 1,203 cf
Primary = 2.01 cfs @ 0.16 hrs, Volume= 1,203 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link PRE-DEV: Pre-Development



## Summary for Subcatchment A1: DRAINAGE BASIN A1

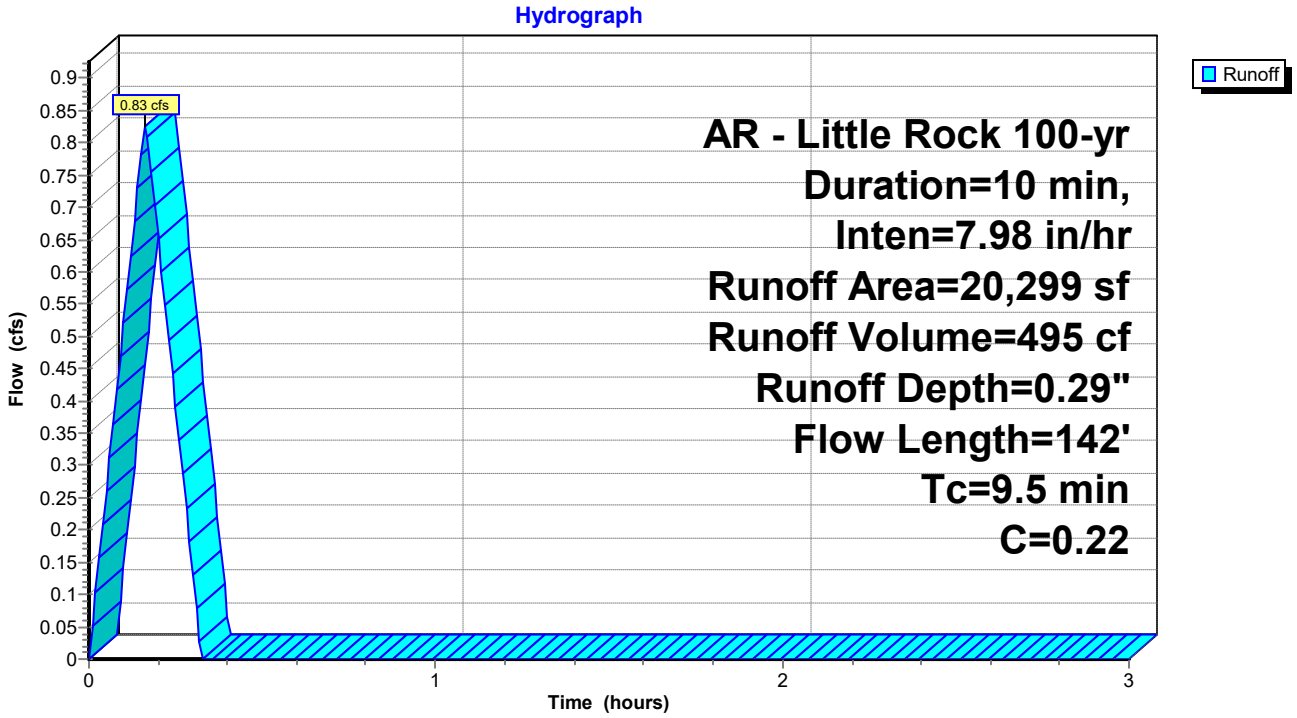
Runoff = 0.83 cfs @ 0.16 hrs, Volume= 495 cf, Depth= 0.29"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=10 min, Inten=7.98 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,299 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 20,299 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 9.2 | 100 | 0.0430 | 0.18 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.3 | 42 | 0.1410 | 2.63 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.5 | 142 | Total | | | |

## Subcatchment A1: DRAINAGE BASIN A1



## Summary for Subcatchment A2: DRAINAGE BASIN A2

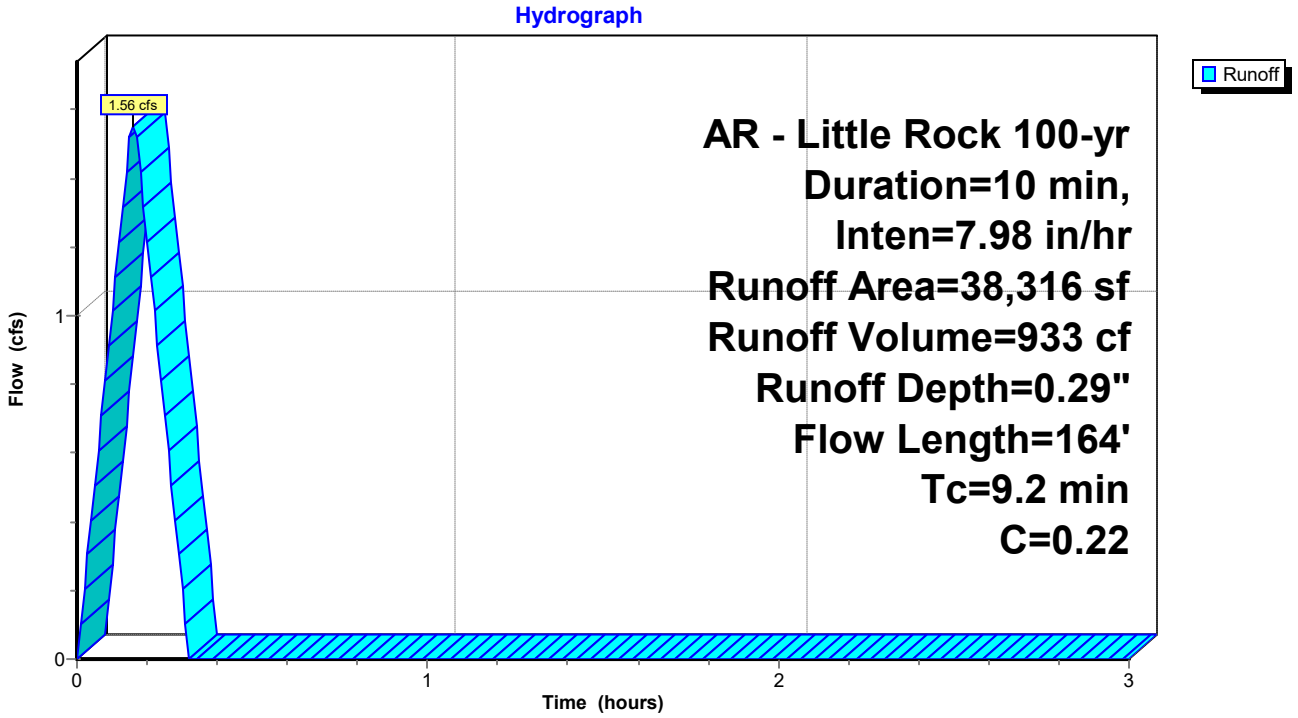
Runoff = 1.56 cfs @ 0.16 hrs, Volume= 933 cf, Depth= 0.29"
Routed to Link PRE-DEV : Pre-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=10 min, Inten=7.98 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 38,316 | 0.22 | Sandy Soil 2-7% per manual (undeveloped) |
| 38,316 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 8.3 | 100 | 0.0560 | 0.20 | | **Sheet Flow, Overland Sheet flow**<br>Grass: Dense n= 0.240 P2= 4.20" |
| 0.9 | 64 | 0.0320 | 1.25 | | **Shallow Concentrated Flow, Overland Concentrated Flow**<br>Short Grass Pasture Kv= 7.0 fps |
| 9.2 | 164 | Total | | | |

## Subcatchment A2: DRAINAGE BASIN A2

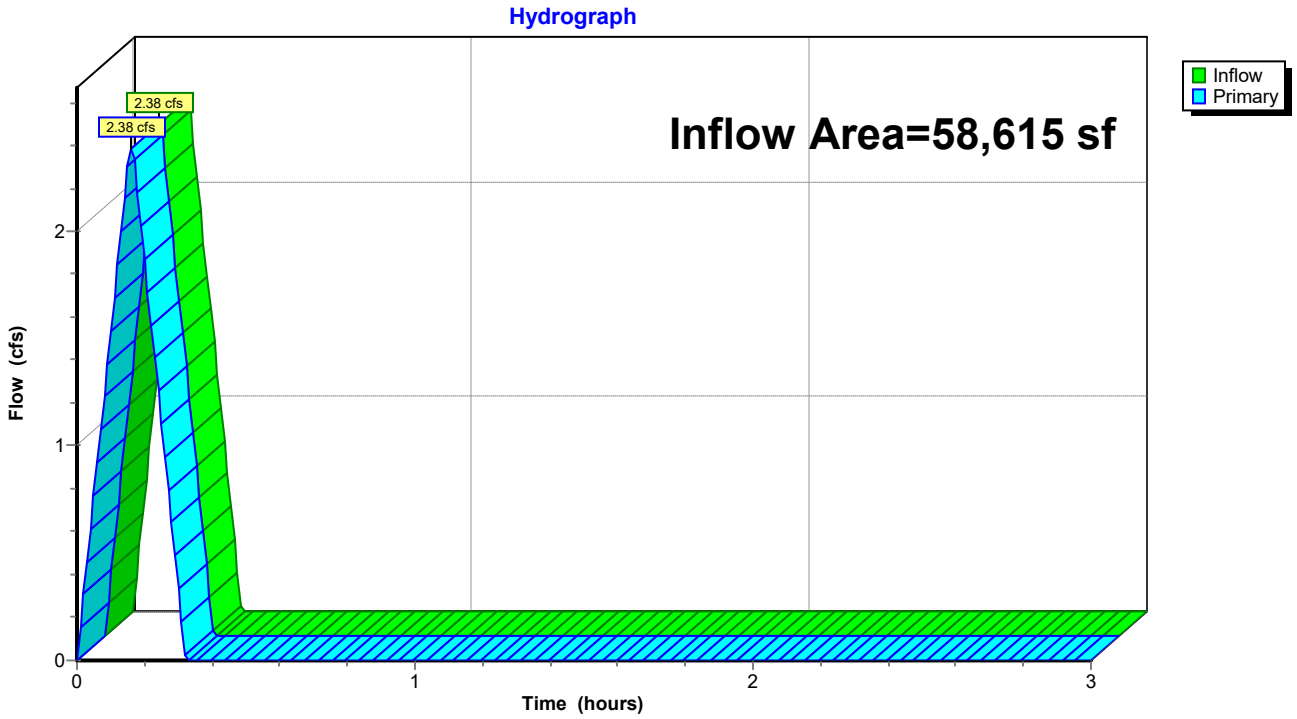


## Summary for Link PRE-DEV: Pre-Development

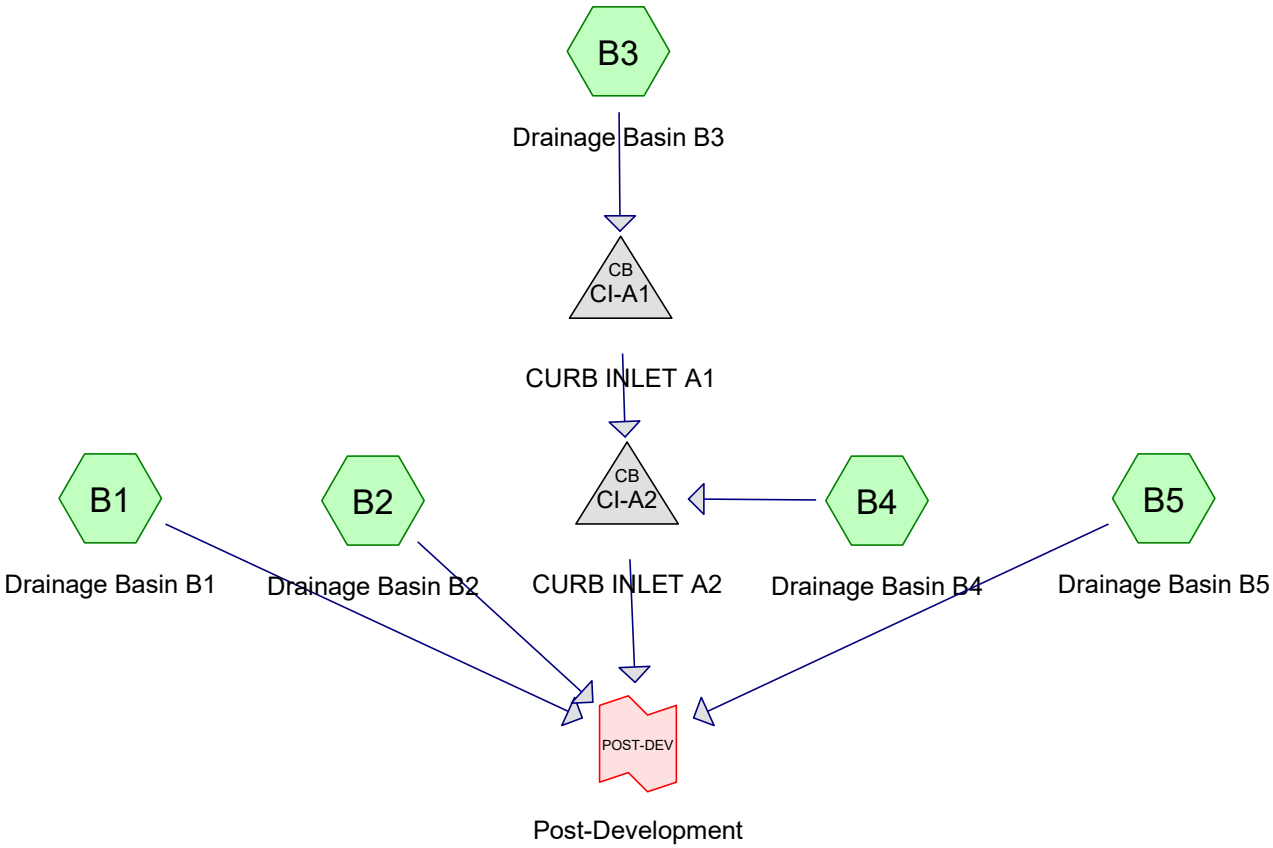
Inflow Area = 58,615 sf, 0.00% Impervious, Inflow Depth = 0.29" for 100-yr event
Inflow = 2.38 cfs @ 0.16 hrs, Volume= 1,428 cf
Primary = 2.38 cfs @ 0.16 hrs, Volume= 1,428 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link PRE-DEV: Pre-Development



# POST DEVELOPMENT HYDROGRAPHS




Subcat Reach Pond Link

**Routing Diagram for New Beginnings Drainage**
Prepared by Phillip Lewis Engineering, Printed 7/15/2025
HydroCAD® 10.20-5c s/n 12520 © 2023 HydroCAD Software Solutions LLC

## Summary for Subcatchment B1: Drainage Basin B1

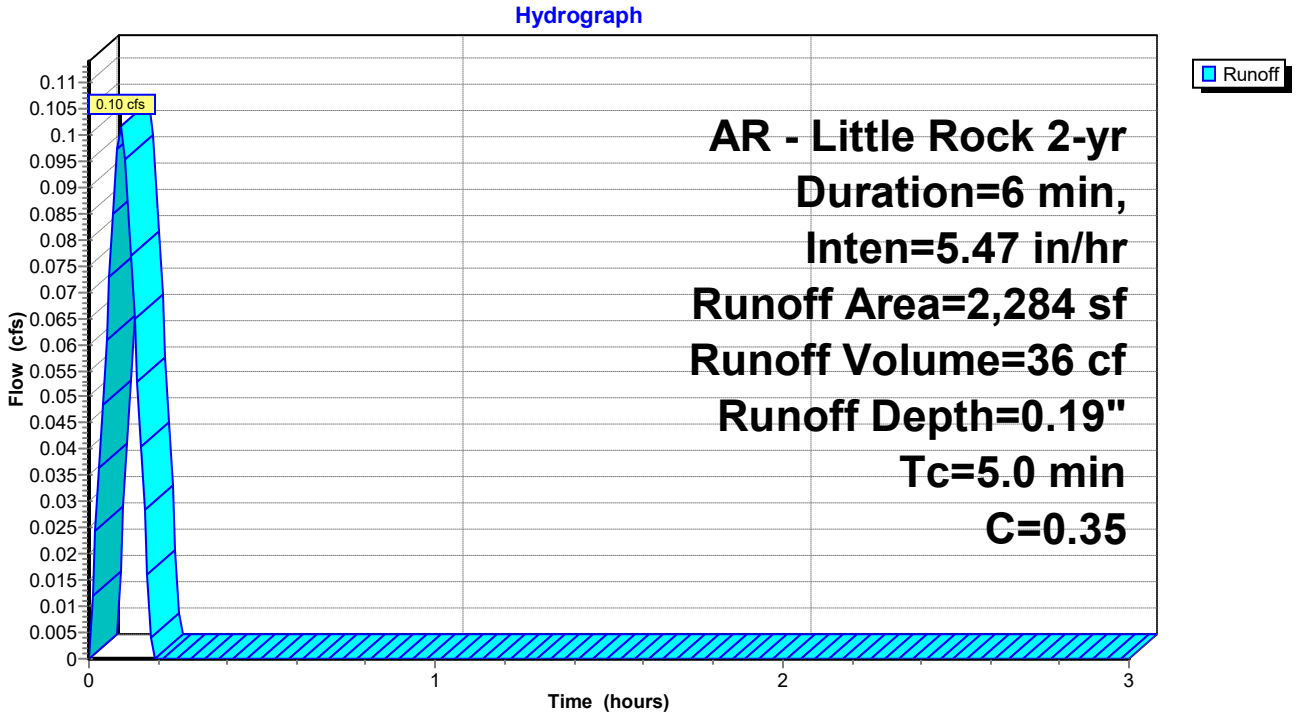
Runoff = 0.10 cfs @ 0.09 hrs, Volume= 36 cf, Depth= 0.19"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=6 min, Inten=5.47 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 2,284 | 0.35 | Sandy Soil 2-7% per manual |
| 0 | 0.92 | Paved Areas |
| 2,284 | 0.35 | Weighted Average |
| 2,284 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 5.0 | | | | | **Direct Entry, Minimum Adjustment** |

## Subcatchment B1: Drainage Basin B1



## Summary for Subcatchment B2: Drainage Basin B2

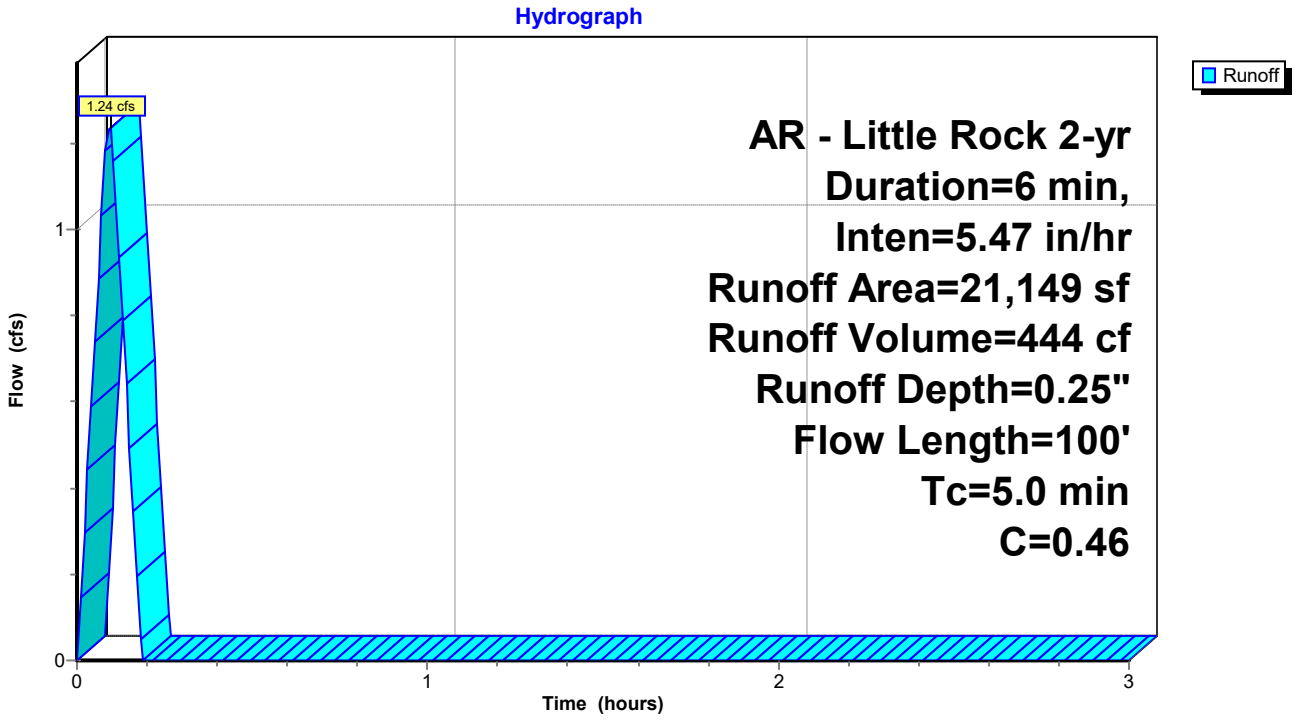
Runoff = 1.24 cfs @ 0.09 hrs, Volume= 444 cf, Depth= 0.25"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=6 min, Inten=5.47 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 16,931 | 0.35 | Sandy Soil 2-7% per manual |
| 4,218 | 0.92 | Paved Areas |
| 21,149 | 0.46 | Weighted Average |
| 21,149 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 42 | 0.1667 | 3.09 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.5 | 58 | 0.0500 | 2.04 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 4.3 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 100 | Total | | | |

## Subcatchment B2: Drainage Basin B2



## Summary for Subcatchment B3: Drainage Basin B3

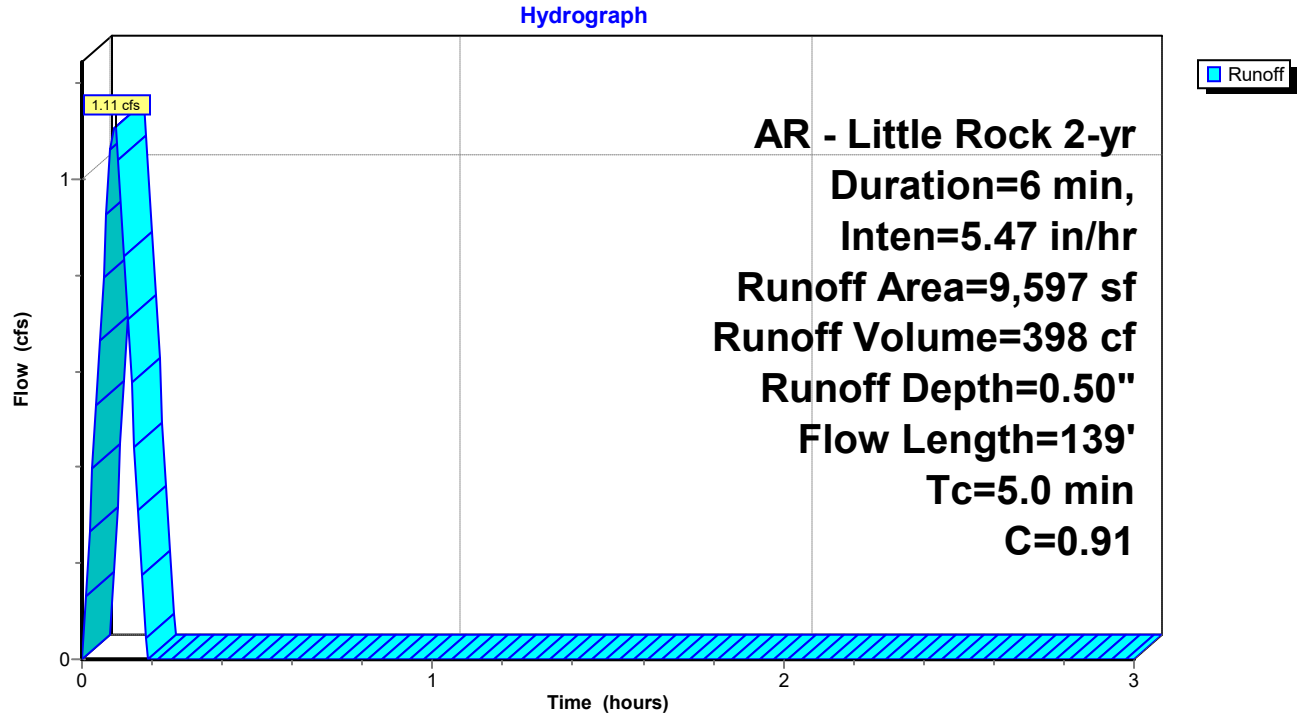
Runoff = 1.11 cfs @ 0.09 hrs, Volume= 398 cf, Depth= 0.50"
Routed to Pond CI-A1 : CURB INLET A1

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=6 min, Inten=5.47 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 155 | 0.35 | Sandy Soil 2-7% per manual |
| 9,442 | 0.92 | Paved Areas |
| 9,597 | 0.91 | Weighted Average |
| 9,597 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 28 | 0.1667 | 2.85 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 30 | 0.0160 | 1.13 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 41 | 0.0520 | 1.93 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.2 | 40 | 0.0360 | 3.85 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 3.8 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 139 | Total | | | |

## Subcatchment B3: Drainage Basin B3



## Summary for Subcatchment B4: Drainage Basin B4

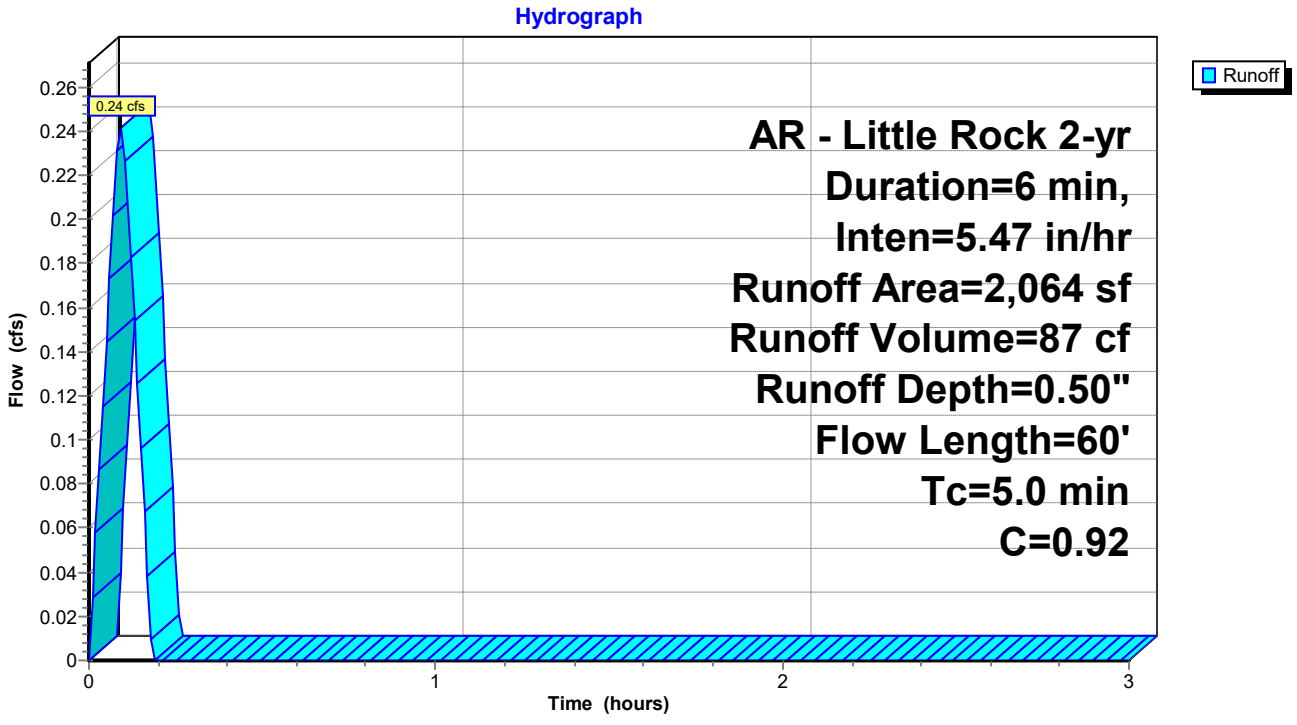
Runoff = 0.24 cfs @ 0.09 hrs, Volume= 87 cf, Depth= 0.50"
Routed to Pond CI-A2 : CURB INLET A2

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=6 min, Inten=5.47 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 0 | 0.35 | Sandy Soil 2-7% per manual |
| 2,064 | 0.92 | Paved Areas |
| 2,064 | 0.92 | Weighted Average |
| 2,064 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.6 | 45 | 0.0170 | 1.26 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.0 | 15 | 0.0840 | 5.88 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 4.4 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 60 | Total | | | |

## Subcatchment B4: Drainage Basin B4



## Summary for Subcatchment B5: Drainage Basin B5

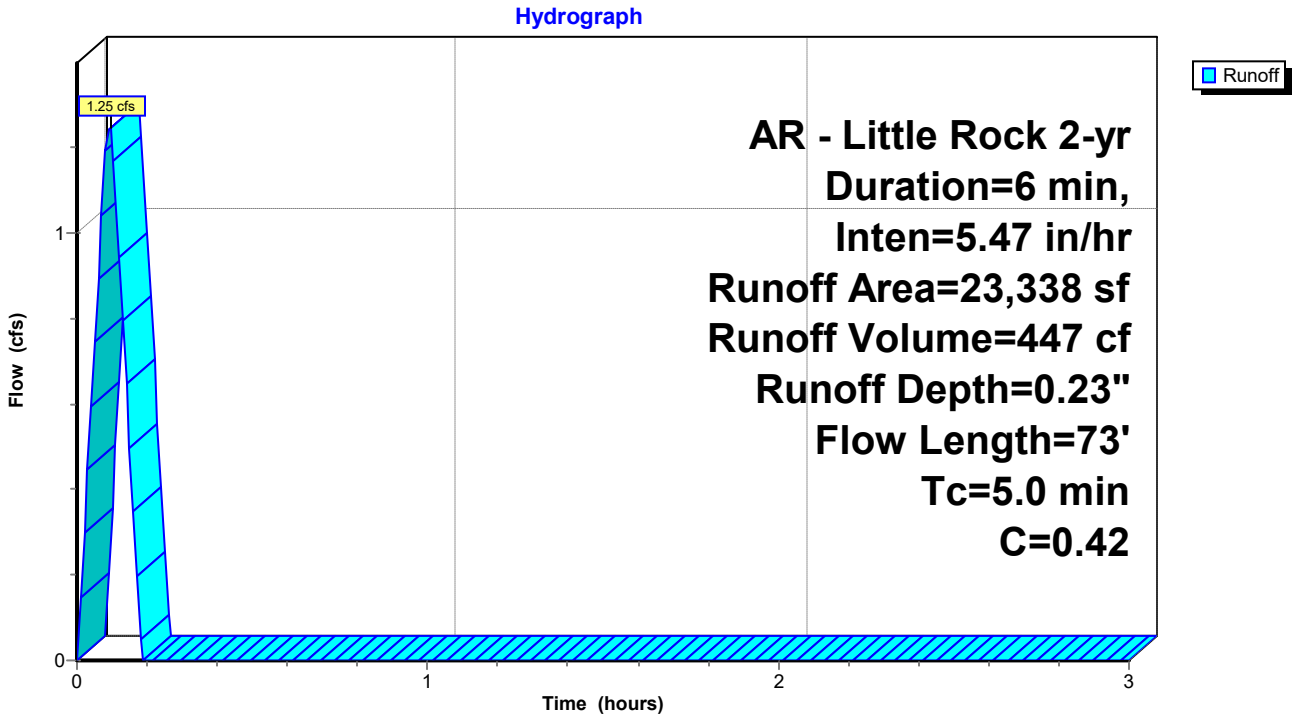
Runoff = 1.25 cfs @ 0.09 hrs, Volume= 447 cf, Depth= 0.23"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 2-yr Duration=6 min, Inten=5.47 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,627 | 0.35 | Sandy Soil 2-7% per manual |
| 2,711 | 0.92 | Paved Areas |
| 23,338 | 0.42 | Weighted Average |
| 23,338 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.1 | 18 | 0.1667 | 2.61 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 55 | 0.0860 | 2.05 | | **Shallow Concentrated Flow, Overland Concentrated** Short Grass Pasture Kv= 7.0 fps |
| 4.5 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 73 | Total | | | |

## Subcatchment B5: Drainage Basin B5



## Summary for Pond CI-A1: CURB INLET A1

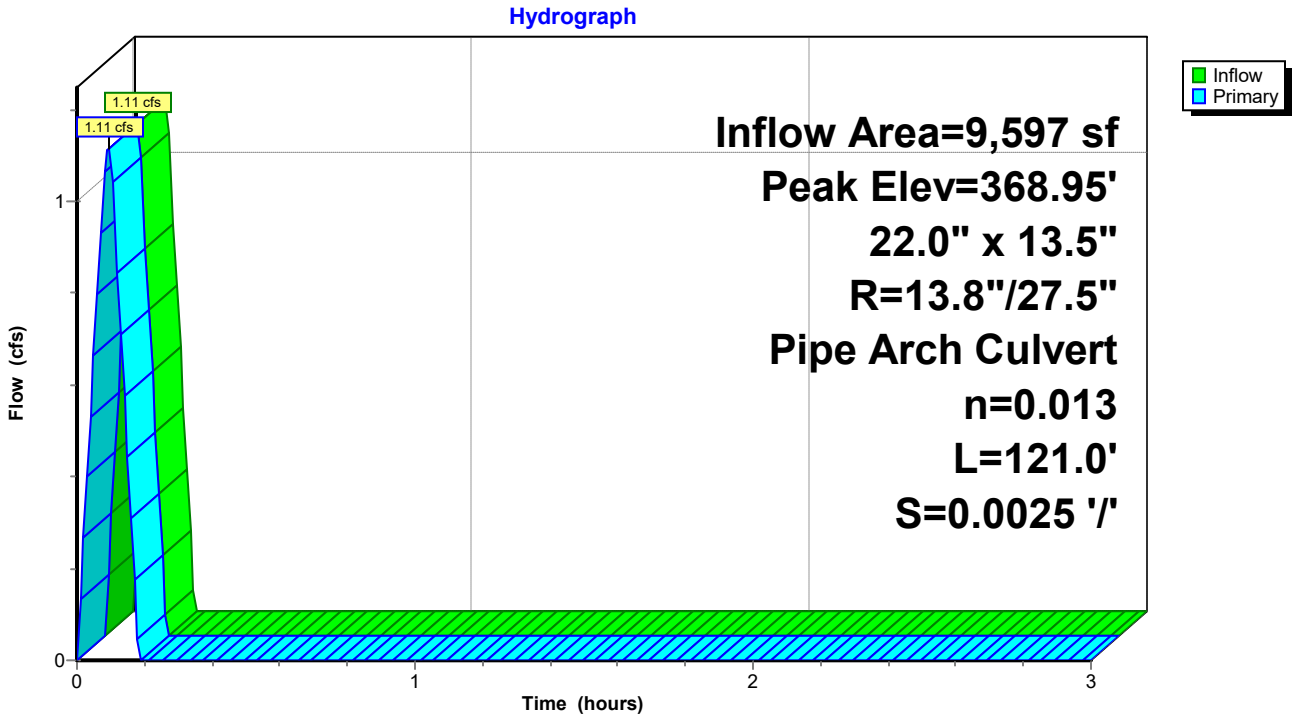
Inflow Area = 9,597 sf, 0.00% Impervious, Inflow Depth = 0.50" for 2-yr event
Inflow = 1.11 cfs @ 0.09 hrs, Volume= 398 cf
Outflow = 1.11 cfs @ 0.09 hrs, Volume= 398 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.11 cfs @ 0.09 hrs, Volume= 398 cf
Routed to Pond CI-A2 : CURB INLET A2

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 368.95' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **22.0" W x 13.5" H, R=13.8"/27.5" Pipe Arch RCP_Arch 22x14** L= 121.0' RCP, rounded edge headwall, Ke= 0.100 Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900 n= 0.013, Flow Area= 1.65 sf |

**Primary OutFlow** Max=1.11 cfs @ 0.09 hrs HW=368.95' (Free Discharge)
**1=RCP_Arch 22x14** (Barrel Controls 1.11 cfs @ 2.28 fps)

## Pond CI-A1: CURB INLET A1



## Summary for Pond CI-A2: CURB INLET A2

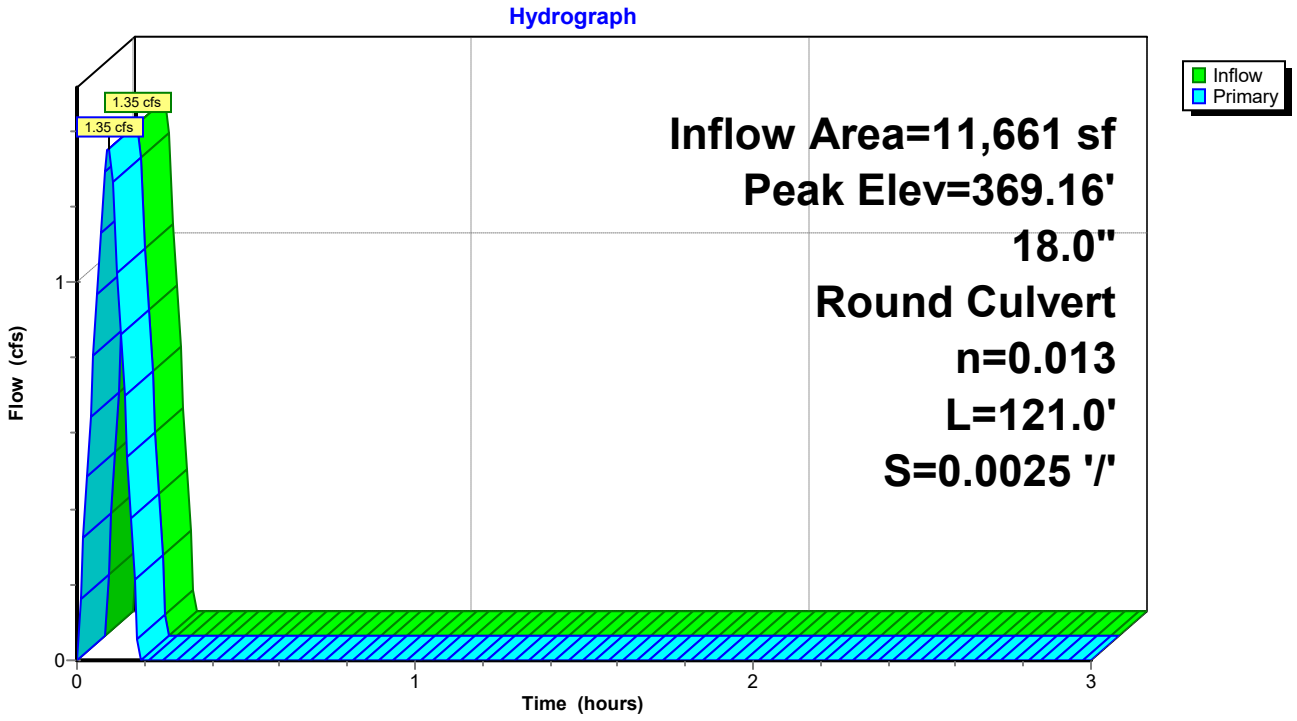
Inflow Area = 11,661 sf, 0.00% Impervious, Inflow Depth = 0.50" for 2-yr event
Inflow = 1.35 cfs @ 0.09 hrs, Volume= 485 cf
Outflow = 1.35 cfs @ 0.09 hrs, Volume= 485 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.35 cfs @ 0.09 hrs, Volume= 485 cf
Routed to Link POST-DEV : Post-Development

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.16' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **18.0" Round RCP_Round 18"**<br>L= 121.0' RCP, rounded edge headwall, Ke= 0.100<br>Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900<br>n= 0.013, Flow Area= 1.77 sf |

**Primary OutFlow** Max=1.35 cfs @ 0.09 hrs HW=369.16' (Free Discharge)
**1=RCP_Round 18"** (Barrel Controls 1.35 cfs @ 2.62 fps)

## Pond CI-A2: CURB INLET A2

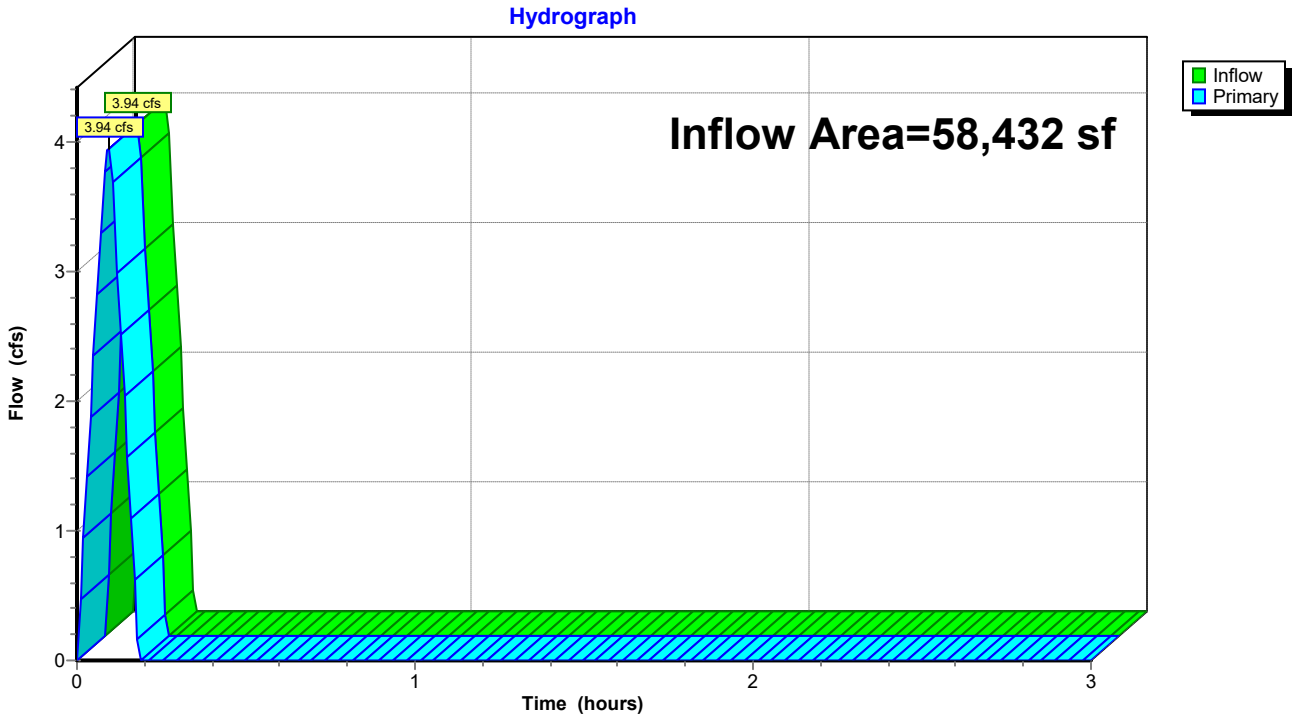


## Summary for Link POST-DEV: Post-Development

Inflow Area = 58,432 sf, 0.00% Impervious, Inflow Depth = 0.29" for 2-yr event
Inflow = 3.94 cfs @ 0.09 hrs, Volume= 1,413 cf
Primary = 3.94 cfs @ 0.09 hrs, Volume= 1,413 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link POST-DEV: Post-Development



## Summary for Subcatchment B1: Drainage Basin B1

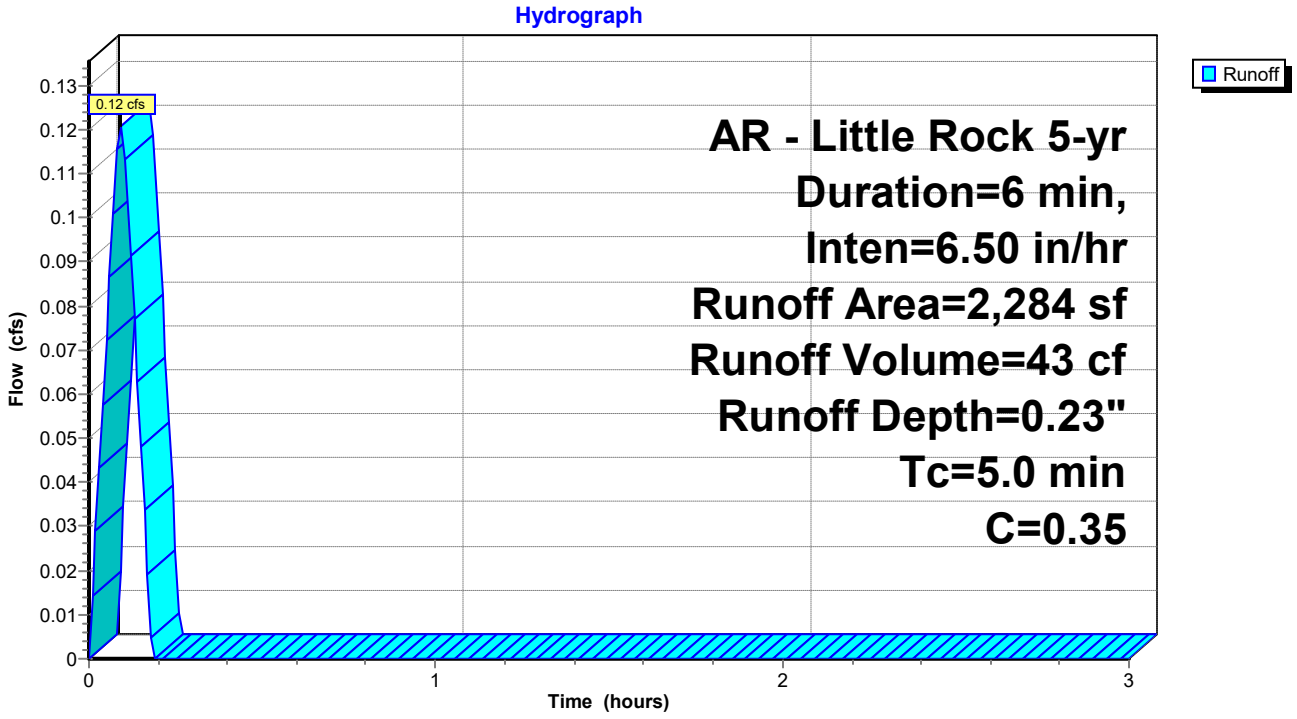
Runoff = 0.12 cfs @ 0.09 hrs, Volume= 43 cf, Depth= 0.23"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=6 min, Inten=6.50 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 2,284 | 0.35 | Sandy Soil 2-7% per manual |
| 0 | 0.92 | Paved Areas |
| 2,284 | 0.35 | Weighted Average |
| 2,284 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 5.0 | | | | | **Direct Entry, Minimum Adjustment** |

### Subcatchment B1: Drainage Basin B1



## Summary for Subcatchment B2: Drainage Basin B2

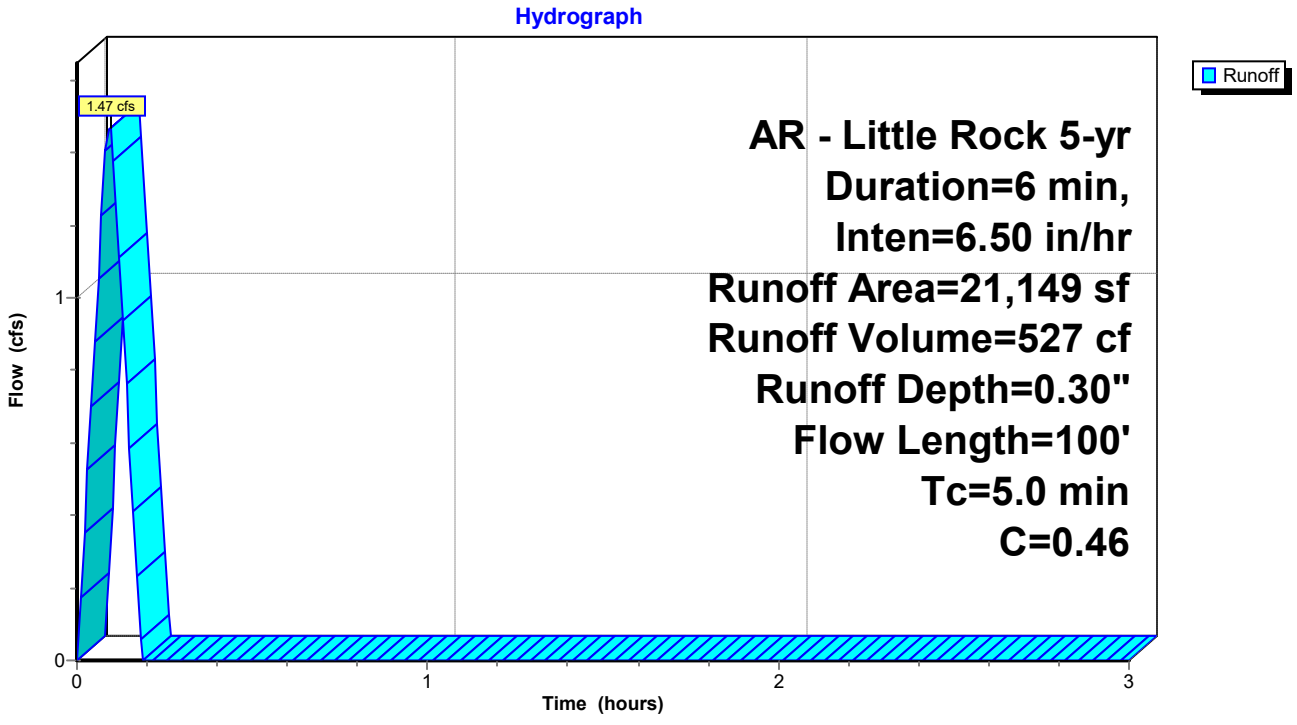
Runoff = 1.47 cfs @ 0.09 hrs, Volume= 527 cf, Depth= 0.30"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=6 min, Inten=6.50 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 16,931 | 0.35 | Sandy Soil 2-7% per manual |
| 4,218 | 0.92 | Paved Areas |
| 21,149 | 0.46 | Weighted Average |
| 21,149 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 42 | 0.1667 | 3.09 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.5 | 58 | 0.0500 | 2.04 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 4.3 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 100 | Total | | | |

## Subcatchment B2: Drainage Basin B2



## Summary for Subcatchment B3: Drainage Basin B3

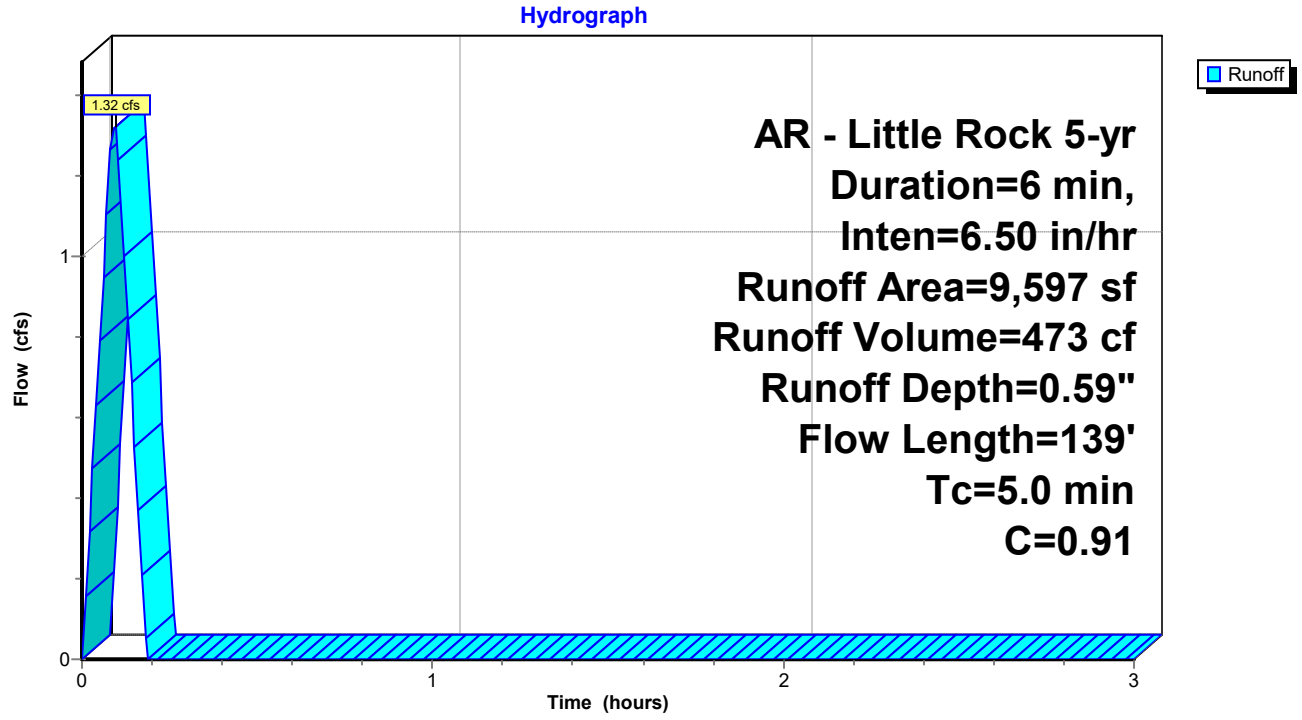
Runoff = 1.32 cfs @ 0.09 hrs, Volume= 473 cf, Depth= 0.59"
Routed to Pond CI-A1 : CURB INLET A1

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=6 min, Inten=6.50 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 155 | 0.35 | Sandy Soil 2-7% per manual |
| 9,442 | 0.92 | Paved Areas |
| 9,597 | 0.91 | Weighted Average |
| 9,597 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 28 | 0.1667 | 2.85 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 30 | 0.0160 | 1.13 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 41 | 0.0520 | 1.93 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.2 | 40 | 0.0360 | 3.85 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 3.8 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 139 | Total | | | |

## Subcatchment B3: Drainage Basin B3



## Summary for Subcatchment B4: Drainage Basin B4

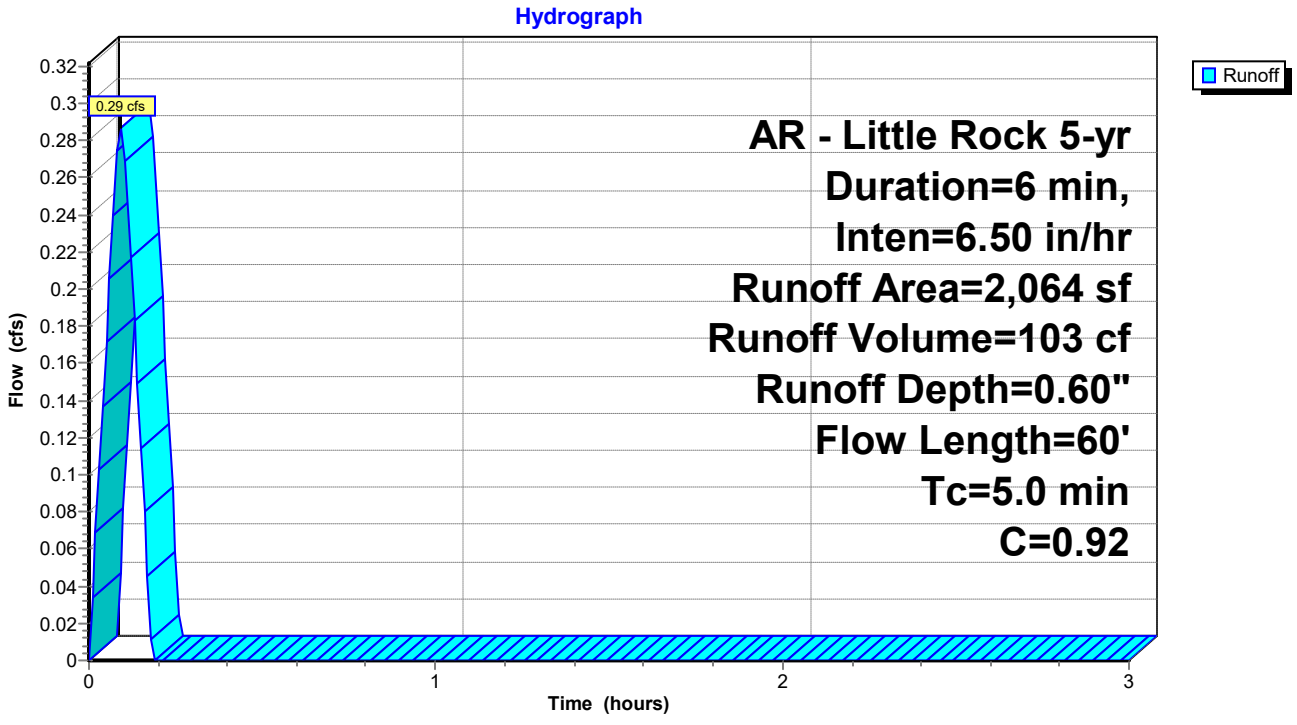
Runoff = 0.29 cfs @ 0.09 hrs, Volume= 103 cf, Depth= 0.60"
Routed to Pond CI-A2 : CURB INLET A2

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=6 min, Inten=6.50 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 0 | 0.35 | Sandy Soil 2-7% per manual |
| 2,064 | 0.92 | Paved Areas |
| 2,064 | 0.92 | Weighted Average |
| 2,064 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.6 | 45 | 0.0170 | 1.26 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.0 | 15 | 0.0840 | 5.88 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 4.4 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 60 | Total | | | |

## Subcatchment B4: Drainage Basin B4



## Summary for Subcatchment B5: Drainage Basin B5

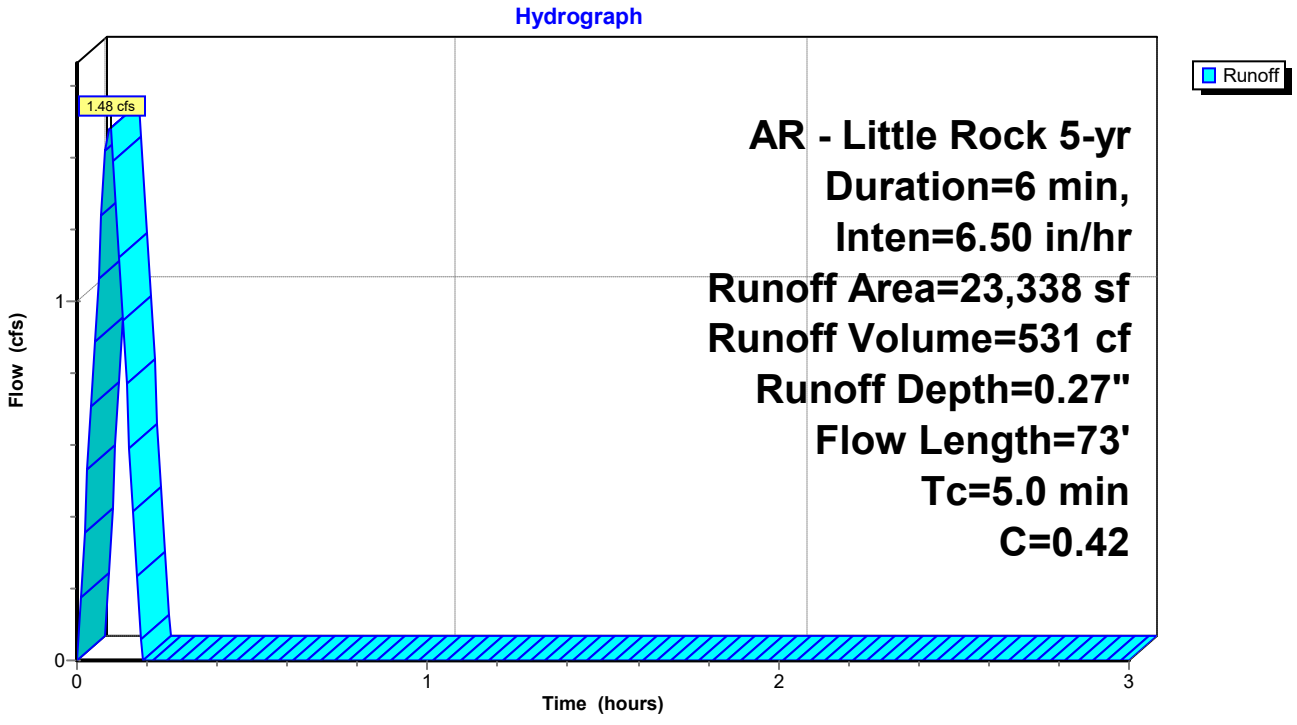
Runoff = 1.48 cfs @ 0.09 hrs, Volume= 531 cf, Depth= 0.27"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 5-yr Duration=6 min, Inten=6.50 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,627 | 0.35 | Sandy Soil 2-7% per manual |
| 2,711 | 0.92 | Paved Areas |
| 23,338 | 0.42 | Weighted Average |
| 23,338 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.1 | 18 | 0.1667 | 2.61 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 55 | 0.0860 | 2.05 | | **Shallow Concentrated Flow, Overland Concentrated** Short Grass Pasture Kv= 7.0 fps |
| 4.5 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 73 | Total | | | |

## Subcatchment B5: Drainage Basin B5



## Summary for Pond CI-A1: CURB INLET A1

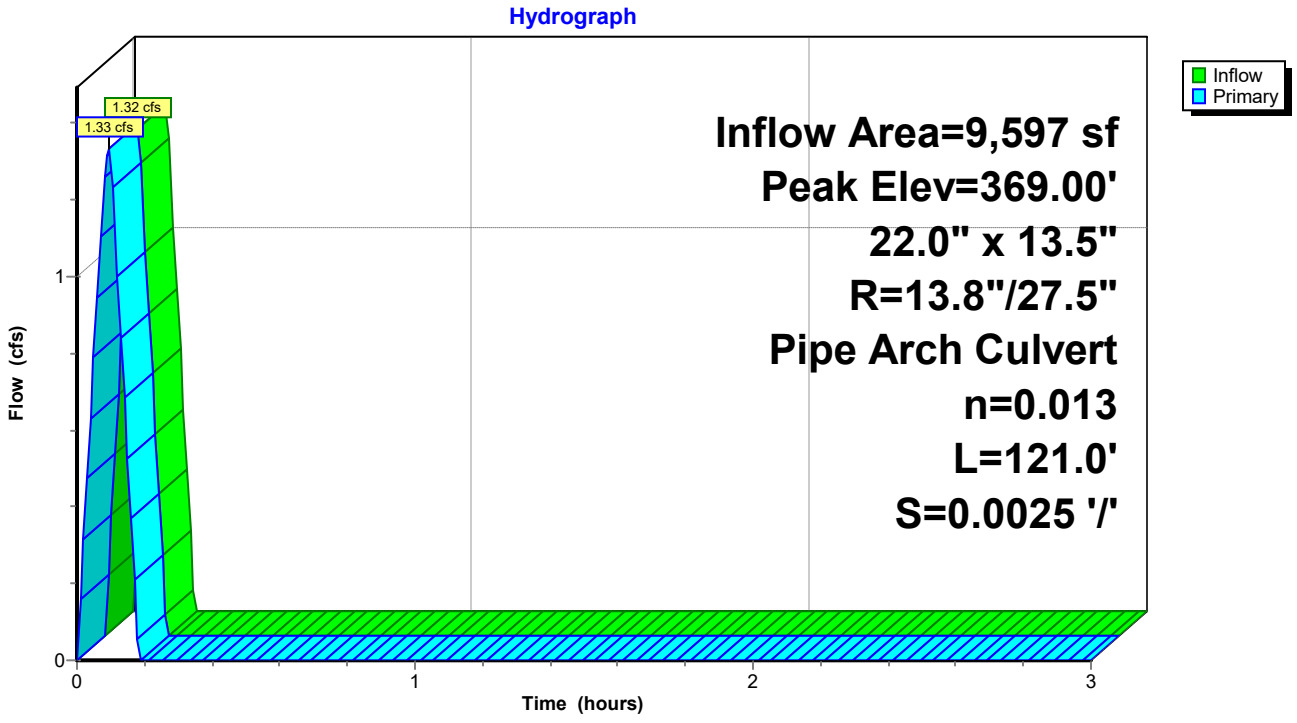
Inflow Area = 9,597 sf, 0.00% Impervious, Inflow Depth = 0.59" for 5-yr event
Inflow = 1.32 cfs @ 0.09 hrs, Volume= 473 cf
Outflow = 1.33 cfs @ 0.10 hrs, Volume= 473 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.33 cfs @ 0.10 hrs, Volume= 473 cf
Routed to Pond CI-A2 : CURB INLET A2

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.00' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **22.0" W x 13.5" H, R=13.8"/27.5" Pipe Arch RCP_Arch 22x14** L= 121.0' RCP, rounded edge headwall, Ke= 0.100 Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900 n= 0.013, Flow Area= 1.65 sf |

**Primary OutFlow** Max=1.31 cfs @ 0.10 hrs HW=369.00' (Free Discharge)
**1=RCP_Arch 22x14** (Barrel Controls 1.31 cfs @ 2.41 fps)

## Pond CI-A1: CURB INLET A1



## Summary for Pond CI-A2: CURB INLET A2

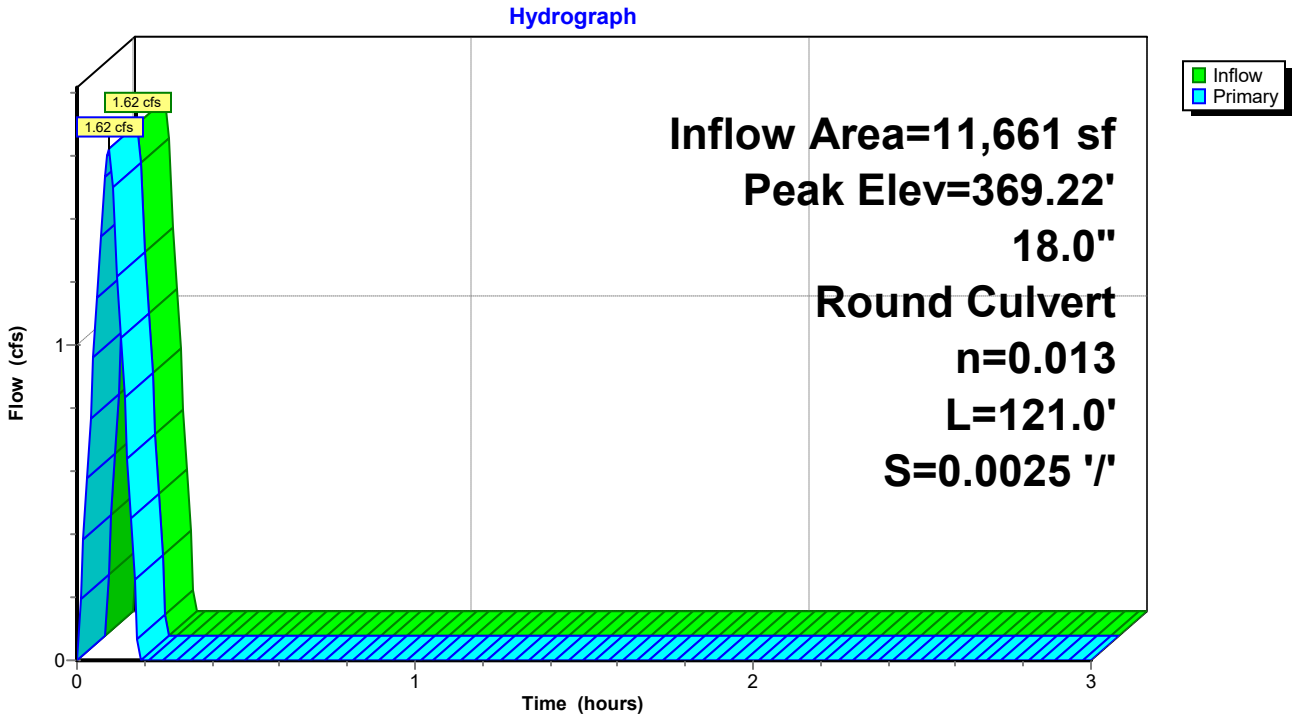
Inflow Area = 11,661 sf, 0.00% Impervious, Inflow Depth = 0.59" for 5-yr event
Inflow = 1.62 cfs @ 0.10 hrs, Volume= 576 cf
Outflow = 1.62 cfs @ 0.10 hrs, Volume= 576 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.62 cfs @ 0.10 hrs, Volume= 576 cf
Routed to Link POST-DEV : Post-Development

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.22' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **18.0" Round RCP_Round 18"**<br>L= 121.0' RCP, rounded edge headwall, Ke= 0.100<br>Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900<br>n= 0.013, Flow Area= 1.77 sf |

**Primary OutFlow** Max=1.60 cfs @ 0.10 hrs HW=369.22' (Free Discharge)
**1=RCP_Round 18"** (Barrel Controls 1.60 cfs @ 2.75 fps)

## Pond CI-A2: CURB INLET A2

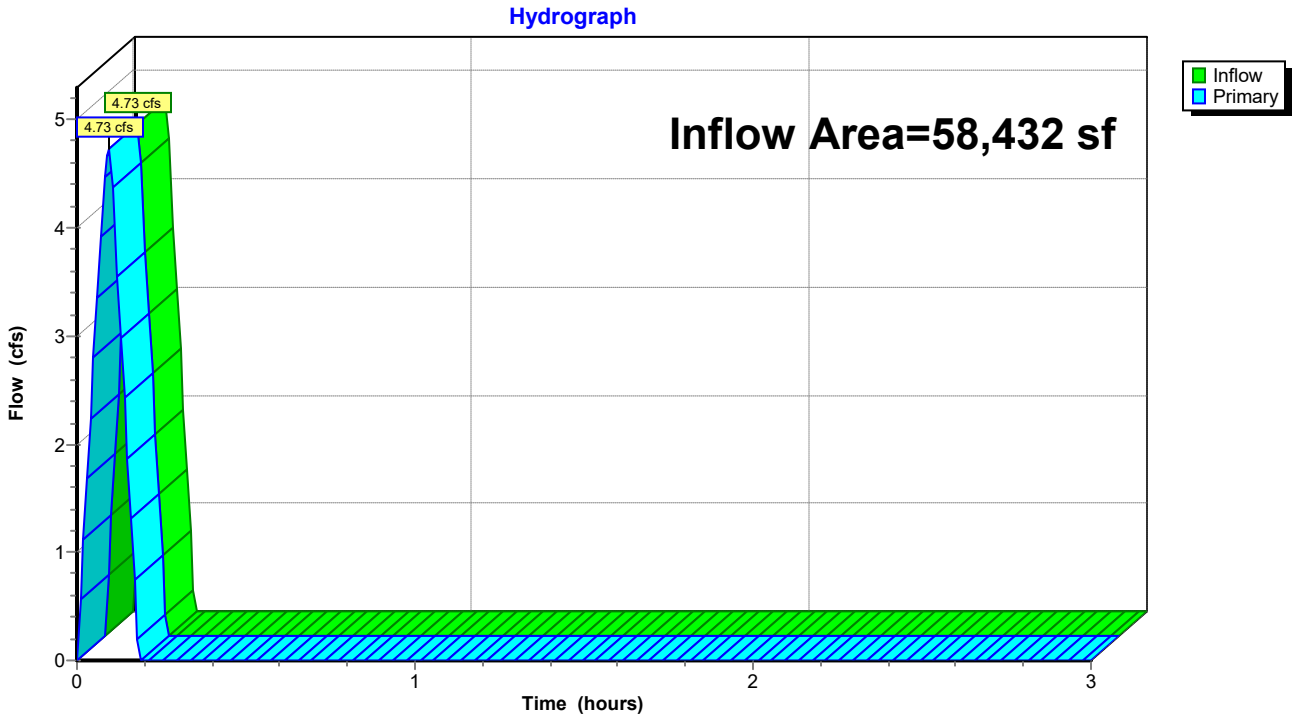


## Summary for Link POST-DEV: Post-Development

Inflow Area = 58,432 sf, 0.00% Impervious, Inflow Depth = 0.34" for 5-yr event
Inflow = 4.73 cfs @ 0.10 hrs, Volume= 1,678 cf
Primary = 4.73 cfs @ 0.10 hrs, Volume= 1,678 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link POST-DEV: Post-Development



## Summary for Subcatchment B1: Drainage Basin B1

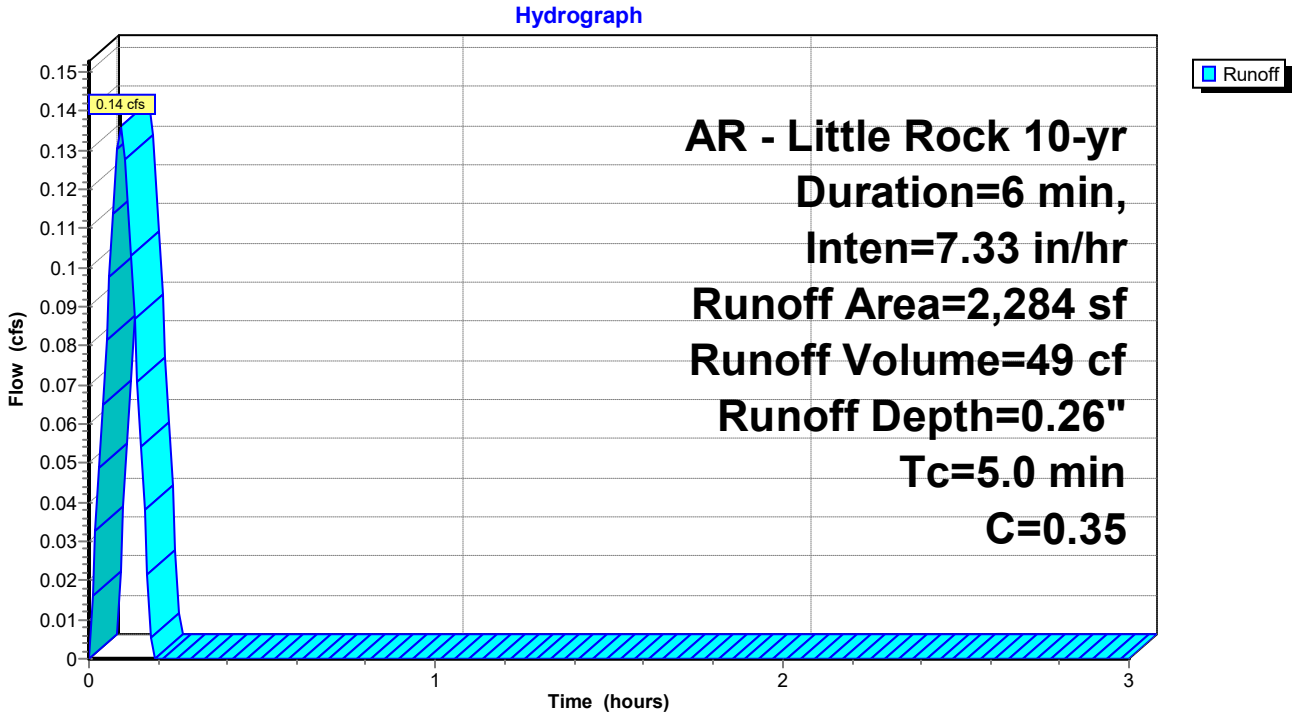
Runoff = 0.14 cfs @ 0.09 hrs, Volume= 49 cf, Depth= 0.26"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=6 min, Inten=7.33 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 2,284 | 0.35 | Sandy Soil 2-7% per manual |
| 0 | 0.92 | Paved Areas |
| 2,284 | 0.35 | Weighted Average |
| 2,284 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 5.0 | | | | | **Direct Entry, Minimum Adjustment** |

### Subcatchment B1: Drainage Basin B1



## Summary for Subcatchment B2: Drainage Basin B2

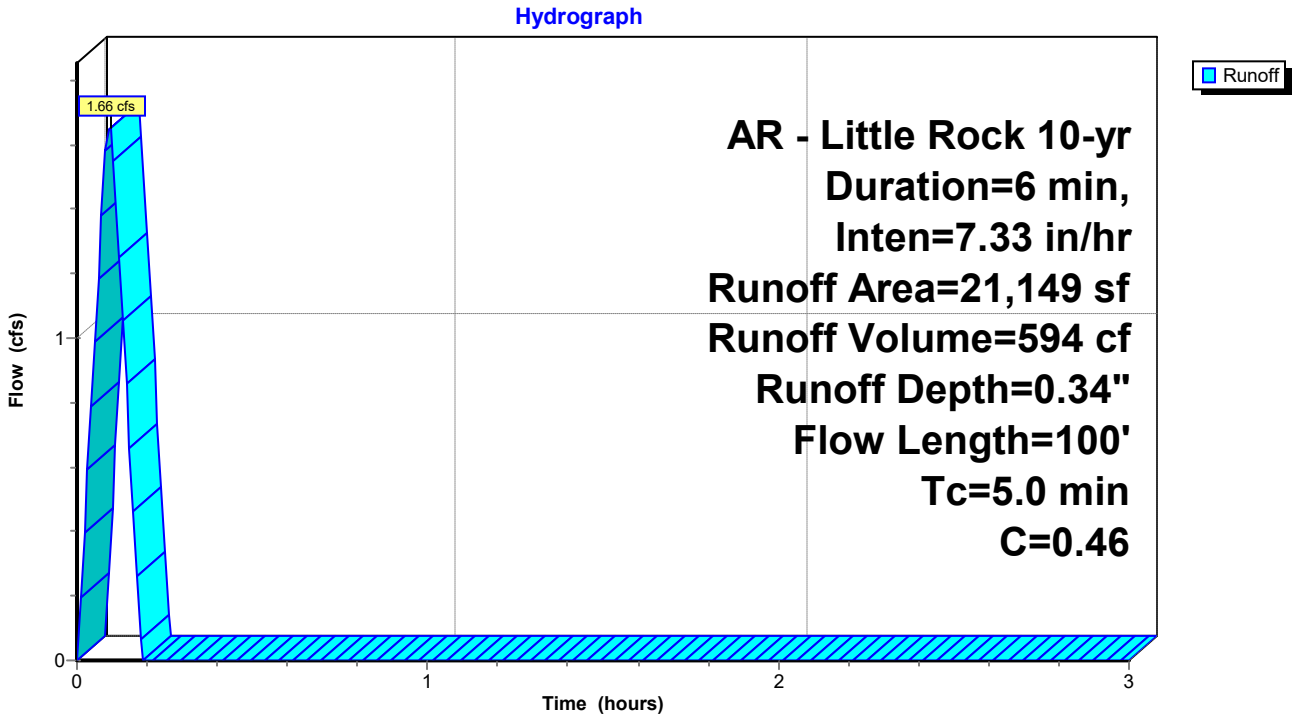
Runoff = 1.66 cfs @ 0.09 hrs, Volume= 594 cf, Depth= 0.34"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=6 min, Inten=7.33 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 16,931 | 0.35 | Sandy Soil 2-7% per manual |
| 4,218 | 0.92 | Paved Areas |
| 21,149 | 0.46 | Weighted Average |
| 21,149 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 42 | 0.1667 | 3.09 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.5 | 58 | 0.0500 | 2.04 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 4.3 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 100 | Total | | | |

## Subcatchment B2: Drainage Basin B2



## Summary for Subcatchment B3: Drainage Basin B3

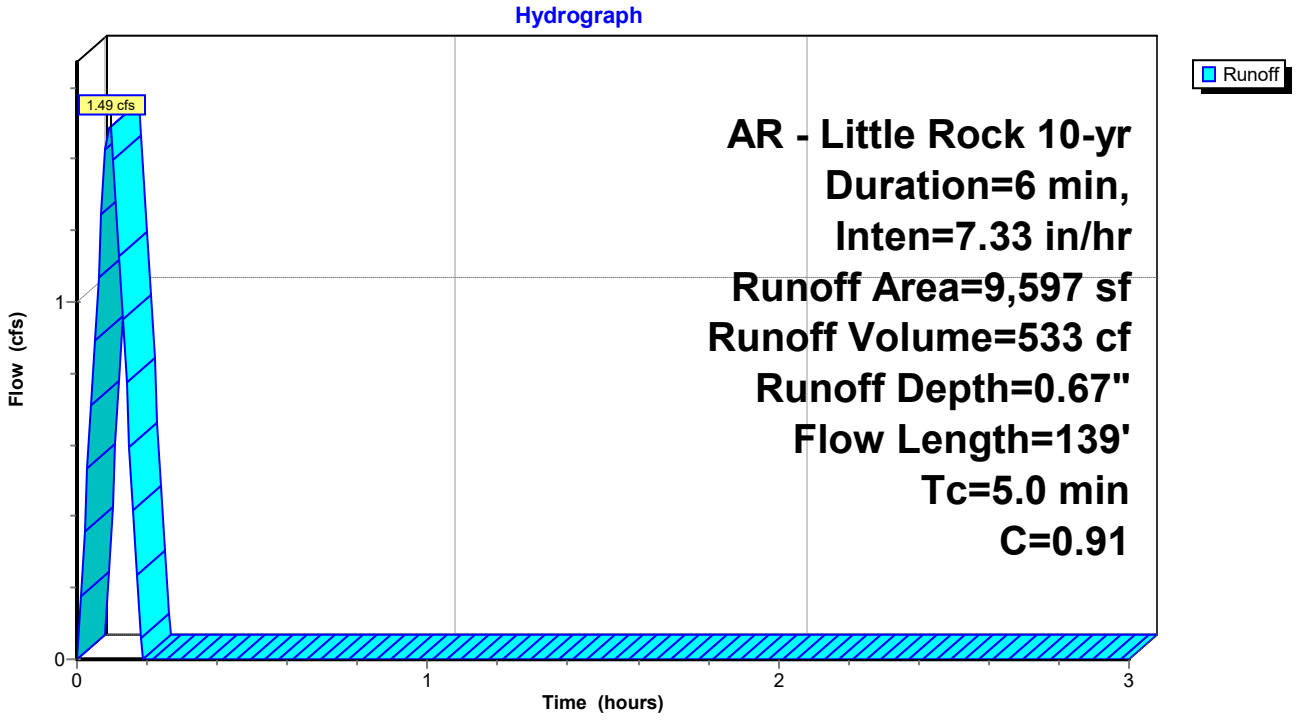
Runoff = 1.49 cfs @ 0.10 hrs, Volume= 533 cf, Depth= 0.67"
Routed to Pond CI-A1 : CURB INLET A1

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=6 min, Inten=7.33 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 155 | 0.35 | Sandy Soil 2-7% per manual |
| 9,442 | 0.92 | Paved Areas |
| 9,597 | 0.91 | Weighted Average |
| 9,597 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 28 | 0.1667 | 2.85 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 30 | 0.0160 | 1.13 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 41 | 0.0520 | 1.93 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.2 | 40 | 0.0360 | 3.85 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 3.8 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 139 | Total | | | |

## Subcatchment B3: Drainage Basin B3



## Summary for Subcatchment B4: Drainage Basin B4

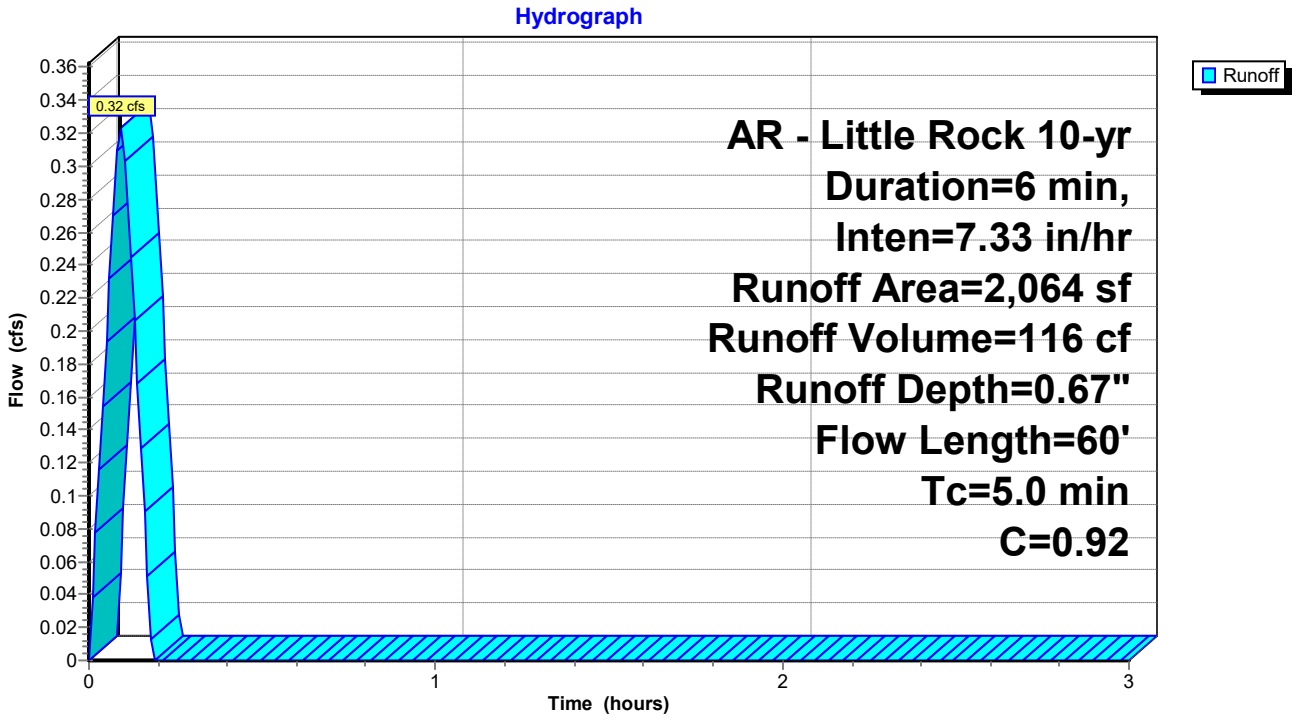
Runoff = 0.32 cfs @ 0.09 hrs, Volume= 116 cf, Depth= 0.67"
Routed to Pond CI-A2 : CURB INLET A2

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=6 min, Inten=7.33 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 0 | 0.35 | Sandy Soil 2-7% per manual |
| 2,064 | 0.92 | Paved Areas |
| 2,064 | 0.92 | Weighted Average |
| 2,064 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.6 | 45 | 0.0170 | 1.26 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.0 | 15 | 0.0840 | 5.88 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 4.4 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 60 | Total | | | |

## Subcatchment B4: Drainage Basin B4



## Summary for Subcatchment B5: Drainage Basin B5

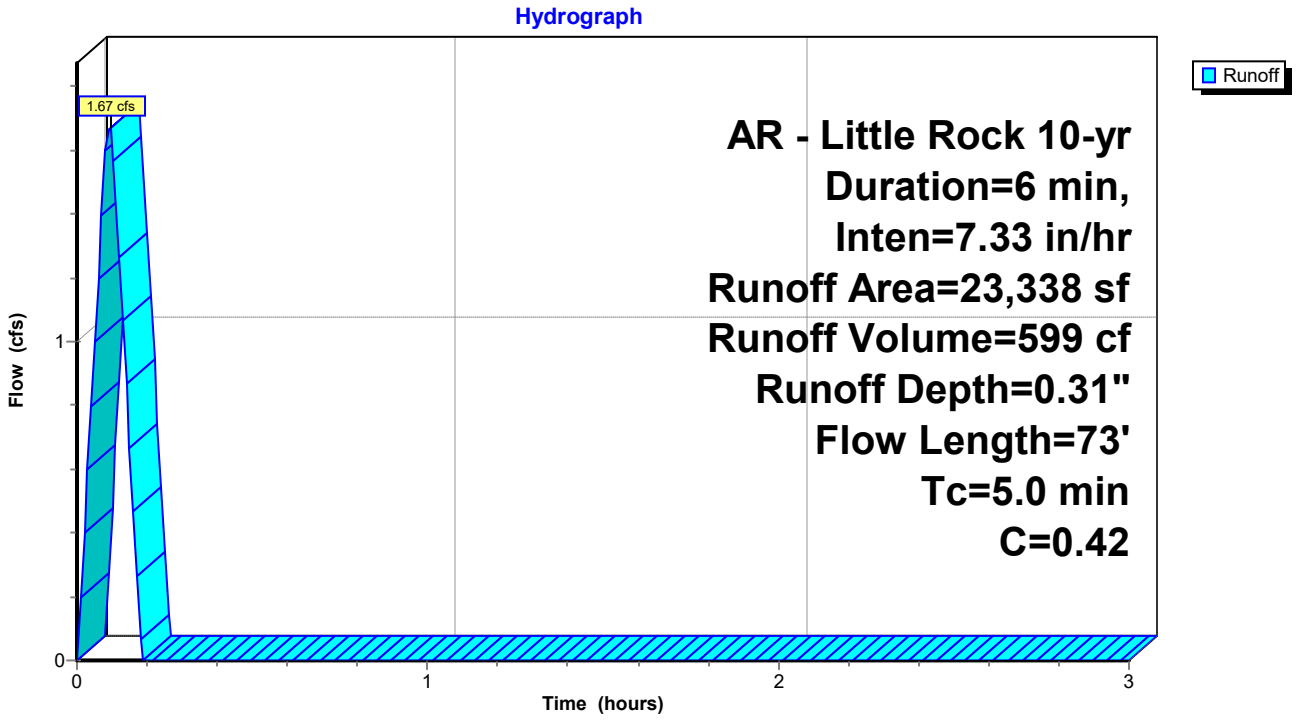
Runoff = 1.67 cfs @ 0.10 hrs, Volume= 599 cf, Depth= 0.31"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 10-yr Duration=6 min, Inten=7.33 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,627 | 0.35 | Sandy Soil 2-7% per manual |
| 2,711 | 0.92 | Paved Areas |
| 23,338 | 0.42 | Weighted Average |
| 23,338 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.1 | 18 | 0.1667 | 2.61 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 55 | 0.0860 | 2.05 | | **Shallow Concentrated Flow, Overland Concentrated** Short Grass Pasture Kv= 7.0 fps |
| 4.5 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 73 | Total | | | |

## Subcatchment B5: Drainage Basin B5



## Summary for Pond CI-A1: CURB INLET A1

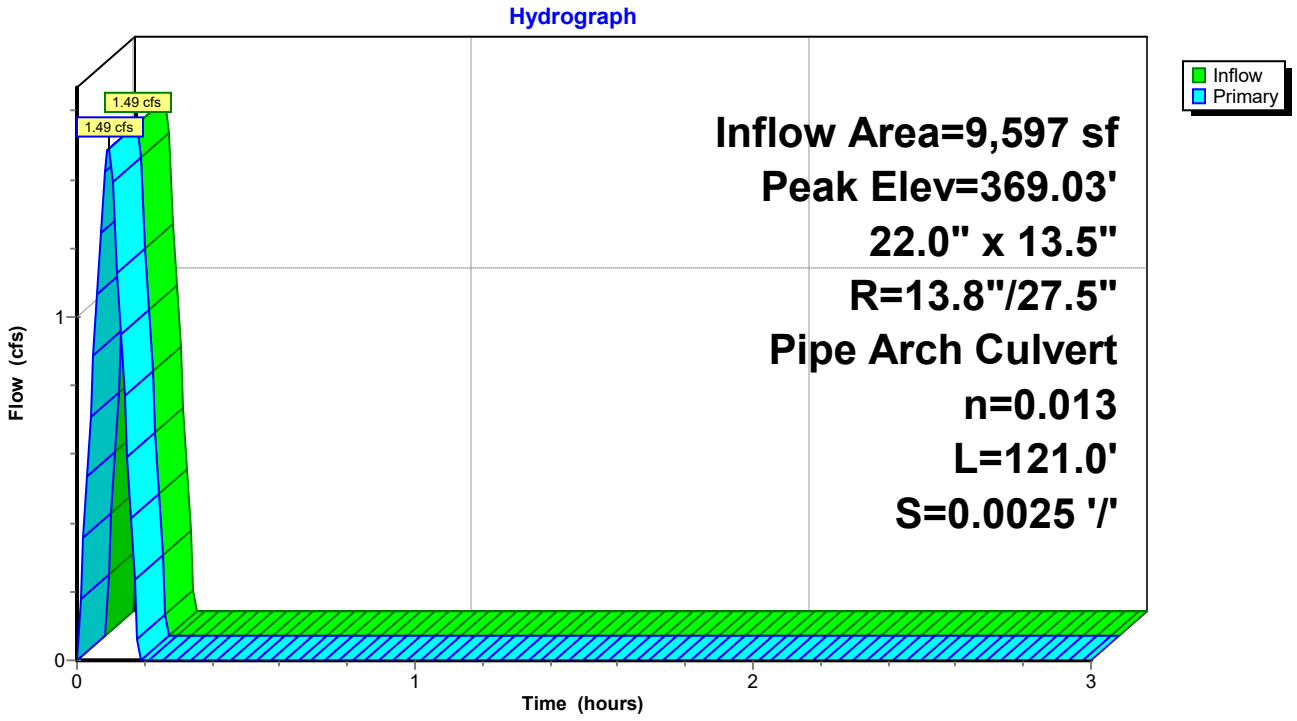
Inflow Area = 9,597 sf, 0.00% Impervious, Inflow Depth = 0.67" for 10-yr event
Inflow = 1.49 cfs @ 0.10 hrs, Volume= 533 cf
Outflow = 1.49 cfs @ 0.09 hrs, Volume= 533 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.49 cfs @ 0.09 hrs, Volume= 533 cf
Routed to Pond CI-A2 : CURB INLET A2

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.03' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **22.0" W x 13.5" H, R=13.8"/27.5" Pipe Arch RCP_Arch 22x14** L= 121.0' RCP, rounded edge headwall, Ke= 0.100 Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900 n= 0.013, Flow Area= 1.65 sf |

**Primary OutFlow** Max=1.48 cfs @ 0.09 hrs HW=369.03' (Free Discharge)
**1=RCP_Arch 22x14** (Barrel Controls 1.48 cfs @ 2.51 fps)

## Pond CI-A1: CURB INLET A1



## Summary for Pond CI-A2: CURB INLET A2

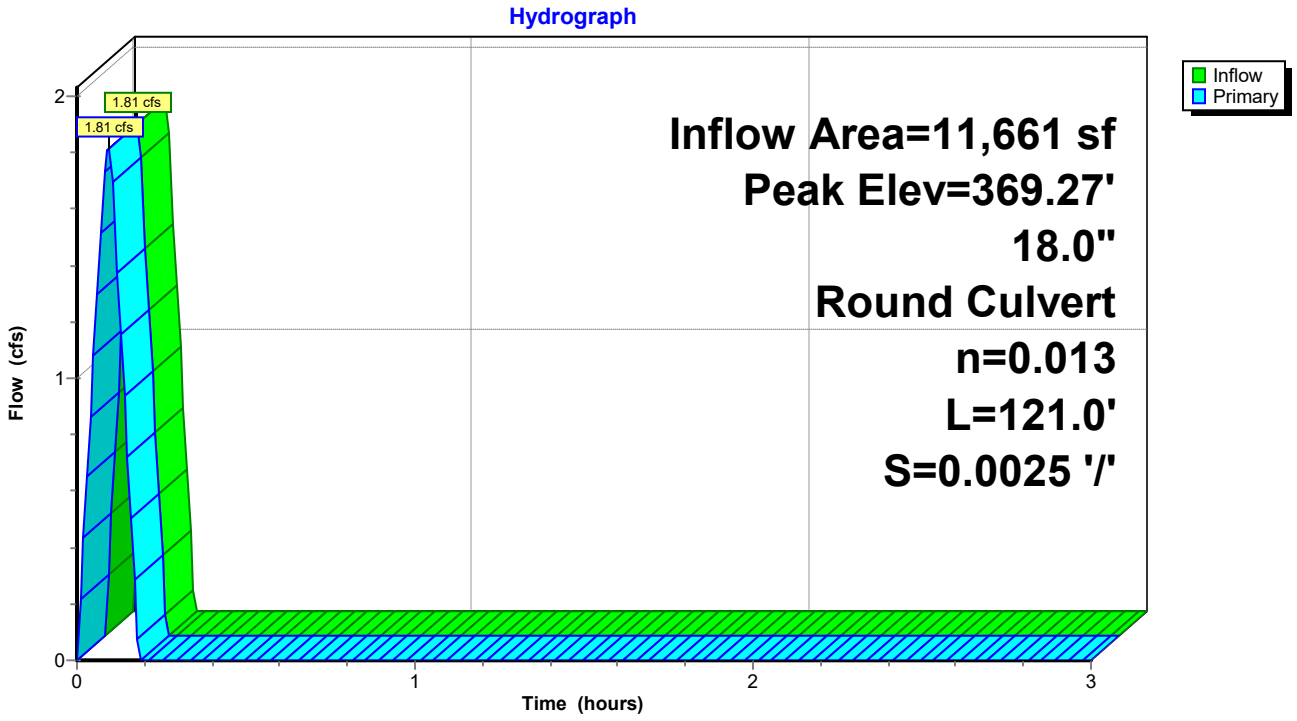
Inflow Area = 11,661 sf, 0.00% Impervious, Inflow Depth = 0.67" for 10-yr event
Inflow = 1.81 cfs @ 0.09 hrs, Volume= 649 cf
Outflow = 1.81 cfs @ 0.09 hrs, Volume= 649 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.81 cfs @ 0.09 hrs, Volume= 649 cf
Routed to Link POST-DEV : Post-Development

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.27' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **18.0" Round RCP_Round 18"**<br>L= 121.0' RCP, rounded edge headwall, Ke= 0.100<br>Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900<br>n= 0.013, Flow Area= 1.77 sf |

**Primary OutFlow** Max=1.80 cfs @ 0.09 hrs HW=369.26' (Free Discharge)
**1=RCP_Round 18"** (Barrel Controls 1.80 cfs @ 2.85 fps)

## Pond CI-A2: CURB INLET A2

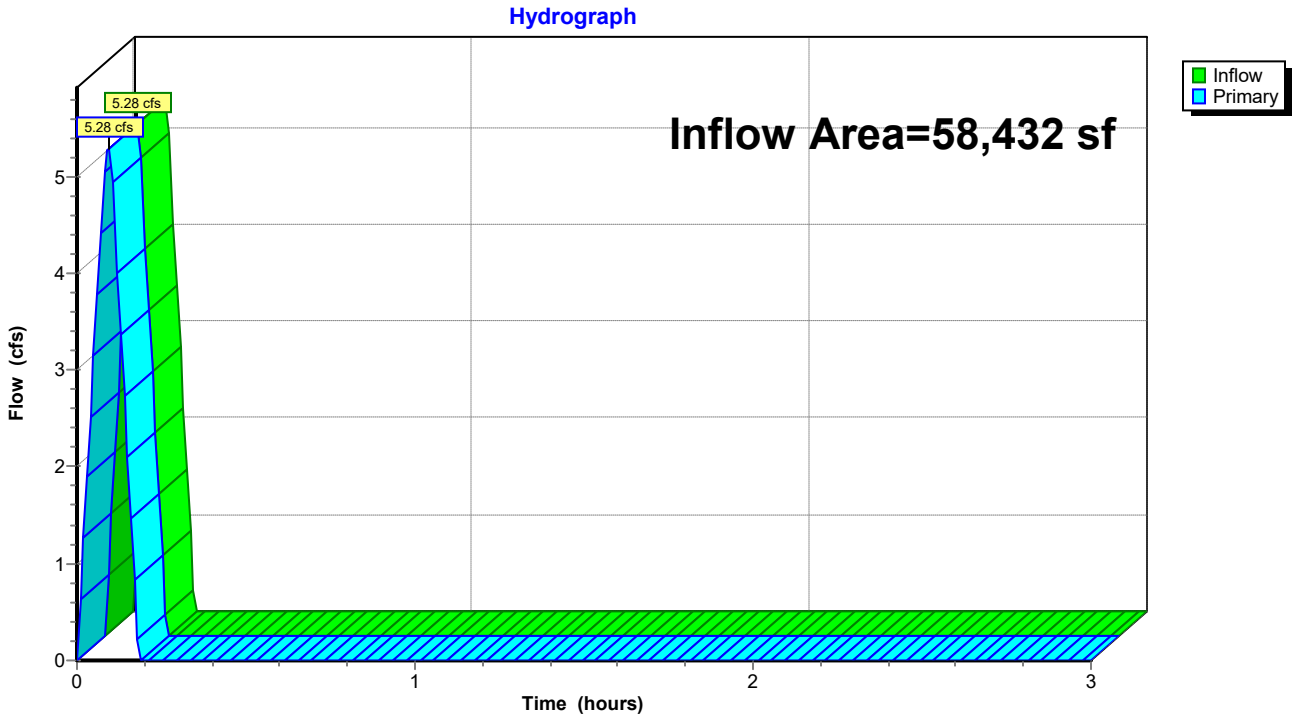


## Summary for Link POST-DEV: Post-Development

Inflow Area = 58,432 sf, 0.00% Impervious, Inflow Depth = 0.39" for 10-yr event
Inflow = 5.28 cfs @ 0.09 hrs, Volume= 1,891 cf
Primary = 5.28 cfs @ 0.09 hrs, Volume= 1,891 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link POST-DEV: Post-Development



## Summary for Subcatchment B1: Drainage Basin B1

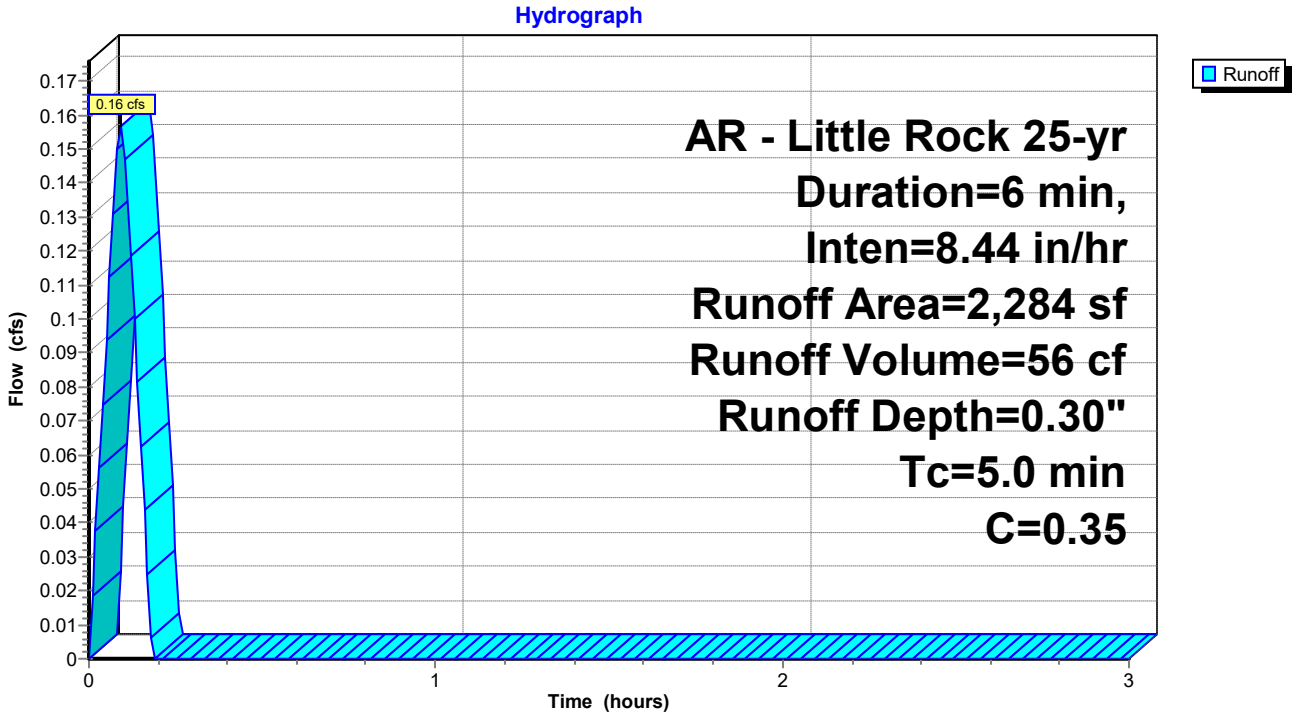
Runoff = 0.16 cfs @ 0.09 hrs, Volume= 56 cf, Depth= 0.30"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=6 min, Inten=8.44 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 2,284 | 0.35 | Sandy Soil 2-7% per manual |
| 0 | 0.92 | Paved Areas |
| 2,284 | 0.35 | Weighted Average |
| 2,284 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 5.0 | | | | | **Direct Entry, Minimum Adjustment** |

### Subcatchment B1: Drainage Basin B1



## Summary for Subcatchment B2: Drainage Basin B2

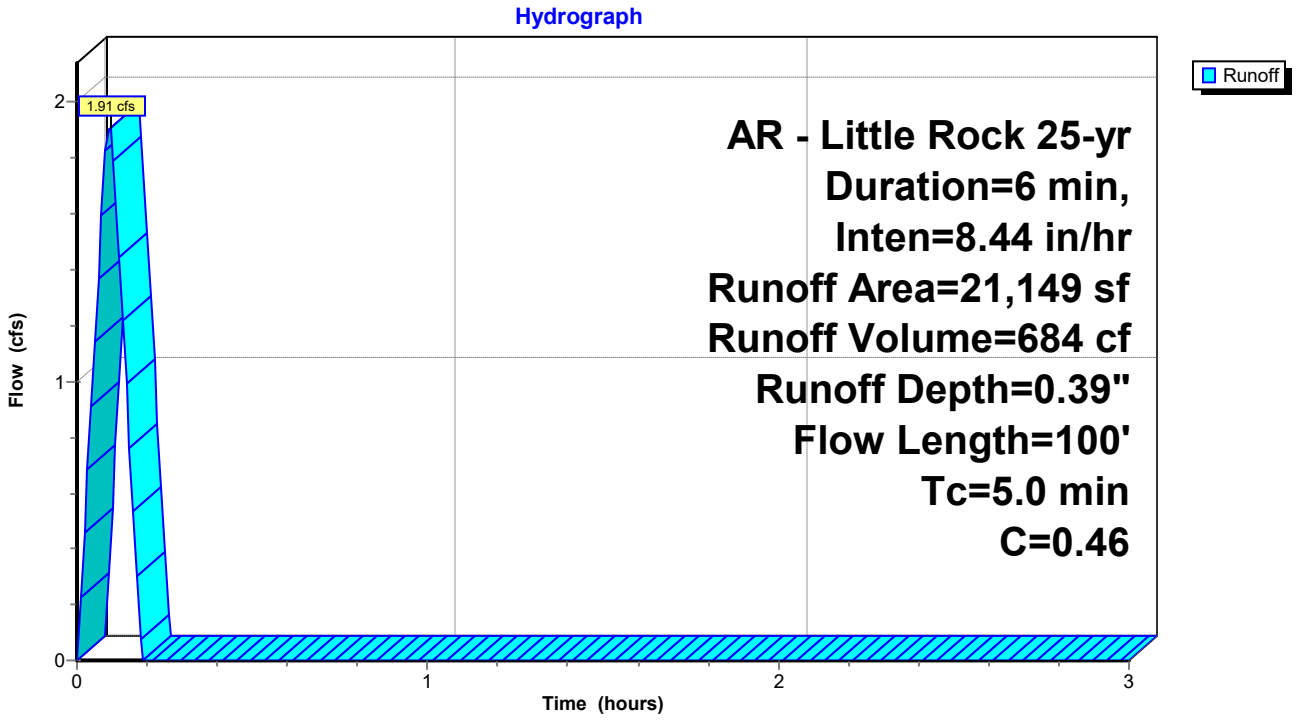
Runoff = 1.91 cfs @ 0.09 hrs, Volume= 684 cf, Depth= 0.39"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=6 min, Inten=8.44 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 16,931 | 0.35 | Sandy Soil 2-7% per manual |
| 4,218 | 0.92 | Paved Areas |
| 21,149 | 0.46 | Weighted Average |
| 21,149 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 42 | 0.1667 | 3.09 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.5 | 58 | 0.0500 | 2.04 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 4.3 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 100 | Total | | | |

## Subcatchment B2: Drainage Basin B2



## Summary for Subcatchment B3: Drainage Basin B3

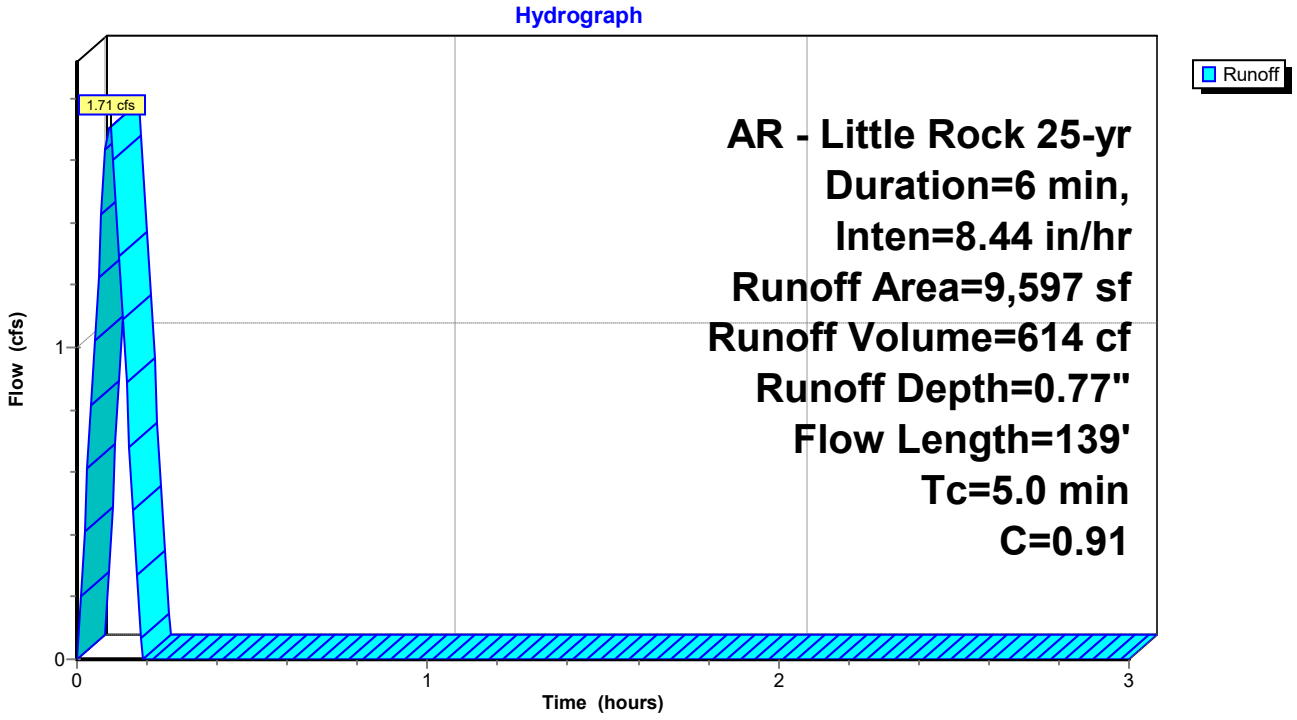
Runoff = 1.71 cfs @ 0.09 hrs, Volume= 614 cf, Depth= 0.77"
Routed to Pond CI-A1 : CURB INLET A1

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=6 min, Inten=8.44 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 155 | 0.35 | Sandy Soil 2-7% per manual |
| 9,442 | 0.92 | Paved Areas |
| 9,597 | 0.91 | Weighted Average |
| 9,597 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 28 | 0.1667 | 2.85 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 30 | 0.0160 | 1.13 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 41 | 0.0520 | 1.93 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.2 | 40 | 0.0360 | 3.85 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 3.8 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 139 | Total | | | |

## Subcatchment B3: Drainage Basin B3



## Summary for Subcatchment B4: Drainage Basin B4

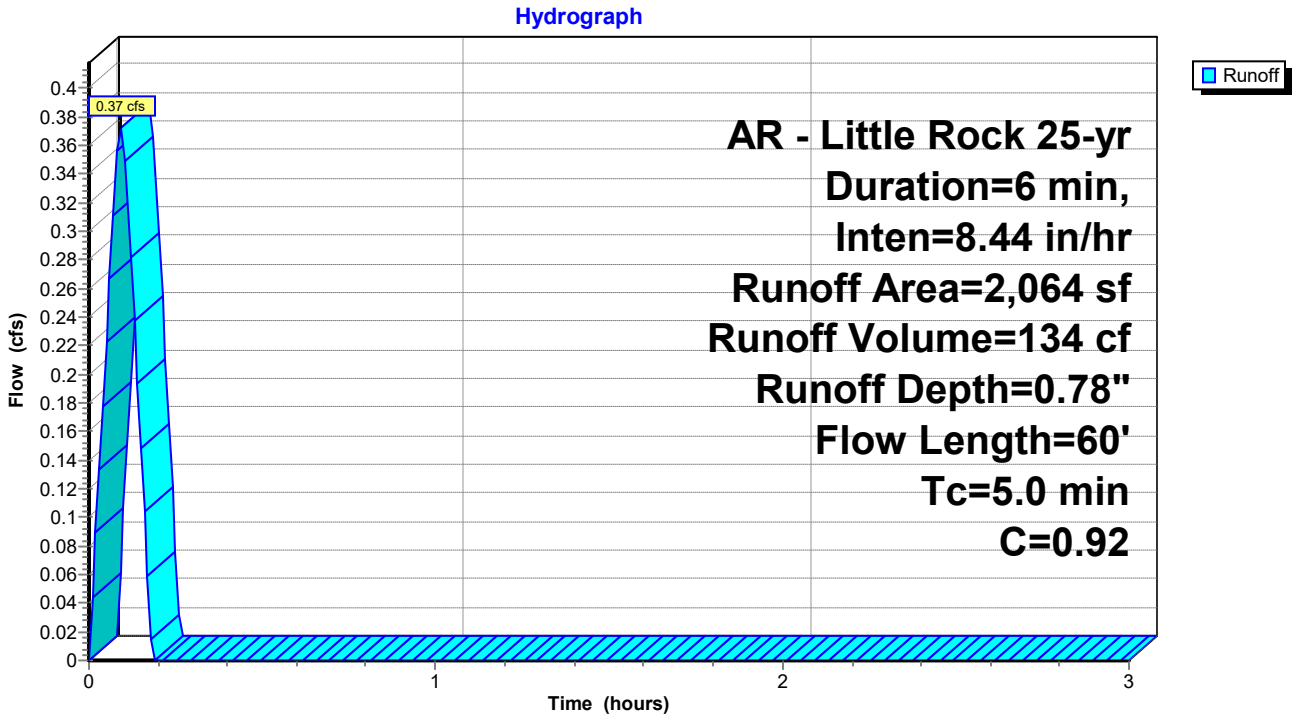
Runoff = 0.37 cfs @ 0.09 hrs, Volume= 134 cf, Depth= 0.78"
Routed to Pond CI-A2 : CURB INLET A2

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=6 min, Inten=8.44 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 0 | 0.35 | Sandy Soil 2-7% per manual |
| 2,064 | 0.92 | Paved Areas |
| 2,064 | 0.92 | Weighted Average |
| 2,064 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.6 | 45 | 0.0170 | 1.26 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.0 | 15 | 0.0840 | 5.88 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 4.4 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 60 | Total | | | |

## Subcatchment B4: Drainage Basin B4



## Summary for Subcatchment B5: Drainage Basin B5

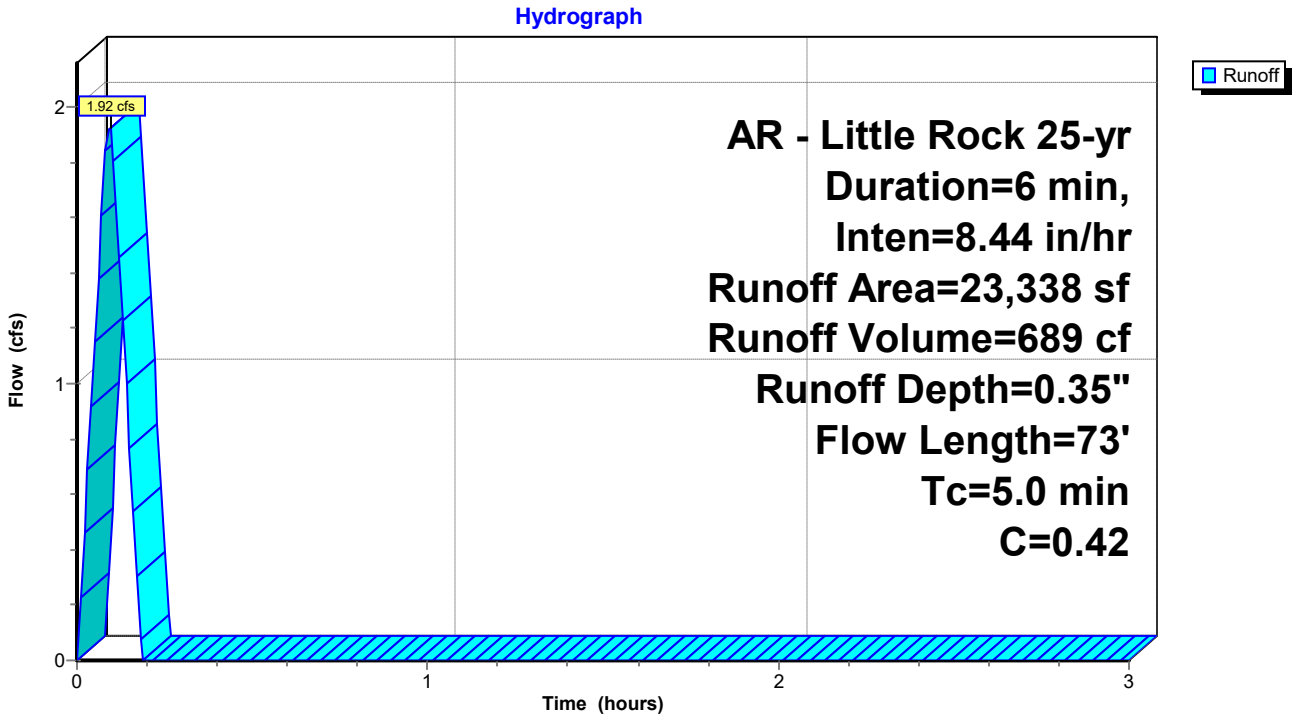
Runoff = 1.92 cfs @ 0.09 hrs, Volume= 689 cf, Depth= 0.35"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 25-yr Duration=6 min, Inten=8.44 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,627 | 0.35 | Sandy Soil 2-7% per manual |
| 2,711 | 0.92 | Paved Areas |
| 23,338 | 0.42 | Weighted Average |
| 23,338 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.1 | 18 | 0.1667 | 2.61 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 55 | 0.0860 | 2.05 | | **Shallow Concentrated Flow, Overland Concentrated** Short Grass Pasture Kv= 7.0 fps |
| 4.5 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 73 | Total | | | |

## Subcatchment B5: Drainage Basin B5



## Summary for Pond CI-A1: CURB INLET A1

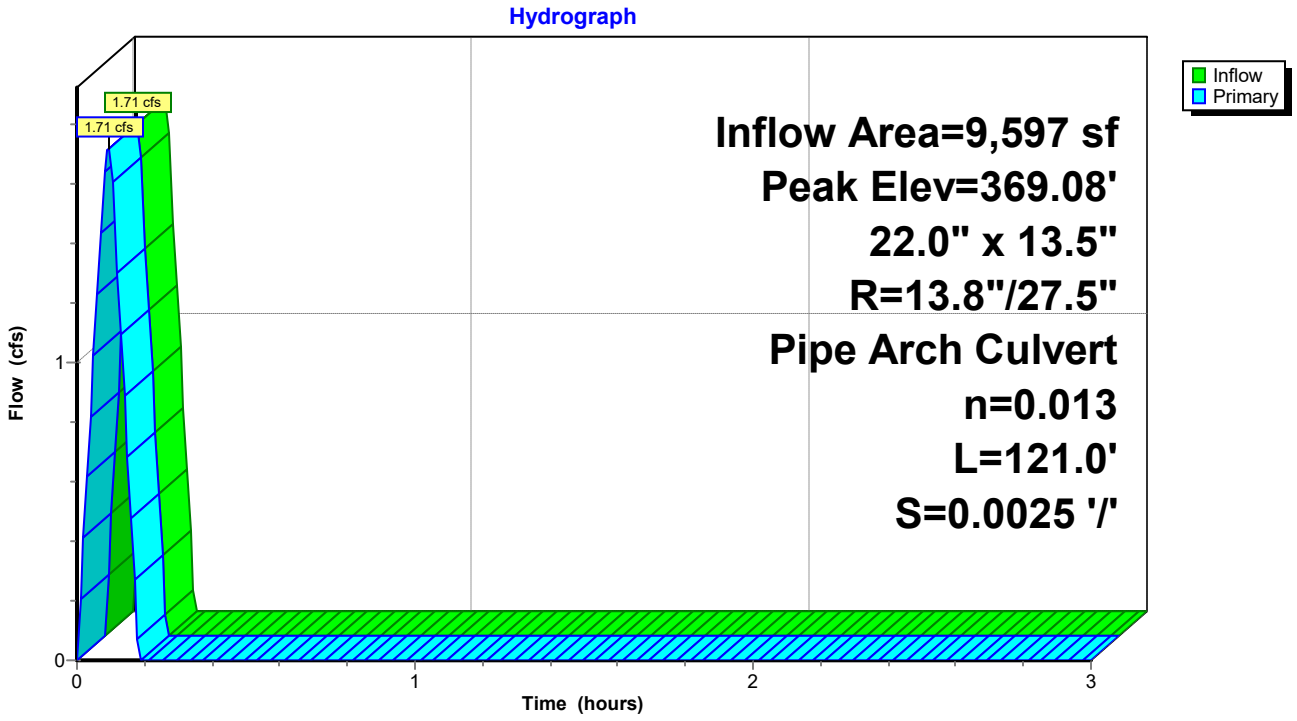
Inflow Area = 9,597 sf, 0.00% Impervious, Inflow Depth = 0.77" for 25-yr event
Inflow = 1.71 cfs @ 0.09 hrs, Volume= 614 cf
Outflow = 1.71 cfs @ 0.09 hrs, Volume= 614 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.71 cfs @ 0.09 hrs, Volume= 614 cf
Routed to Pond CI-A2 : CURB INLET A2

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.08' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **22.0" W x 13.5" H, R=13.8"/27.5" Pipe Arch RCP_Arch 22x14** L= 121.0' RCP, rounded edge headwall, Ke= 0.100 Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900 n= 0.013, Flow Area= 1.65 sf |

**Primary OutFlow** Max=1.71 cfs @ 0.09 hrs HW=369.07' (Free Discharge)
**1=RCP_Arch 22x14** (Barrel Controls 1.71 cfs @ 2.62 fps)

## Pond CI-A1: CURB INLET A1



## Summary for Pond CI-A2: CURB INLET A2

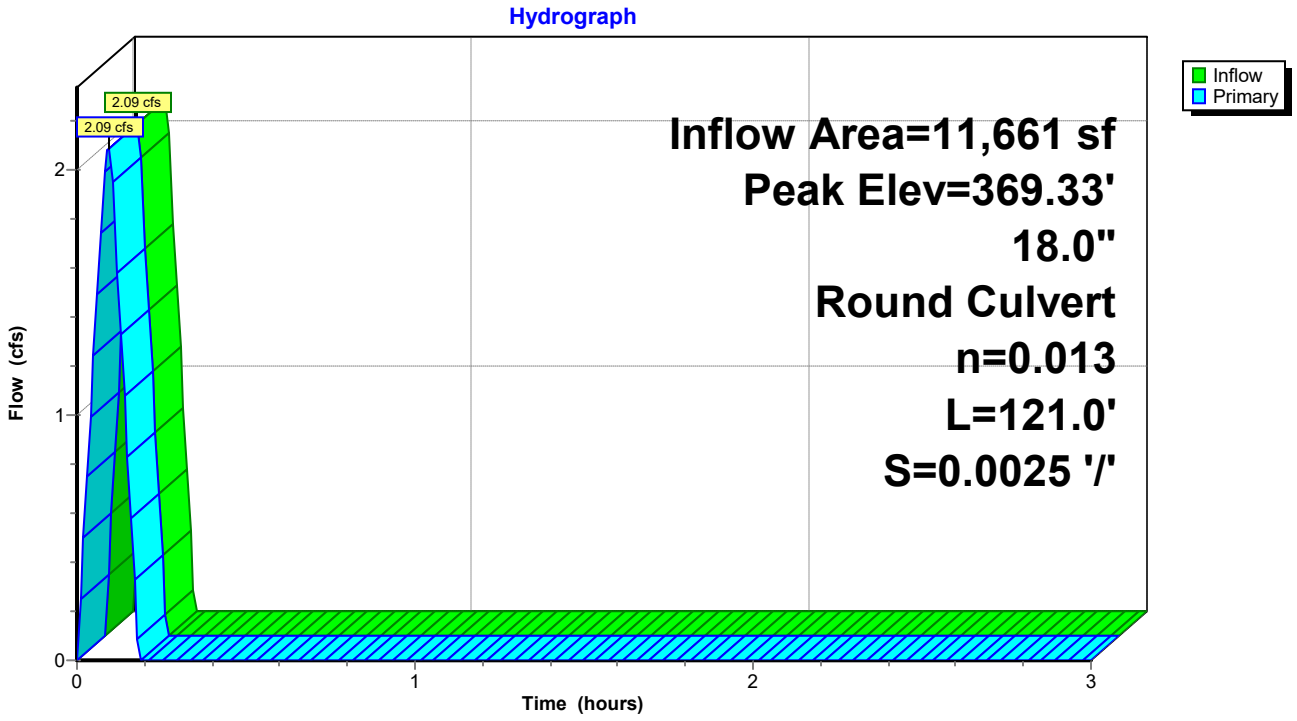
Inflow Area = 11,661 sf, 0.00% Impervious, Inflow Depth = 0.77" for 25-yr event
Inflow = 2.09 cfs @ 0.09 hrs, Volume= 748 cf
Outflow = 2.09 cfs @ 0.09 hrs, Volume= 748 cf, Atten= 0%, Lag= 0.0 min
Primary = 2.09 cfs @ 0.09 hrs, Volume= 748 cf
Routed to Link POST-DEV : Post-Development

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.33' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **18.0" Round RCP_Round 18"**<br>L= 121.0' RCP, rounded edge headwall, Ke= 0.100<br>Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900<br>n= 0.013, Flow Area= 1.77 sf |

**Primary OutFlow** Max=2.08 cfs @ 0.09 hrs HW=369.32' (Free Discharge)
**1=RCP_Round 18"** (Barrel Controls 2.08 cfs @ 2.97 fps)

## Pond CI-A2: CURB INLET A2

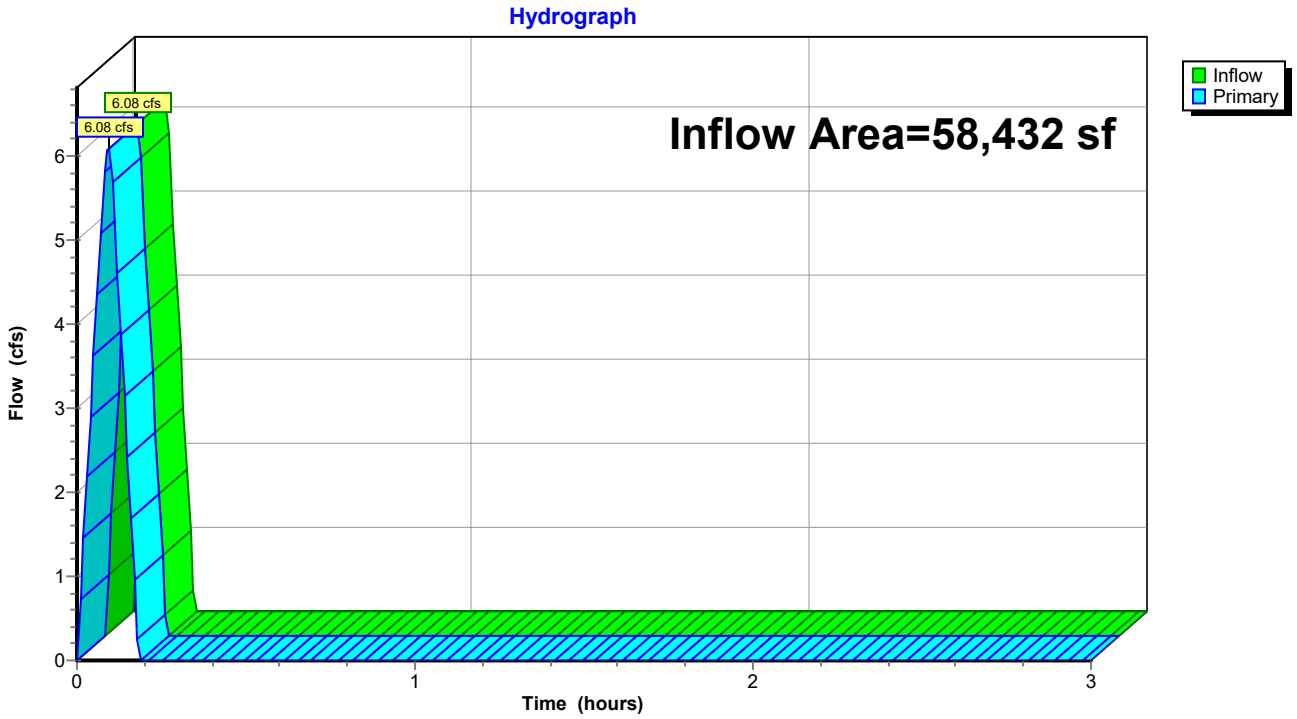


## Summary for Link POST-DEV: Post-Development

Inflow Area = 58,432 sf, 0.00% Impervious, Inflow Depth = 0.45" for 25-yr event
Inflow = 6.08 cfs @ 0.10 hrs, Volume= 2,178 cf
Primary = 6.08 cfs @ 0.10 hrs, Volume= 2,178 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link POST-DEV: Post-Development



## Summary for Subcatchment B1: Drainage Basin B1

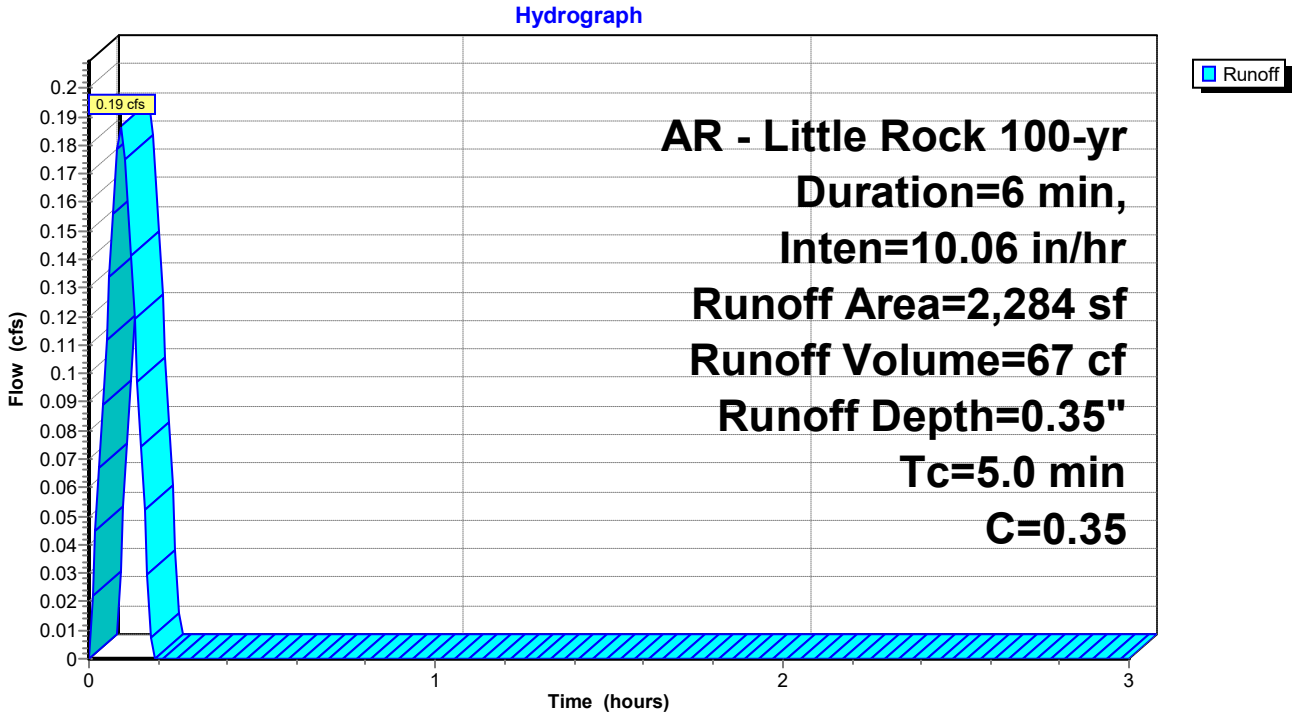
Runoff = 0.19 cfs @ 0.09 hrs, Volume= 67 cf, Depth= 0.35"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=6 min, Inten=10.06 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 2,284 | 0.35 | Sandy Soil 2-7% per manual |
| 0 | 0.92 | Paved Areas |
| 2,284 | 0.35 | Weighted Average |
| 2,284 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 5.0 | | | | | **Direct Entry, Minimum Adjustment** |

### Subcatchment B1: Drainage Basin B1



## Summary for Subcatchment B2: Drainage Basin B2

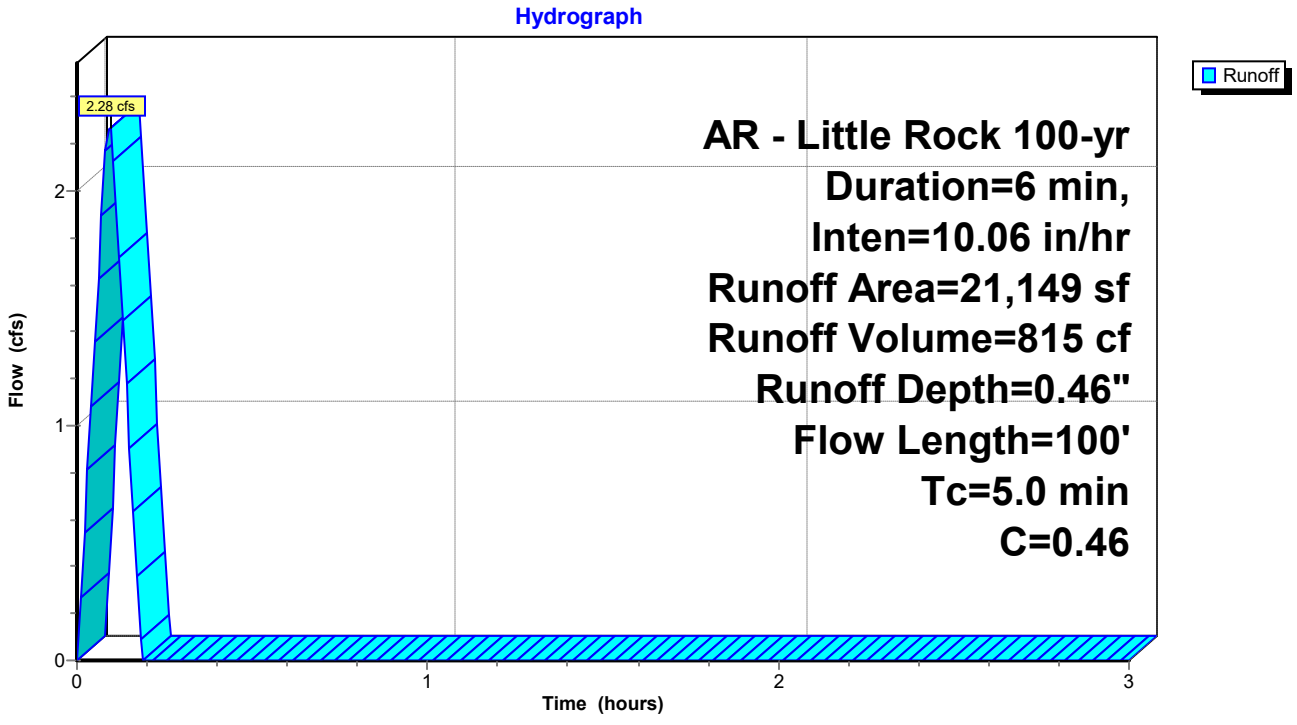
Runoff = 2.28 cfs @ 0.09 hrs, Volume= 815 cf, Depth= 0.46"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=6 min, Inten=10.06 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 16,931 | 0.35 | Sandy Soil 2-7% per manual |
| 4,218 | 0.92 | Paved Areas |
| 21,149 | 0.46 | Weighted Average |
| 21,149 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 42 | 0.1667 | 3.09 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.5 | 58 | 0.0500 | 2.04 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 4.3 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 100 | Total | | | |

## Subcatchment B2: Drainage Basin B2



## Summary for Subcatchment B3: Drainage Basin B3

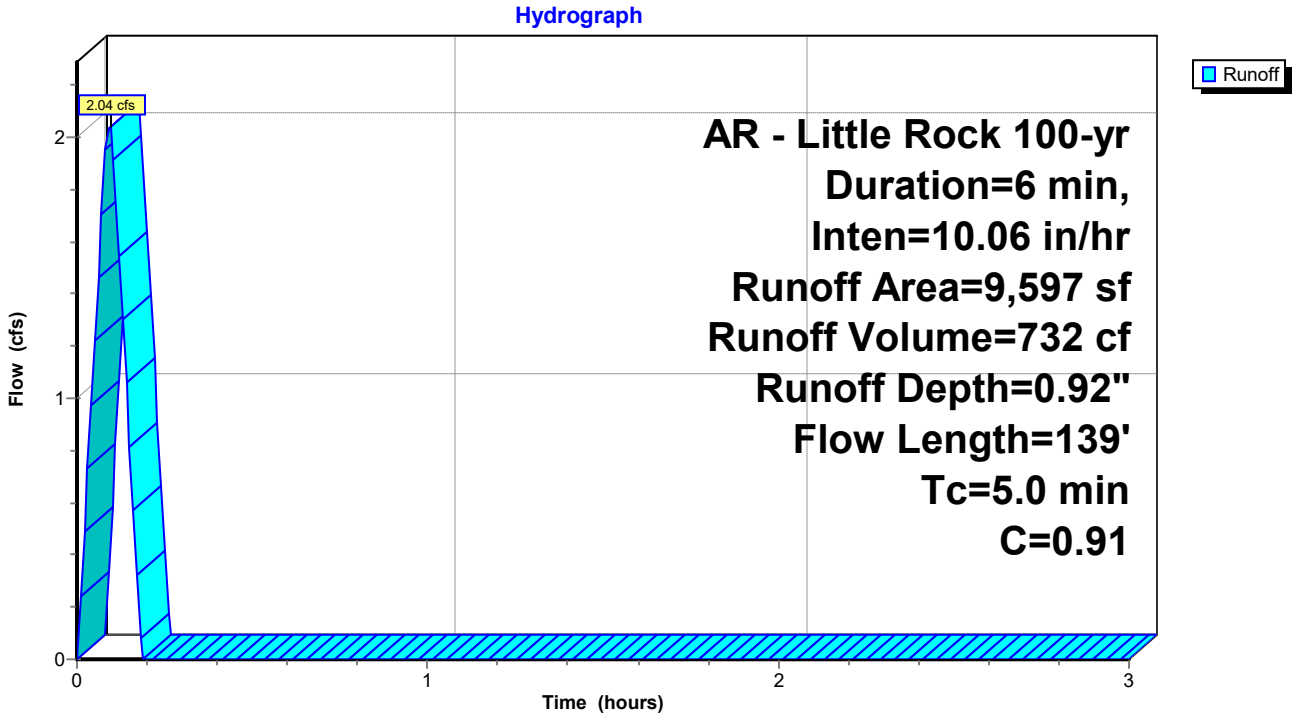
Runoff = 2.04 cfs @ 0.09 hrs, Volume= 732 cf, Depth= 0.92"
Routed to Pond CI-A1 : CURB INLET A1

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=6 min, Inten=10.06 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 155 | 0.35 | Sandy Soil 2-7% per manual |
| 9,442 | 0.92 | Paved Areas |
| 9,597 | 0.91 | Weighted Average |
| 9,597 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.2 | 28 | 0.1667 | 2.85 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 30 | 0.0160 | 1.13 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 41 | 0.0520 | 1.93 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.2 | 40 | 0.0360 | 3.85 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 3.8 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 139 | Total | | | |

## Subcatchment B3: Drainage Basin B3



## Summary for Subcatchment B4: Drainage Basin B4

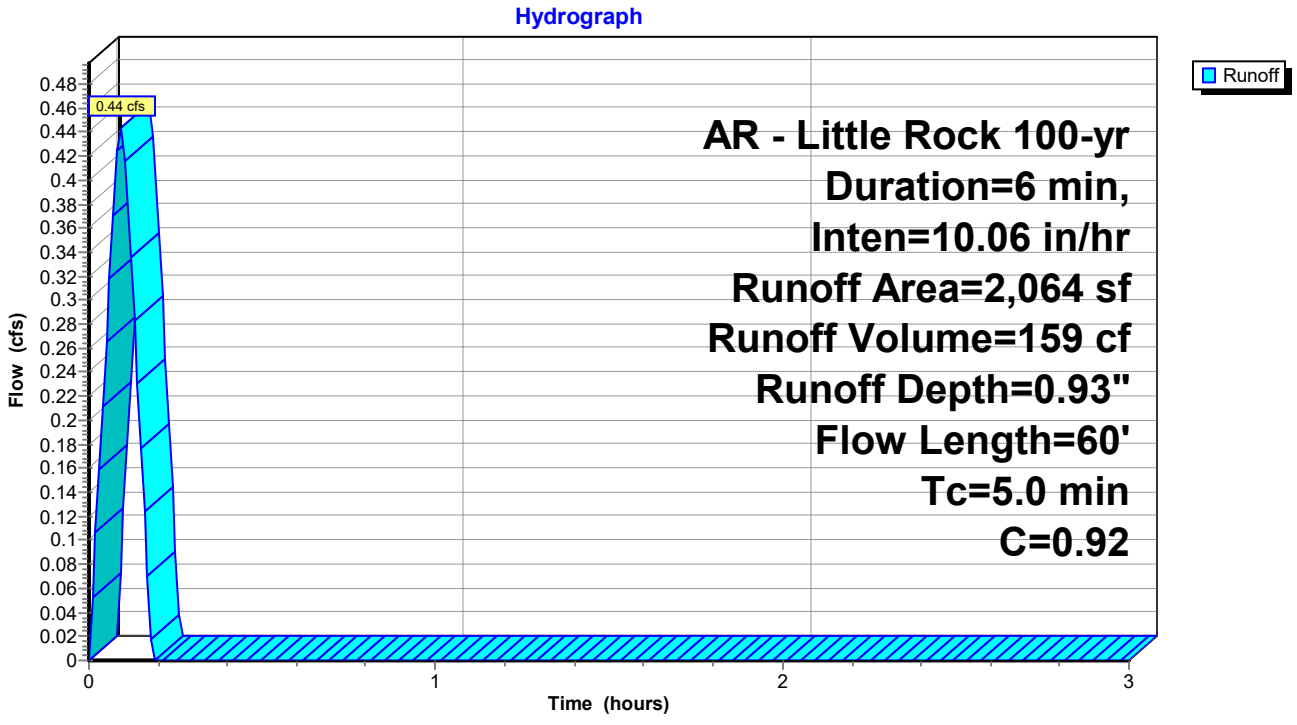
Runoff = 0.44 cfs @ 0.09 hrs, Volume= 159 cf, Depth= 0.93"
Routed to Pond CI-A2 : CURB INLET A2

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=6 min, Inten=10.06 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 0 | 0.35 | Sandy Soil 2-7% per manual |
| 2,064 | 0.92 | Paved Areas |
| 2,064 | 0.92 | Weighted Average |
| 2,064 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.6 | 45 | 0.0170 | 1.26 | | **Sheet Flow, Asphalt Sheet Flow** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.0 | 15 | 0.0840 | 5.88 | | **Shallow Concentrated Flow, Gutter Flow** Paved Kv= 20.3 fps |
| 4.4 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 60 | Total | | | |

## Subcatchment B4: Drainage Basin B4



## Summary for Subcatchment B5: Drainage Basin B5

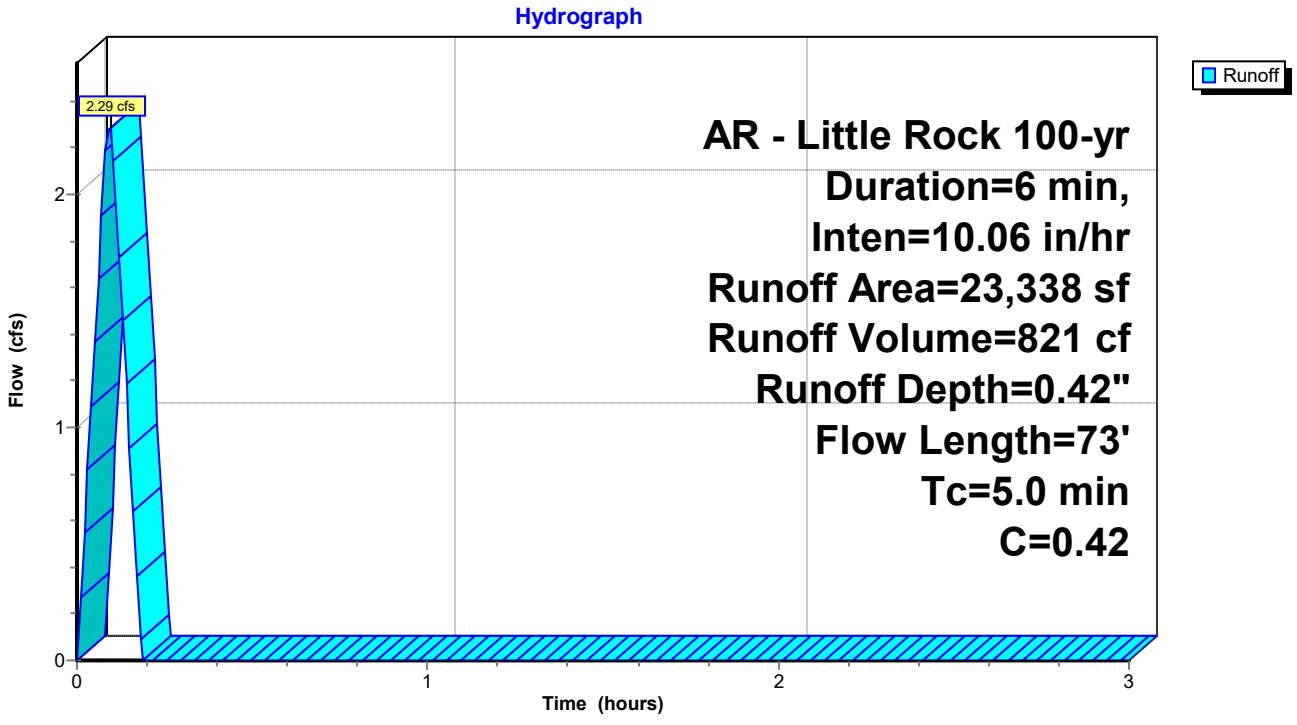
Runoff = 2.29 cfs @ 0.09 hrs, Volume= 821 cf, Depth= 0.42"
Routed to Link POST-DEV : Post-Development

Runoff by Rational method, Rise/Fall=1.0/1.0 xTc, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
AR - Little Rock 100-yr Duration=6 min, Inten=10.06 in/hr

| Area (sf) | C | Description |
|---|---|---|
| 20,627 | 0.35 | Sandy Soil 2-7% per manual |
| 2,711 | 0.92 | Paved Areas |
| 23,338 | 0.42 | Weighted Average |
| 23,338 | | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|---|---|---|---|---|---|
| 0.1 | 18 | 0.1667 | 2.61 | | **Sheet Flow, Rooftop** Smooth surfaces n= 0.011 P2= 4.20" |
| 0.4 | 55 | 0.0860 | 2.05 | | **Shallow Concentrated Flow, Overland Concentrated** Short Grass Pasture Kv= 7.0 fps |
| 4.5 | | | | | **Direct Entry, Minimum Adjustment** |
| 5.0 | 73 | Total | | | |

## Subcatchment B5: Drainage Basin B5



## Summary for Pond CI-A1: CURB INLET A1

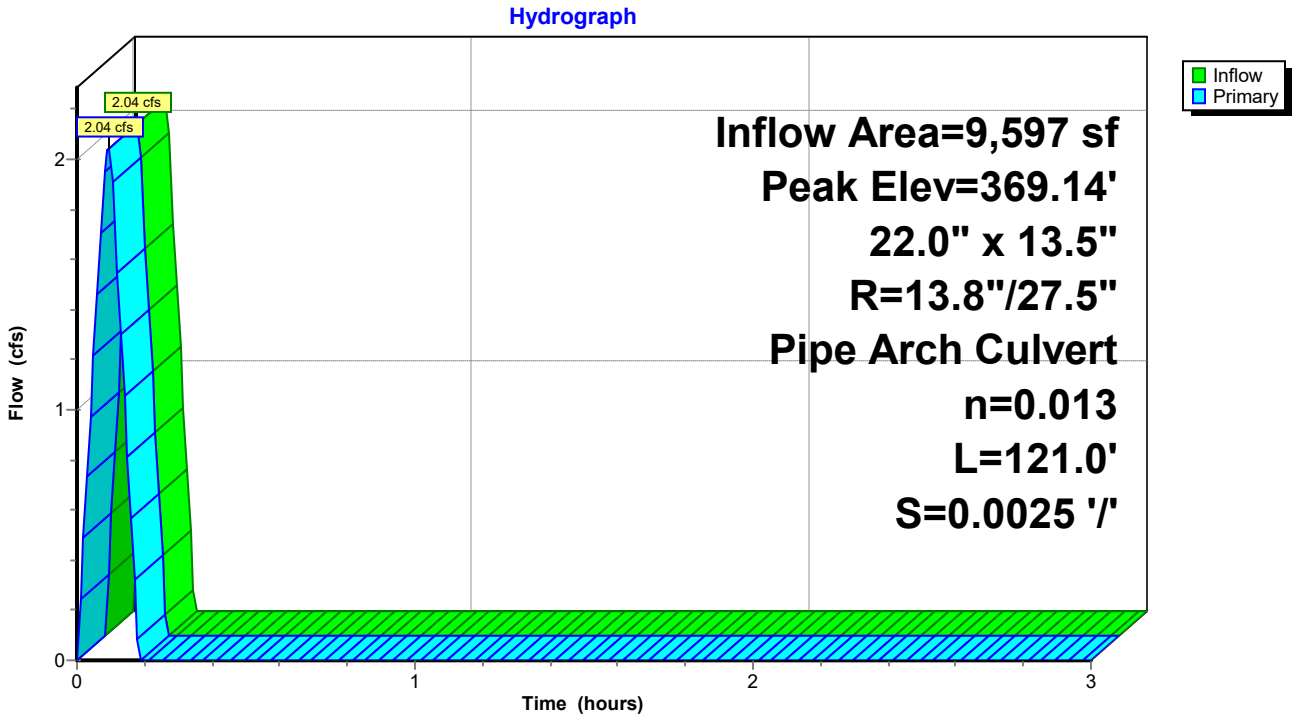
Inflow Area = 9,597 sf, 0.00% Impervious, Inflow Depth = 0.92" for 100-yr event
Inflow = 2.04 cfs @ 0.09 hrs, Volume= 732 cf
Outflow = 2.04 cfs @ 0.09 hrs, Volume= 732 cf, Atten= 0%, Lag= 0.0 min
Primary = 2.04 cfs @ 0.09 hrs, Volume= 732 cf
Routed to Pond CI-A2 : CURB INLET A2

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.14' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **22.0" W x 13.5" H, R=13.8"/27.5" Pipe Arch RCP_Arch 22x14** L= 121.0' RCP, rounded edge headwall, Ke= 0.100 Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900 n= 0.013, Flow Area= 1.65 sf |

**Primary OutFlow** Max=2.03 cfs @ 0.09 hrs HW=369.13' (Free Discharge)
**1=RCP_Arch 22x14** (Barrel Controls 2.03 cfs @ 2.77 fps)

## Pond CI-A1: CURB INLET A1



## Summary for Pond CI-A2: CURB INLET A2

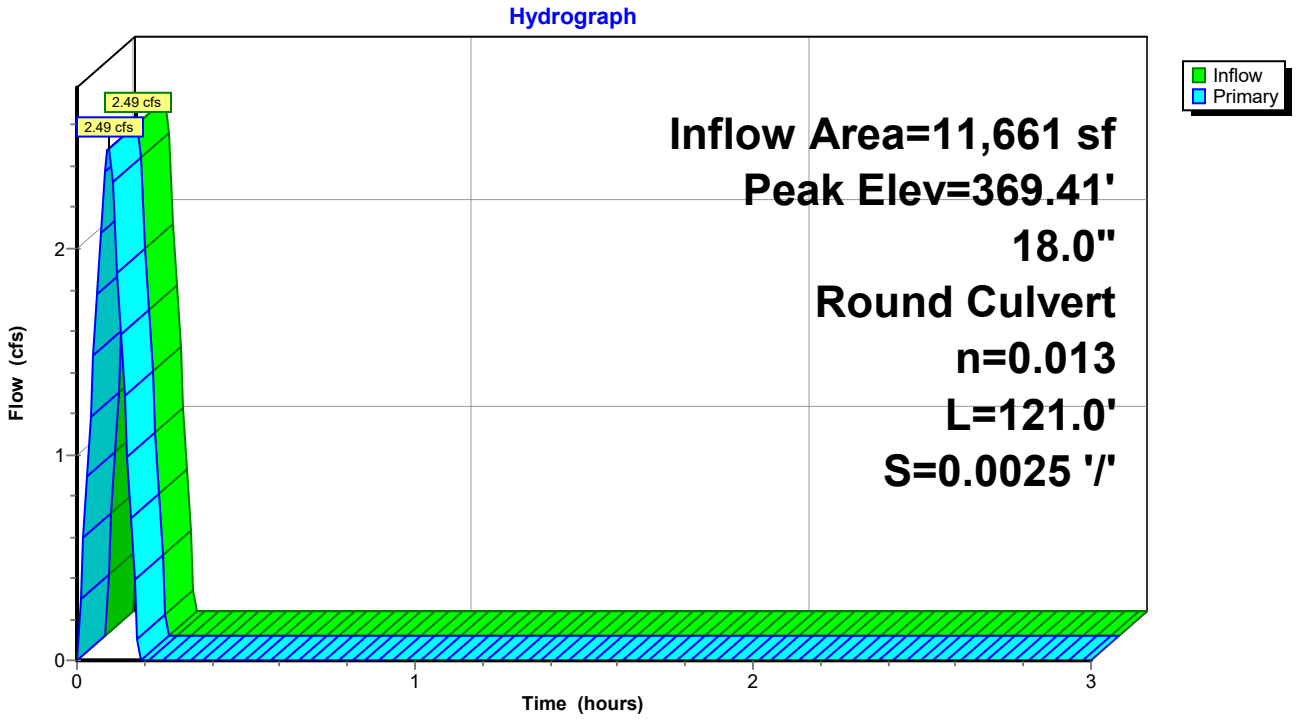
Inflow Area = 11,661 sf, 0.00% Impervious, Inflow Depth = 0.92" for 100-yr event
Inflow = 2.49 cfs @ 0.09 hrs, Volume= 891 cf
Outflow = 2.49 cfs @ 0.09 hrs, Volume= 891 cf, Atten= 0%, Lag= 0.0 min
Primary = 2.49 cfs @ 0.09 hrs, Volume= 891 cf
Routed to Link POST-DEV : Post-Development

Routing by Stor-Ind method, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs
Peak Elev= 369.41' @ 0.09 hrs

| Device | Routing | Invert | Outlet Devices |
|---|---|---|---|
| #1 | Primary | 368.49' | **18.0" Round RCP_Round 18"**<br>L= 121.0' RCP, rounded edge headwall, Ke= 0.100<br>Inlet / Outlet Invert= 368.49' / 368.19' S= 0.0025 '/' Cc= 0.900<br>n= 0.013, Flow Area= 1.77 sf |

**Primary OutFlow** Max=2.47 cfs @ 0.09 hrs HW=369.41' (Free Discharge)
**1=RCP_Round 18"** (Barrel Controls 2.47 cfs @ 3.13 fps)

## Pond CI-A2: CURB INLET A2

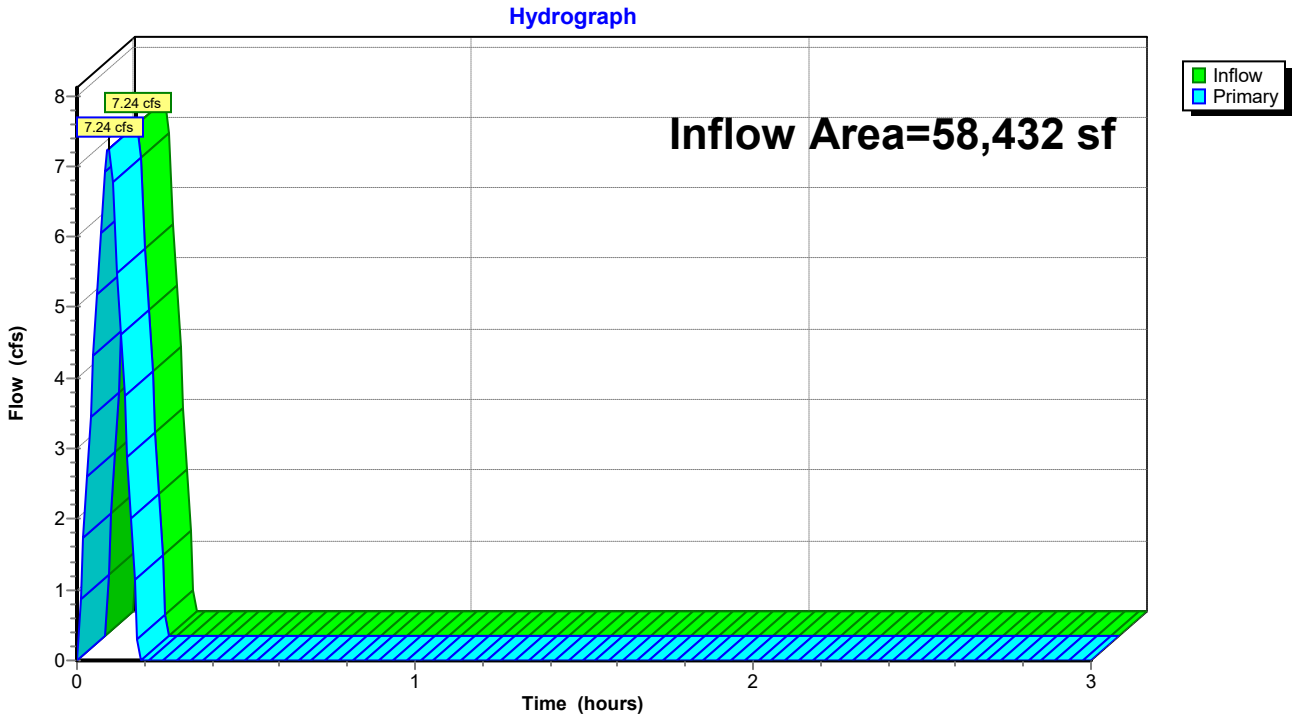


## Summary for Link POST-DEV: Post-Development

Inflow Area = 58,432 sf, 0.00% Impervious, Inflow Depth = 0.53" for 100-yr event
Inflow = 7.24 cfs @ 0.09 hrs, Volume= 2,594 cf
Primary = 7.24 cfs @ 0.09 hrs, Volume= 2,594 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-3.00 hrs, dt= 0.01 hrs

## Link POST-DEV: Post-Development



# STORM SEWER SIZING

# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Tuesday, Jul 15 2025

## PIPE A1 (25 YR)

**Circular**

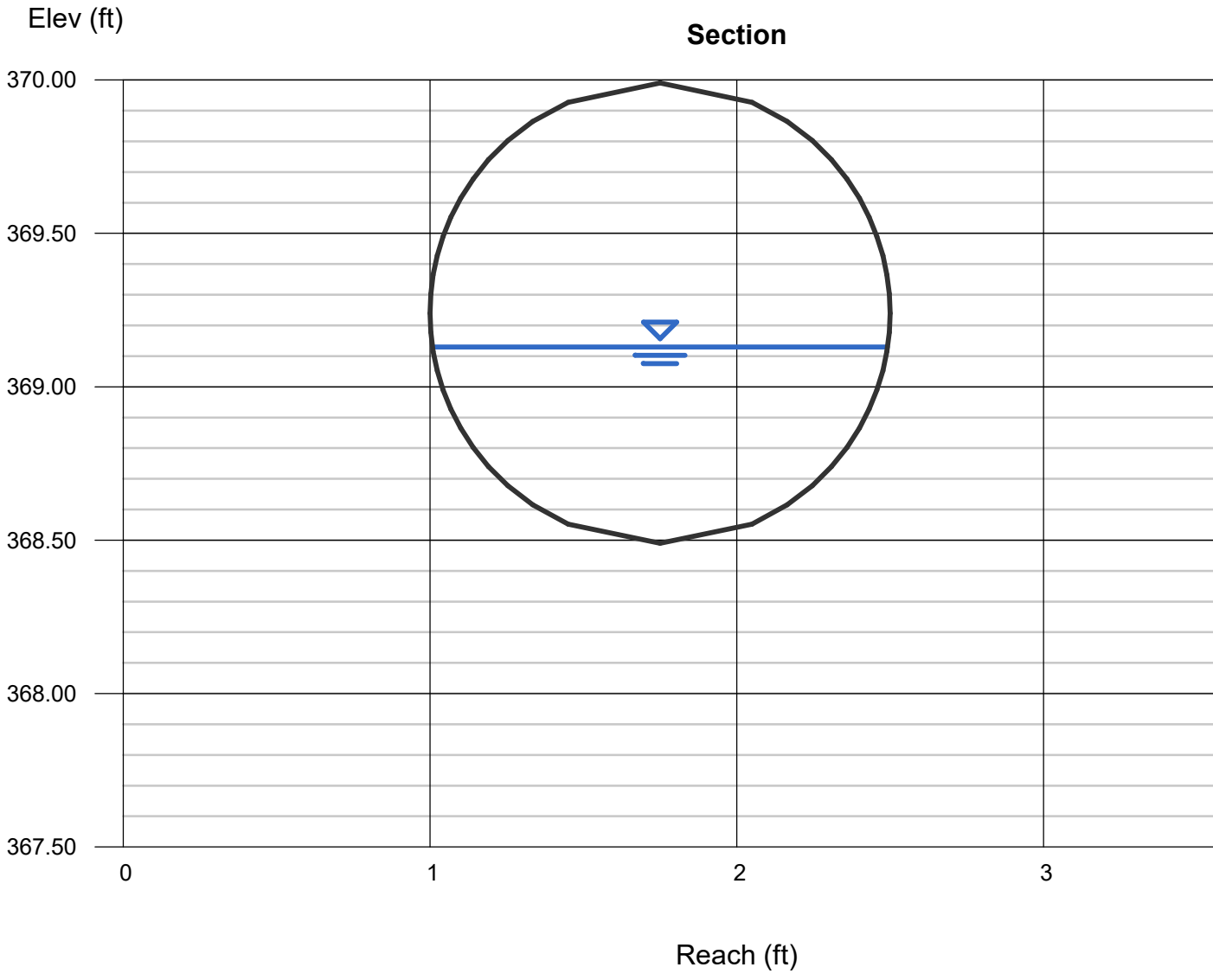
| | |
|---|---|
| Diameter (ft) | = 1.50 |
| Invert Elev (ft) | = 368.49 |
| Slope (%) | = 0.25 |
| N-Value | = 0.015 |

**Calculations**

| | |
|---|---|
| Compute by: | Known Q |
| Known Q (cfs) | = 1.71 |

**Highlighted**

| | |
|---|---|
| Depth (ft) | = 0.64 |
| Q (cfs) | = 1.710 |
| Area (sqft) | = 0.72 |
| Velocity (ft/s) | = 2.37 |
| Wetted Perim (ft) | = 2.14 |
| Crit Depth, Yc (ft) | = 0.49 |
| Top Width (ft) | = 1.48 |
| EGL (ft) | = 0.73 |



# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Tuesday, Jul 15 2025

## PIPE A2 (25 YR)

**Circular**

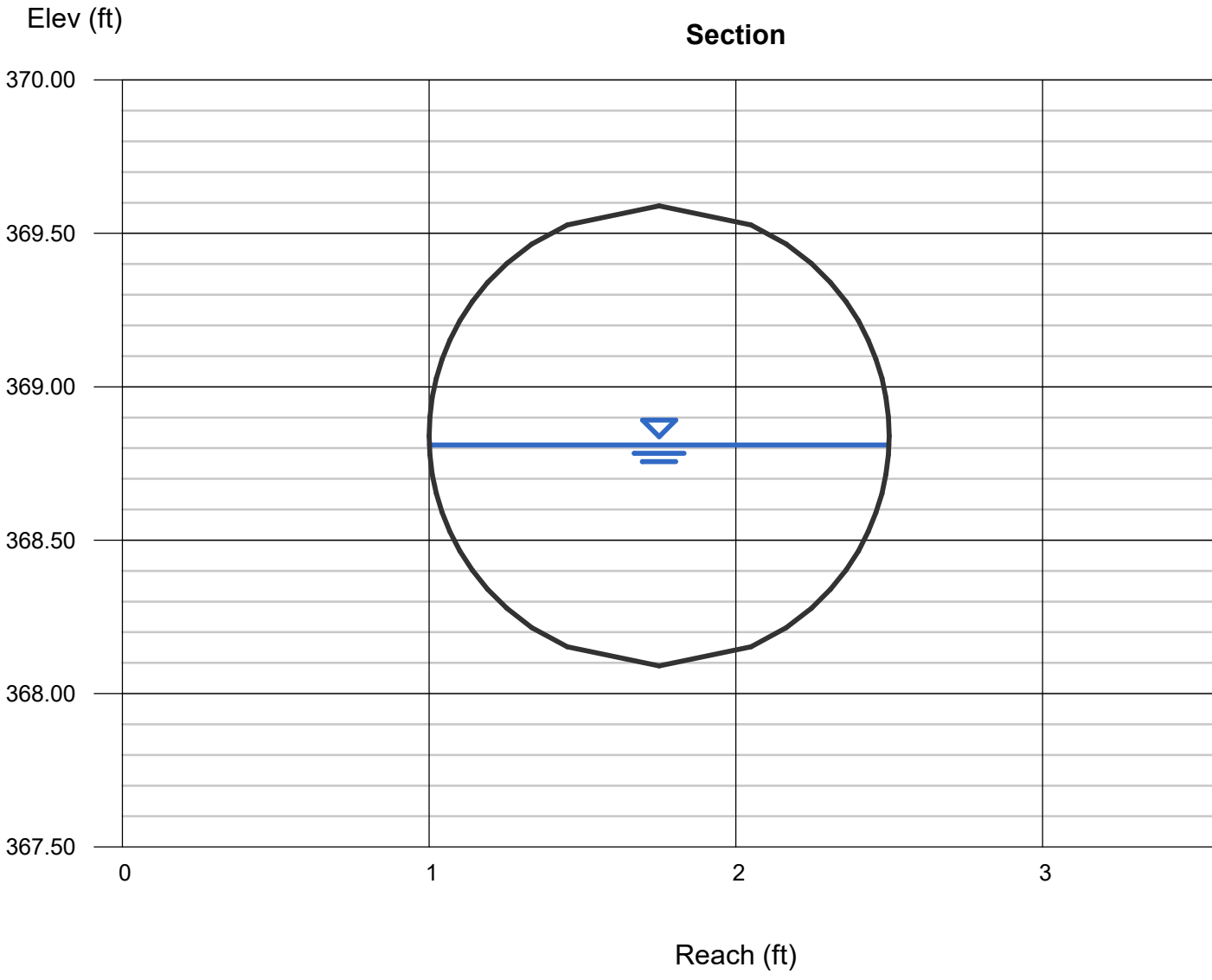
| | |
|---|---|
| Diameter (ft) | = 1.50 |
| Invert Elev (ft) | = 368.09 |
| Slope (%) | = 0.25 |
| N-Value | = 0.015 |

**Calculations**

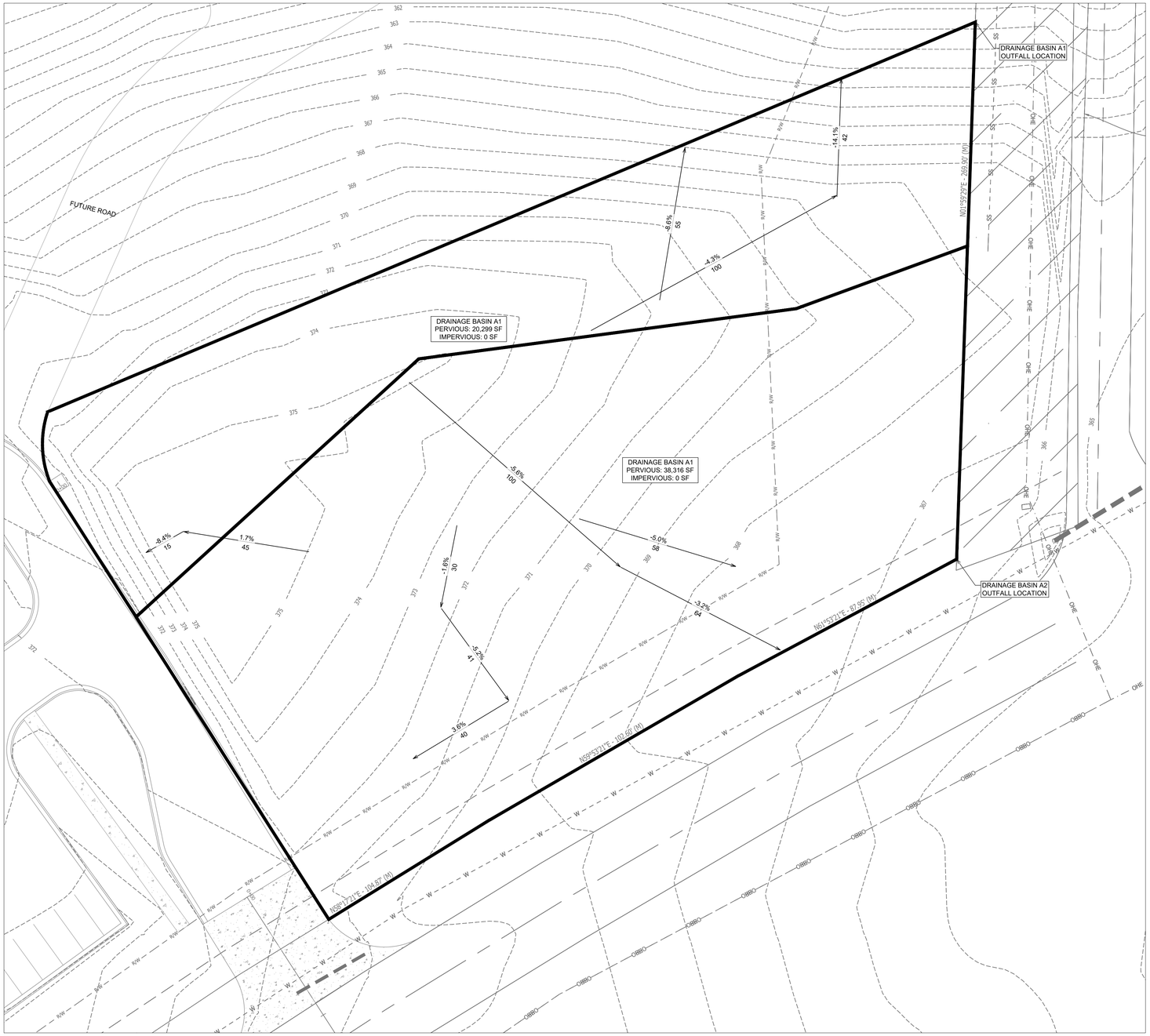
| | |
|---|---|
| Compute by: | Known Q |
| Known Q (cfs) | = 2.09 |

**Highlighted**

| | |
|---|---|
| Depth (ft) | = 0.72 |
| Q (cfs) | = 2.090 |
| Area (sqft) | = 0.84 |
| Velocity (ft/s) | = 2.48 |
| Wetted Perim (ft) | = 2.30 |
| Crit Depth, Yc (ft) | = 0.55 |
| Top Width (ft) | = 1.50 |
| EGL (ft) | = 0.82 |



# DRAINAGE BASIN MAPS




## PRE-DEVELOPMENT DRAINAGE BASIN PLAN

SCALE 1" = 20'

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGININGS**
HIGHWAY 5
BRYANT, ARKANSAS

CERTIFICATE OF AUTHORIZATION
PHILLIP LEWIS ENGINEERING, INC.
No. 566
ARKANSAS ENGINEER

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

N

0 20'

1" = 20'-0"

PROJECT NUMBER:

SHEET ISSUE DATE:
---

PAGE TITLE:
PRE-DEV DRAINAGE

SHEET NUMBER:
C1.10

# POST-DEV DRAINAGE

SCALE 1" = 20'

## GENERAL SITE NOTES

1. TOTAL NEW DEVELOPMENT AREA = (+/-) 1.4 ACRES
2. PROPERTY IS ZONED C-2
3. 21 PARKING SPACES PROVIDED INCLUDING 2 ADA ACCESSIBLE PARKING SPACES
4. ALL DIMENSIONS ARE TO THE BACK OF CURB AND/OR EDGE OF PAVEMENT
5. DAMAGE TO PUBLIC AND PRIVATE PROPERTY DUE TO HAULING OPERATIONS OR OPERATIONS OF CONSTRUCTION RELATED EQUIPMENT FROM A CONSTRUCTION SITE SHALL BE REPAIRED BY THE THE RESPONSIBLE PARTY PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY.
6. REPAIR, REPLACE, OR EXTEND EXISTING DAMAGED OR MISSING CURB AND GUTTER, SIDEWALK OR RAMPS WITHIN THE PUBLIC RIGHT OF WAY.
7. ALL SIGNAGE, PAVEMENT MARKING AND PARKING LOT STRIPING SHALL CONFORM TO REQUIREMENTS GIVEN IN MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD). MUTCD REQUIRES THAT PARKING SPACES BE MARKED IN WHITE.

PHILLIP LEWIS ENGINEERING, INC.
Structural + Civil Consultants
23620 Interstate 30 | Bryant, Arkansas
PH: 501-350-9840

REVISION:

**NEW BEGINNINGS**
HIGHWAY 5
BRYANT, ARKANSAS

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ARKANSAS ENGINEERING

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 9540
PHILLIP A. LEWIS

PROJECT NUMBER:

SHEET ISSUE DATE:
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PAGE TITLE:
POST-DEV DRAINAGE

SHEET NUMBER:
C1.11

N

0 10'
1" = 10'-0"

# SOIL CLASSIFICATION MAPS

United States Department of Agriculture

NRCS

Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Saline County, Arkansas

August 30, 2024

# Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report
## Soil Map

## MAP LEGEND

**Area of Interest (AOI)**
- Area of Interest (AOI)

**Soils**
- Soil Map Unit Polygons
- Soil Map Unit Lines
- Soil Map Unit Points

**Special Point Features**
- Blowout
- Borrow Pit
- Clay Spot
- Closed Depression
- Gravel Pit
- Gravelly Spot
- Landfill
- Lava Flow
- Marsh or swamp
- Mine or Quarry
- Miscellaneous Water
- Perennial Water
- Rock Outcrop
- Saline Spot
- Sandy Spot
- Severely Eroded Spot
- Sinkhole
- Slide or Slip
- Sodic Spot
- Spoil Area
- Stony Spot
- Very Stony Spot
- Wet Spot
- Other
- Special Line Features

**Water Features**
- Streams and Canals

**Transportation**
- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

**Background**
- Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Saline County, Arkansas
Survey Area Data: Version 20, Sep 12, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 1, 2022—May 29, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|---|---|---|---|
| 16 | Ouachita silt loam, 0 to 1 percent slopes, frequently flooded | 3.6 | 25.0% |
| 22 | Savannah fine sandy loam, 3 to 8 percent slopes | 2.5 | 17.8% |
| 27 | Smithdale loamy sand, 8 to 12 percent slopes | 4.9 | 34.4% |
| 29 | Tiak silt loam, 3 to 8 percent slopes | 3.3 | 22.9% |
| **Totals for Area of Interest** | | **14.2** | **100.0%** |

# Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

# Saline County, Arkansas

## 16—Ouachita silt loam, 0 to 1 percent slopes, frequently flooded

### Map Unit Setting

*National map unit symbol:* 30g3t
*Elevation:* 120 to 250 feet
*Mean annual precipitation:* 48 to 64 inches
*Mean annual air temperature:* 52 to 75 degrees F
*Frost-free period:* 225 to 290 days
*Farmland classification:* Farmland of statewide importance

### Map Unit Composition

*Ouachita, frequently flooded, brief duration, and similar soils:* 85 percent
*Minor components:* 15 percent
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Ouachita, Frequently Flooded, Brief Duration

#### Setting

*Landform:* Flood plains
*Landform position (three-dimensional):* Talf
*Down-slope shape:* Linear
*Across-slope shape:* Linear
*Parent material:* Loamy alluvium

#### Typical profile

*A - 0 to 4 inches:* silt loam
*Bw - 4 to 42 inches:* silt loam
*2C - 42 to 80 inches:* very fine sandy loam

#### Properties and qualities

*Slope:* 0 to 1 percent
*Depth to restrictive feature:* More than 80 inches
*Drainage class:* Well drained
*Runoff class:* Low
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.57 in/hr)
*Depth to water table:* More than 80 inches
*Frequency of flooding:* Frequent
*Frequency of ponding:* None
*Maximum salinity:* Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)
*Available water supply, 0 to 60 inches:* High (about 10.3 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified
*Land capability classification (nonirrigated):* 5w
*Hydrologic Soil Group:* C
*Ecological site:* F133BY017TX - Loamy Bottomland
*Hydric soil rating:* No

### Minor Components

#### Ouachita, frequently flooded, long duration

*Percent of map unit:* 5 percent
*Landform:* Flood plains

*Landform position (three-dimensional):* Talf
*Down-slope shape:* Linear
*Across-slope shape:* Linear
*Ecological site:* F133BY017TX - Loamy Bottomland
*Hydric soil rating:* Yes

**Aquents, frequently flooded**
*Percent of map unit:* 5 percent
*Landform:* Depressions
*Landform position (three-dimensional):* Dip
*Down-slope shape:* Concave
*Across-slope shape:* Convex
*Ecological site:* F133BY012TX - Wet Terrace
*Hydric soil rating:* Yes

**Una, frequently flooded**
*Percent of map unit:* 3 percent
*Landform:* Flood plains
*Landform position (three-dimensional):* Talf
*Down-slope shape:* Linear
*Across-slope shape:* Linear
*Ecological site:* F133BY018TX - Clayey Bottomland
*Hydric soil rating:* Yes

**Guyton, frequently flooded**
*Percent of map unit:* 2 percent
*Landform:* Flood plains
*Landform position (three-dimensional):* Talf
*Down-slope shape:* Linear
*Across-slope shape:* Linear
*Ecological site:* F133BY017TX - Loamy Bottomland
*Hydric soil rating:* Yes

## 22—Savannah fine sandy loam, 3 to 8 percent slopes

**Map Unit Setting**
*National map unit symbol:* 2tzrt
*Elevation:* 50 to 250 feet
*Mean annual precipitation:* 38 to 61 inches
*Mean annual air temperature:* 52 to 73 degrees F
*Frost-free period:* 220 to 260 days
*Farmland classification:* Farmland of statewide importance

**Map Unit Composition**
*Savannah and similar soils:* 95 percent
*Minor components:* 5 percent
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Savannah

#### Setting

*Landform:* Interfluves
*Landform position (three-dimensional):* Riser
*Down-slope shape:* Convex
*Across-slope shape:* Linear
*Parent material:* Loamy marine deposits

#### Typical profile

*Ap - 0 to 9 inches:* fine sandy loam
*Bt - 9 to 24 inches:* loam
*Btx - 24 to 59 inches:* loam
*BC - 59 to 72 inches:* sandy loam

#### Properties and qualities

*Slope:* 3 to 8 percent
*Depth to restrictive feature:* 16 to 32 inches to fragipan
*Drainage class:* Moderately well drained
*Runoff class:* Medium
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.57 in/hr)
*Depth to water table:* About 16 to 30 inches
*Frequency of flooding:* None
*Frequency of ponding:* None
*Available water supply, 0 to 60 inches:* Low (about 3.5 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified
*Land capability classification (nonirrigated):* 2e
*Hydrologic Soil Group:* C
*Ecological site:* F133BY005TX - Loamy Upland
*Hydric soil rating:* No

### Minor Components

#### Amy

*Percent of map unit:* 5 percent
*Landform:* Stream terraces
*Landform position (three-dimensional):* Tread
*Down-slope shape:* Concave
*Across-slope shape:* Linear
*Ecological site:* F133BY017TX - Loamy Bottomland
*Hydric soil rating:* Yes

## 27—Smithdale loamy sand, 8 to 12 percent slopes

### Map Unit Setting

*National map unit symbol:* m06n
*Elevation:* 70 to 620 feet

*Mean annual precipitation:* 44 to 61 inches
*Mean annual air temperature:* 49 to 74 degrees F
*Frost-free period:* 185 to 230 days
*Farmland classification:* Not prime farmland

**Map Unit Composition**
*Smithdale and similar soils:* 100 percent
*Estimates are based on observations, descriptions, and transects of the mapunit.*

**Description of Smithdale**

**Setting**
*Landform:* Interfluves
*Down-slope shape:* Convex
*Across-slope shape:* Linear
*Parent material:* Loamy marine deposits

**Typical profile**
*A - 0 to 6 inches:* loamy sand
*BA - 6 to 15 inches:* fine sandy loam
*Bt1 - 15 to 26 inches:* sandy clay loam
*Bt2 - 26 to 102 inches:* fine sandy loam
*BC - 102 to 123 inches:* loamy fine sand

**Properties and qualities**
*Slope:* 8 to 12 percent
*Depth to restrictive feature:* More than 80 inches
*Drainage class:* Well drained
*Runoff class:* Medium
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.57 to 1.98 in/hr)
*Depth to water table:* More than 80 inches
*Frequency of flooding:* None
*Frequency of ponding:* None
*Available water supply, 0 to 60 inches:* Moderate (about 8.0 inches)

**Interpretive groups**
*Land capability classification (irrigated):* None specified
*Land capability classification (nonirrigated):* 4e
*Hydrologic Soil Group:* B
*Ecological site:* F133BY005TX - Loamy Upland
*Hydric soil rating:* No

## 29—Tiak silt loam, 3 to 8 percent slopes

**Map Unit Setting**
*National map unit symbol:* m06q
*Elevation:* 70 to 570 feet
*Mean annual precipitation:* 44 to 61 inches
*Mean annual air temperature:* 49 to 74 degrees F
*Frost-free period:* 185 to 230 days
*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Tiak and similar soils:* 100 percent
*Estimates are based on observations, descriptions, and transects of the mapunit.*

**Description of Tiak**

**Setting**

*Landform:* Interfluves
*Down-slope shape:* Convex
*Across-slope shape:* Linear
*Parent material:* Loamy and clayey marine deposits

**Typical profile**

*A - 0 to 7 inches:* silt loam
*E - 7 to 9 inches:* loam
*Bt1 - 9 to 32 inches:* clay
*Bt2 - 32 to 72 inches:* clay

**Properties and qualities**

*Slope:* 3 to 8 percent
*Depth to restrictive feature:* More than 80 inches
*Drainage class:* Moderately well drained
*Runoff class:* Very high
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to moderately high (0.06 to 0.20 in/hr)
*Depth to water table:* About 12 to 24 inches
*Frequency of flooding:* None
*Frequency of ponding:* None
*Available water supply, 0 to 60 inches:* High (about 9.3 inches)

**Interpretive groups**

*Land capability classification (irrigated):* None specified
*Land capability classification (nonirrigated):* 3e
*Hydrologic Soil Group:* C/D
*Ecological site:* F133BY002TX - Seasonally Wet Upland
*Hydric soil rating:* No

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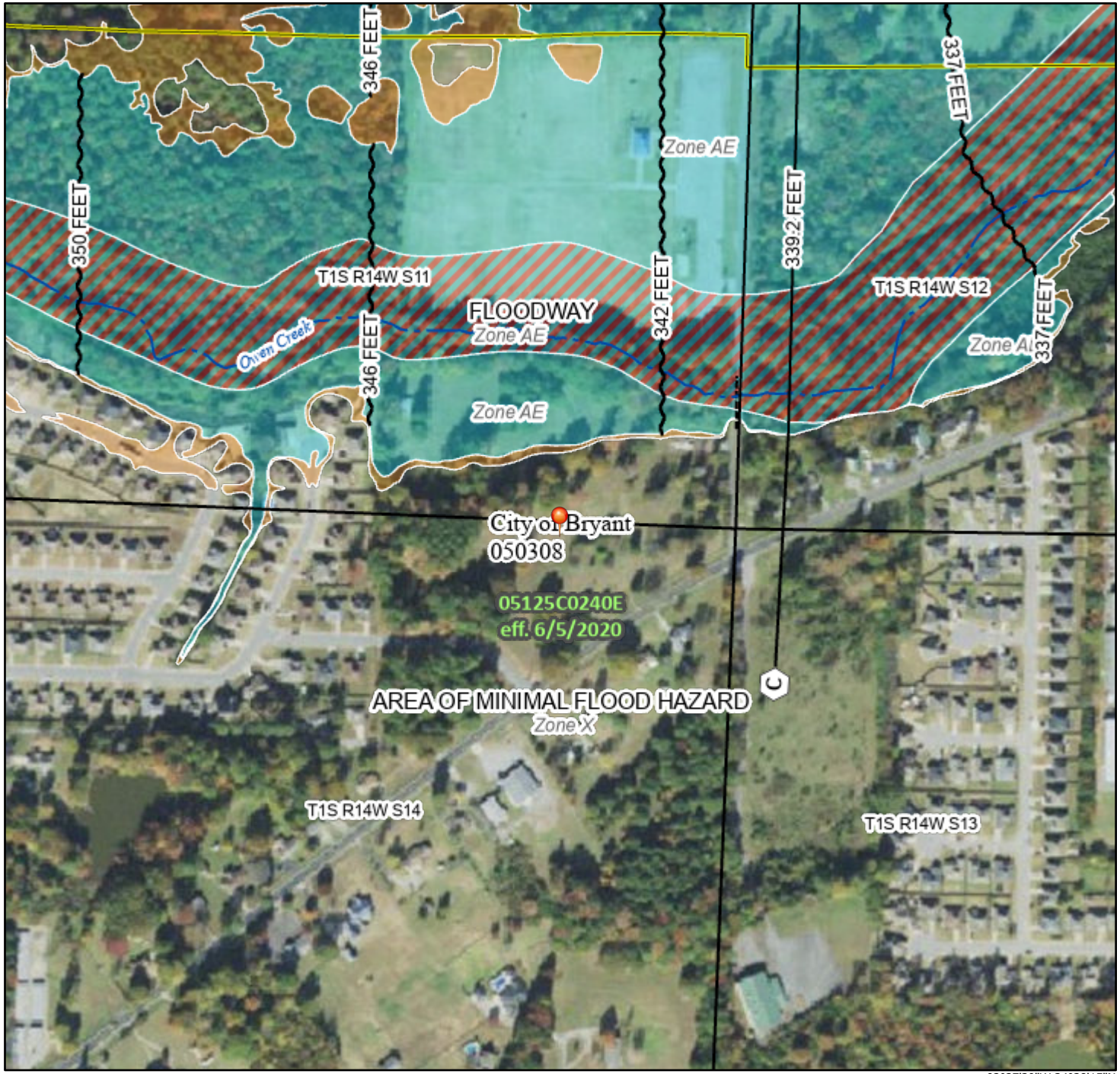
FEMA FLOOD INSURANCE RATE MAP

# National Flood Hazard Layer FIRMette

FEMA

92°28'7"W 34°38'45"N




92°27'30"W 34°38'15"N

0 250 500 1,000 1,500 2,000 Feet

1:6,000

*Basemap Imagery Source: USGS National Map 2023*

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

**SPECIAL FLOOD HAZARD AREAS**
- Without Base Flood Elevation (BFE) *Zone A, V, A99*
- With BFE or Depth *Zone AE, AO, AH, VE, AR*
- Regulatory Floodway

**OTHER AREAS OF FLOOD HAZARD**
- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X*
- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

**OTHER AREAS**
- NO SCREEN Area of Minimal Flood Hazard *Zone X*
- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

**GENERAL STRUCTURES**
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

**OTHER FEATURES**
- 20.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

**MAP PANELS**
- Digital Data Available
- No Digital Data Available
- Unmapped

N

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

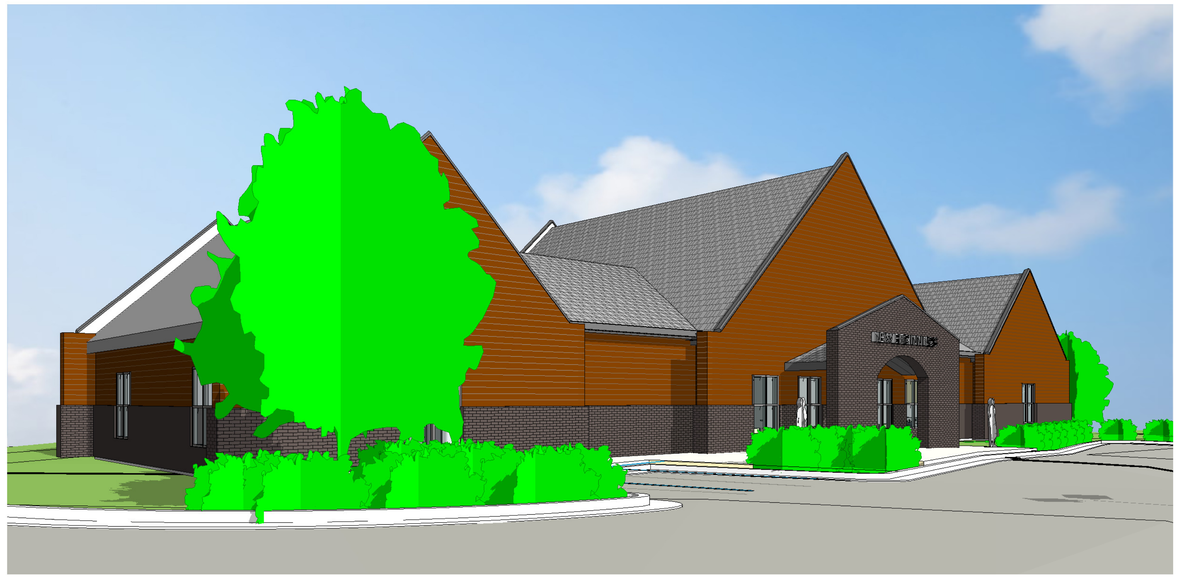
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 10/9/2024 at 5:29 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

1 3D ISO-FRONT-1

3 3D-ISO-REAR-1

5 3D EXT-FRONT-3




2 3D EXT-FRONT-2

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3D VIEWS

A001

1 3D EXT-REAR-4

3 3D EXT-FRONT-4

2 3D EXT-FRONT-1

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3D VIEWS

A002

1 3D ISO-FRONT-2

2 3D-ISO-REAR-2

3 3D EXT-REAR-1


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3D VIEWS

A003

1 3D-P-FROM THE EAST-ELEVATED-1

2 3D-P-FROM THE EAST-ELEVATED-2

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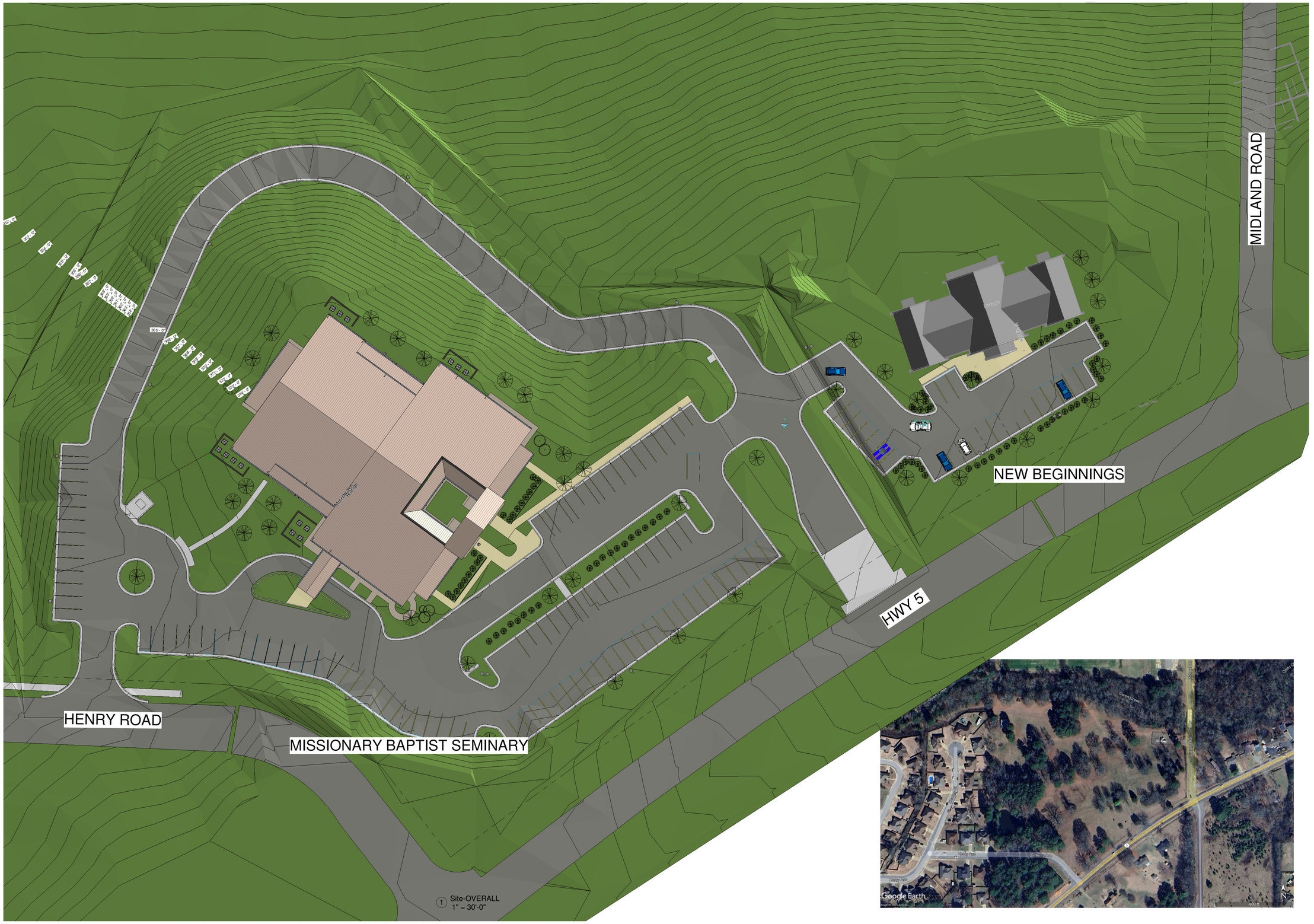
SITE VIEWS

A004




1 Site-OVERALL
1" = 30'-0"

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SITE PLAN

A005

1 FLOOR PLAN
3/16" = 1'-0"

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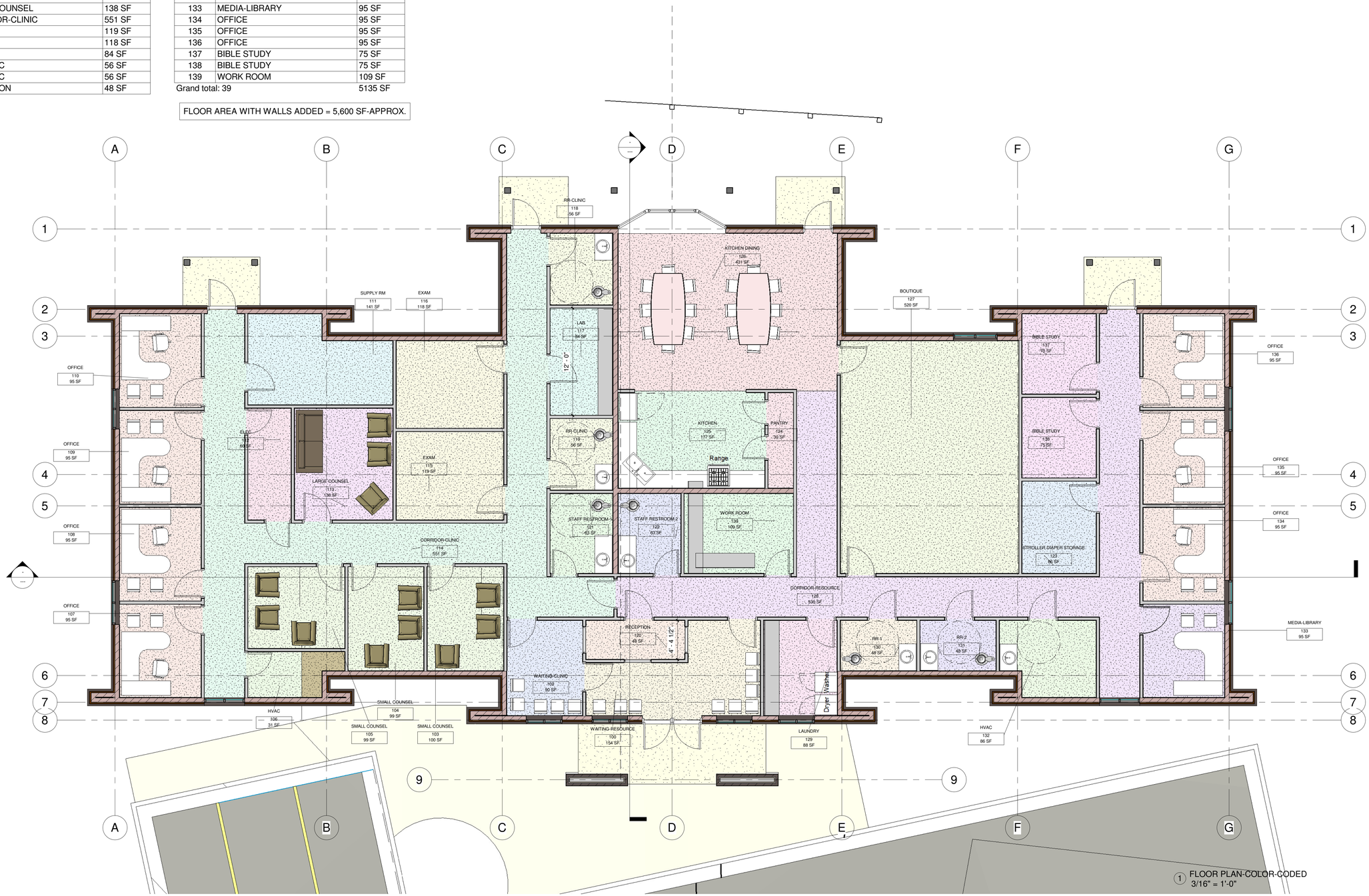
FLOOR PLAN

A101

| ROOM SCHEDULE | | |
|---|---|---|
| NUMBER | NAME | Area |
| 100 | WAITING-RESOURCE | 154 SF |
| 102 | WAITING-CLINIC | 90 SF |
| 103 | SMALL COUNSEL | 100 SF |
| 104 | SMALL COUNSEL | 99 SF |
| 105 | SMALL COUNSEL | 99 SF |
| 106 | HVAC | 31 SF |
| 107 | OFFICE | 95 SF |
| 108 | OFFICE | 95 SF |
| 109 | OFFICE | 95 SF |
| 110 | OFFICE | 95 SF |
| 111 | SUPPLY RM | 141 SF |
| 112 | ELEC | 60 SF |
| 113 | LARGE COUNSEL | 138 SF |
| 114 | CORRIDOR-CLINIC | 551 SF |
| 115 | EXAM | 119 SF |
| 116 | EXAM | 118 SF |
| 117 | LAB | 84 SF |
| 118 | RR-CLINIC | 56 SF |
| 119 | RR-CLINIC | 56 SF |
| 120 | RECEPTION | 48 SF |

| ROOM SCHEDULE | | |
|---|---|---|
| NUMBER | NAME | Area |
| 121 | STAFF RESTROOM-1 | 63 SF |
| 122 | STAFF RESTROOM-2 | 63 SF |
| 123 | STROLLER DIAPER STORAGE | 86 SF |
| 124 | PANTRY | 30 SF |
| 125 | KITCHEN | 177 SF |
| 126 | KITCHEN DINING | 431 SF |
| 127 | BOUTIQUE | 520 SF |
| 128 | CORRIDOR-RESOURCE | 530 SF |
| 129 | LAUNDRY | 88 SF |
| 130 | RR-1 | 48 SF |
| 131 | RR-2 | 48 SF |
| 132 | HVAC | 86 SF |
| 133 | MEDIA-LIBRARY | 95 SF |
| 134 | OFFICE | 95 SF |
| 135 | OFFICE | 95 SF |
| 136 | OFFICE | 95 SF |
| 137 | BIBLE STUDY | 75 SF |
| 138 | BIBLE STUDY | 75 SF |
| 139 | WORK ROOM | 109 SF |
| Grand total: 39 | | 5135 SF |

FLOOR AREA WITH WALLS ADDED = 5,600 SF-APPROX.




1 FLOOR PLAN-COLOR CODED
3/16" = 1'-0"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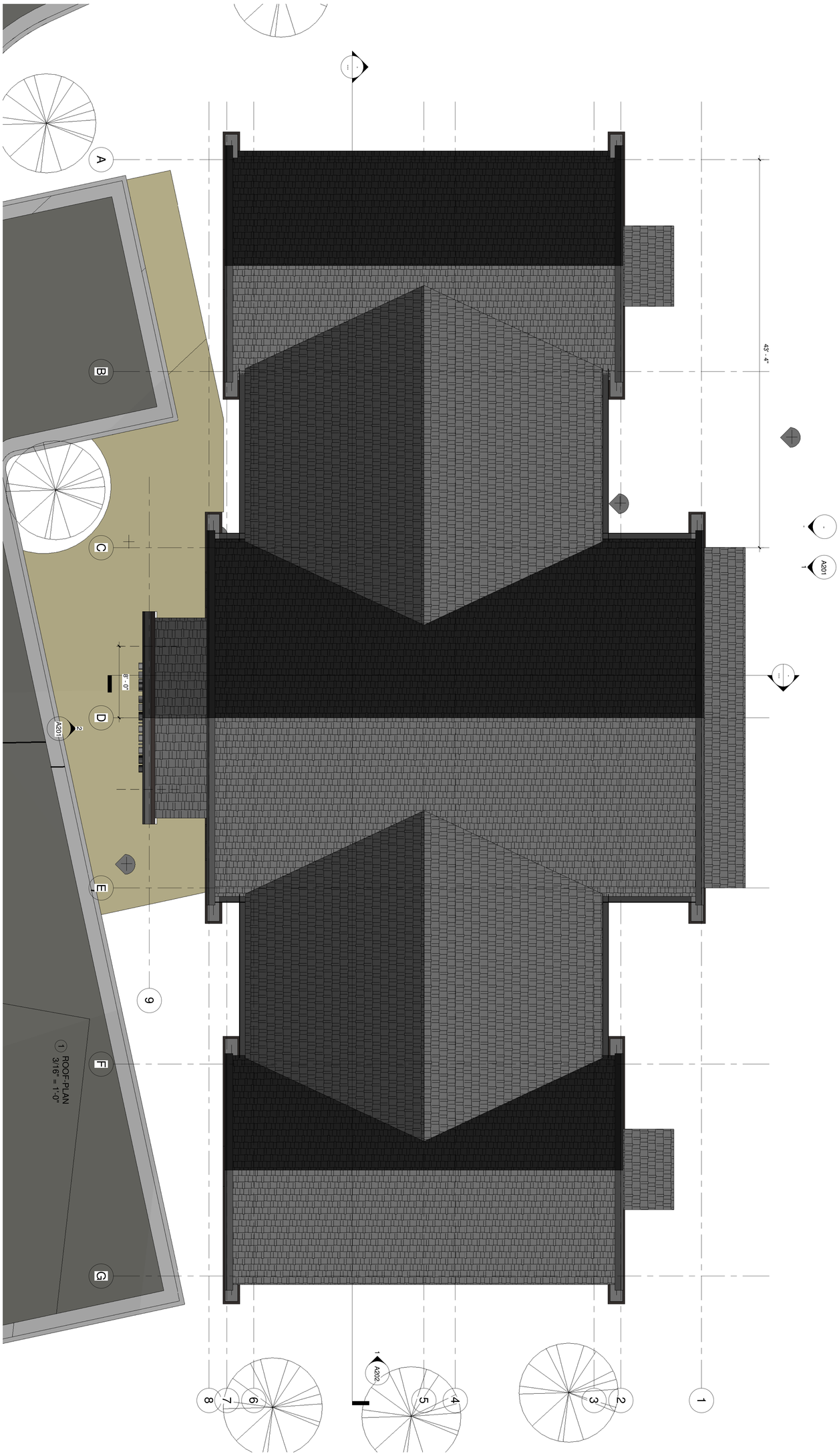
FLOOR PLAN-COLOR CODED

A102




A105

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ROOF PLAN

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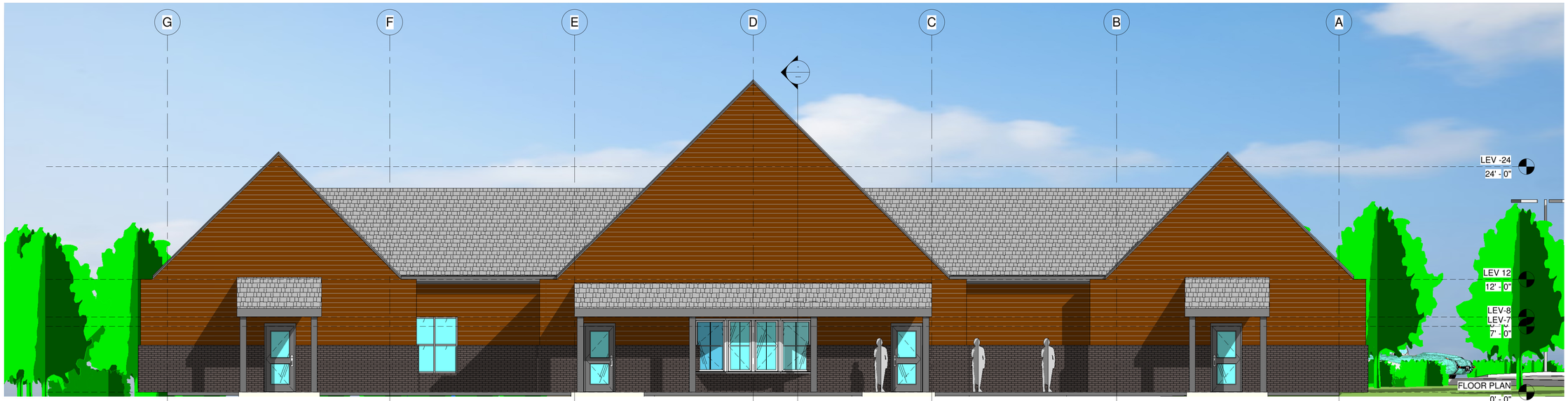
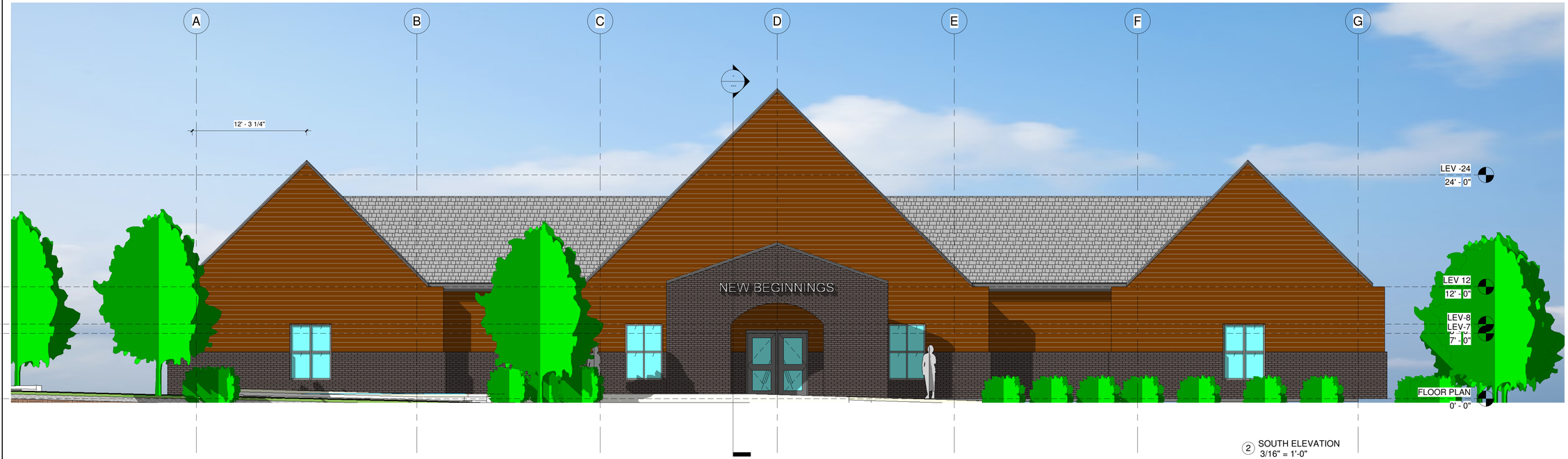



1 NORTH ELEVATION
3/16" = 1'-0"




2 SOUTH ELEVATION
3/16" = 1'-0"

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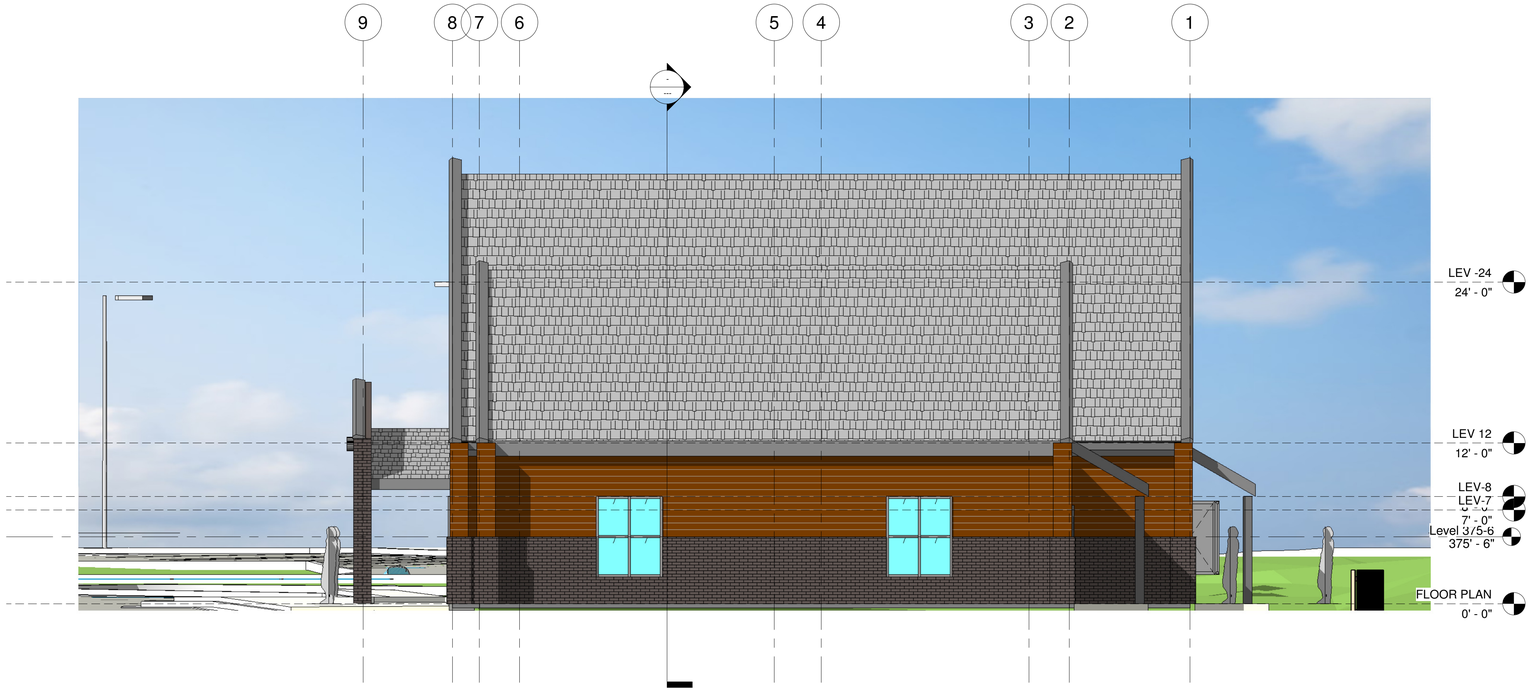
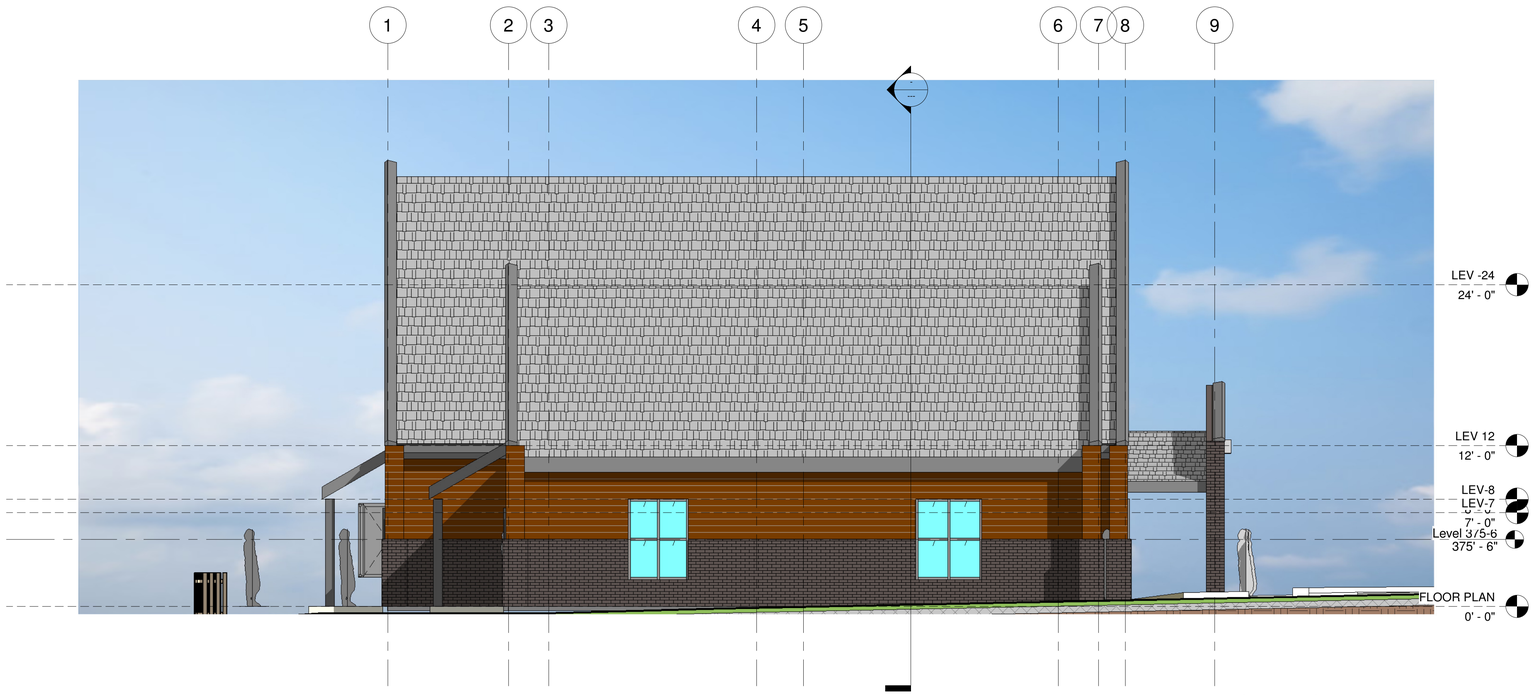
ELEVATIONS

A201




1 EAST ELEVATION
3/16" = 1'-0"




2 WEST ELEVATION
3/16" = 1'-0"

ANDREW D. HICKS ARCHITECT INC
REGISTERED ARCHITECT
NO. C-250
4-7-2025
ARKANSAS

ARCHITECT OF RECORD
ANDREW HICKS ARCHITECT INC

andrew hicks | architect
600 N Mission Blvd.
Fayetteville, Arkansas 72701
m. 501.680.0799
o. 479.332-5050
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**A NEW FACILITY**
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NEW BEGINNINGS
HWY 5, BRYANT, ARKANSAS

ISSUE DATE: 4-7-2025

REVISIONS

| NO. | DATE |
|---|---|
| NO. | |
| NO. | |
| NO. | |
| NO. | |
| NO. | |
| NO. | |

ELEVATIONS

A202

# STORMWATER MANAGEMENT FACILITIES REPORT: CALCULATIONS

**Good Day Farm - Bryant**
**3205 Highway 5 N**
**Bryant, Arkansas**

**Prepared For:**

**Good Day Farm**
425 W. Capitol Avenue
Little Rock, AR 72201
Contact: Ms. Regan Etheridge
Ph. (501) 551-0502

**Prepared By:**

**Stock & Associates Consulting Engineers, Inc.**
257 Chesterfield Business Parkway
St. Louis, Missouri 63005
Ph. 636-530-9100
Fax 636-530-9130
Contact: Mr. Timothy (Ty) Gramling, P.E.

**Date: 06/25/2025**

**STOCK JOB #: 2025-7775**

Report prepared by:

Ty Gramling
Ty Gramling, P.E.
Civil Engineer

Under the direct supervision of:

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
GEORGE STOCK

06-25-2025
George M. Stock, P.E.
Civil Engineer
License No. 9185
Certificate of Authority #4355

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## I. EXECUTIVE SUMMARY

This report was prepared by Stock & Associates Consulting Engineers Inc. on behalf of the developer Good Day Farm, for a new Marijuana Dispensary at 3887 S. Lindbergh Blvd. in Bryant, Arkansas. The project site is zoned as C-2 Highway Commercial. This project is categorized as a "Small Construction Site" per City Stormwater Management Manual since this site has disturbance limits greater than one (1) acre and less than five (5) acres.

One (1) on-site detention basin will be constructed on the site in order to meet stormwater flood protection requirements.

The proposed project will consist of the demolition of an existing building foundation and construction of a new ±2k square foot building. In addition to the one (1) detention basin, the project will also consist of associated parking, one entrance off of Highway No. 5 and one entrance off of Hurricane Lake Road, grading, lighting, landscaping, stormwater drainage, sanitary main extension, and water, and all other associated improvements. The proposed site is located within the Hurricane Creek watershed.

All drainage calculations were done in accordance with City of Bryant Stormwater Management Manual.

## II. INTRODUCTION

### A. Evaluation of Existing Conditions

The existing site consists of 1.98± acres. The existing site includes an existing building foundation near the south end of the site and an existing mobile home near the north end of the site while the remainder is grass-covered with some mature trees. The existing topography ranges from elevations 418 MSD at the southeast corner to 400 at the northwest corner of the property. The existing site drains generally from the south to north. The pre-developed drainage area map is located in Appendix I.

The site lies within Flood Zone X (areas of minimal flood hazard) according to the National Flood Insurance Rate Map Number 05125C0360E with an effective date of June 6, 2020. Refer to Appendix B for the FEMA Firmette.

### B. Evaluation of Proposed Conditions

The proposed improvements will be developed and permitted the City of Bryant and Arkansas Division of Environmental Quality (ADEQ). The proposed development project will involve the construction of a ±2k s.f. building and associated parking. This project shall disturb approximately 1.0 acres of land. The total site will be 34.3% impervious (0.68 Ac.) and 65.7% pervious (1.30 Ac.). Approximately 1.10 total acres will be tributary to the proposed detention basin which includes 0.16 acres of offsite area.

The storm drainage for the proposed development will be taken through the one detention basin. The detention basin will be constructed near the north end of the development to collect and detain runoff from the building/parking area and open space north of the proposed building. The outfall structure will be constructed with a low flow orifice and an intermediate weir to control the post-developed flows from the site to be less than pre-developed. The 18" outfall pipe for basin will drain into a proposed 2' wide swale. All detention and storm sewer facilities are designed to meet City of Bryant stormwater requirements. See Appendix I for the Proposed Drainage Area Map.

## III. STORM SEWER HYDRAULICS, OPEN CHANNEL FLOW & DETENTION DESIGN

### A. Storm Sewer Hydraulics

All proposed storm sewer facilities for this development were designed to convey the 100-year storm event. The Rational Method was used to determine the flow rate for each drainage area and the Manning's equation was used to verify the pipe sizes. Runoff coefficients used to determine storm sewer flow rates for the site are 0.51 for open space/grass (C soils) and 0.95 for impervious areas (C soils). Using Exhibit 400-1 (in the City of Bryant Stormwater Management Manual) and assuming a time of concentration of 5 minutes, a rainfall intensity of 10 in/hour was used. Refer to the Appendix C of this report for the storm sewer hydraulics.

### B. Open Channel Flow

Proposed open channels for this development shall be designed to convey the 100-year storm event. A proposed 2' wide flat bottom grass lined channel with 3:1 side slopes is being proposed near the northwest portion of the site to convey the drainage offsite to the north from the proposed detention basin. Channel calculations were taken at Section A-A at the outlet pipe from the basin and Section B-B near the north end of the site. The channel calculations is included in Appendix D of this report. The proposed drainage channel shall be located within a drainage easement as shown on the Site Grading Plan sheet C5.0 located in Appendix G.

### C. Detention Design

Proposed detention was designed per City of Bryant's Stormwater Management Manual. The detention basin will be sized to provide detention for the 2, 10, 25, 50 and 100 year storm events. Runoff from the new development will be controlled so that the post-development peak rate of runoff does not exceed that of the pre-development. The detention basin shall be located within a drainage easement as shown on the Site Grading Plan sheet C5.0 located in Appendix G.

### Pre-Developed Conditions

The existing drainage area used to determine the current release rates of the proposed detention basin are shown on the pre-developed drainage area map included in Appendix I. The runoff calculations for the pre-developed conditions is included in Appendix E. The pre-developed release rates consist of the following:

**TABLE 1**

**Allowable Peak Discharge**
**Pre-Developed Conditions**

| ***Design Storm (Year)*** | ***Pre- Development Runoff (c.f.s.)*** |
|---|---|
| 2 | 2.53 |
| 10 | 4.61 |
| 25 | 5.77 |
| 50 | 7.22 |
| 100 | 7.75 |

Post-Developed Conditions

For the proposed development, one (1) detention basin will be utilized to provide flood protection. The proposed detention basin is located at the north end of the development. Post-Developed drainage area map is included in Appendix O. All hydrologic calculations for this report were done using Haestad Methods QRT55 computer modeling software. Haestad Methods Pondpack v8i was used for the hydraulic modeling and routing the hydrographs. For this analysis the time of concentration was set to 6 minutes, which is the minimum time of concentration and provides a more conservative post development scenario.

Structure #2.1 located within the basin will serve as the outfall structure for the development utilizing a 2' wide x 4" tall weir (2 sides) as the low flow orifice to control stormwater release from the site. The top of the structure will serve as the emergency spillway and has been designed to accommodate the 100 year flow. The 18" outlet pipe will drain the runoff northerly and drain into an unnamed tributary flowing northerly along the east side of Hurricane Lake Road.

The following tables shows a summary of the 2, 10, 25, 50 and 100 year pre and post-developed flow rates along with the corresponding pond water surface elevation (WSEL) that were calculated for the detention pond for the post development condition model and post development condition model with low flow blocked.

**TABLE 2**

**Peak Discharge - Post-Developed Conditions**

| *Design Storm (Year)* | *Pre-Developed Discharge (cfs)* | *Post-Developed Discharge (cfs)* |
|---|---|---|
| 2 | 2.53 | 1.81 |
| 10 | 4.61 | 3.73 |
| 25 | 5.77 | 5.83 |
| 50 | 7.22 | 6.44 |
| 100 | 7.75 | 6.92 |

**TABLE 3**

**Stormwater Detention Summary**

| *Design Storm (Year)* | *Basin Discharge (cfs)* | *Basin WSEL (feet)* | *Basin Freeboard (feet)* |
|---|---|---|---|
| 2 | 1.81 | 406.46 | 3.54 |
| 10 | 3.73 | 407.31 | 2.69 |
| 25 | 5.83 | 407.44 | 2.56 |
| 50 | 6.44 | 407.72 | 2.28 |
| 100 | 6.92 | 407.82 | 2.18 |

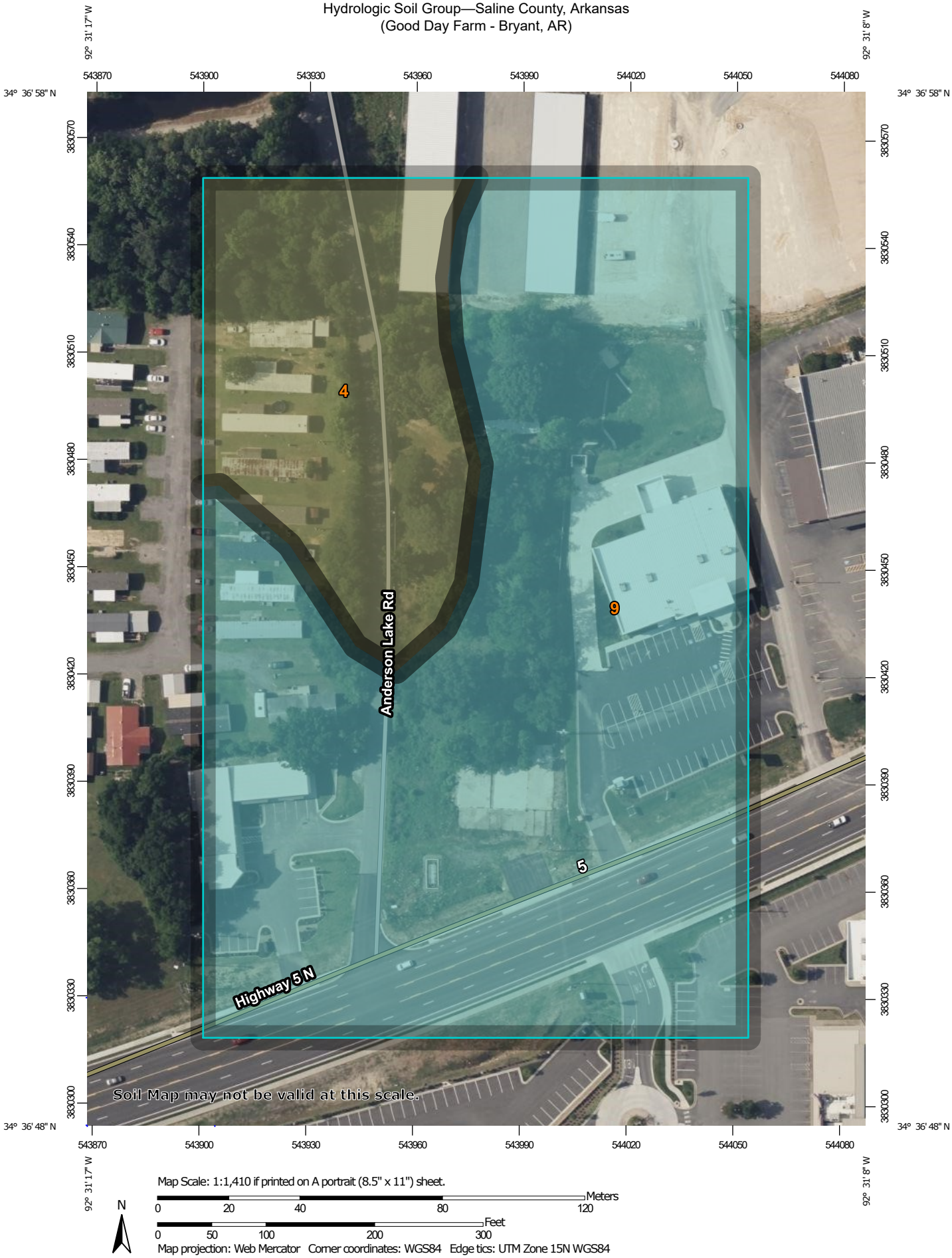
## IV. SUMMARY

All proposed drainage improvements were designed in accordance with the City of Bryant Stormwater Management Manual. There is one (1) proposed on-site detention basin that will be utilized for flood protection for the proposed development. Included at the end of this reports are backup data, drainage area maps and supporting calculations for this project.

## V. APPENDICES

# APPENDIX A:
# USDA NATUAL RESOURCES CONSERVATION SERVICE SOIL MAP

Hydrologic Soil Group—Saline County, Arkansas
(Good Day Farm - Bryant, AR)




Map Scale: 1:1,410 if printed on A portrait (8.5" x 11") sheet.

N

Meters
0 20 40 80 120

Feet
0 50 100 200 300

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 15N WGS84

## MAP LEGEND

**Area of Interest (AOI)**
- Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**
- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

**Soil Rating Lines**
- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

**Soil Rating Points**
- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

**Water Features**
- Streams and Canals

**Transportation**
- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

**Background**
- Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Saline County, Arkansas
Survey Area Data: Version 21, Sep 10, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 1, 2022—May 29, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|---|---|---|---|---|
| 4 | Amy-Gurdon complex, 0 to 3 percent slopes, mounded | C/D | 2.1 | 22.8% |
| 9 | Carnasaw-Townley association, undulating | C | 7.1 | 77.2% |
| **Totals for Area of Interest** | | | **9.1** | **100.0%** |

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff: None Specified*

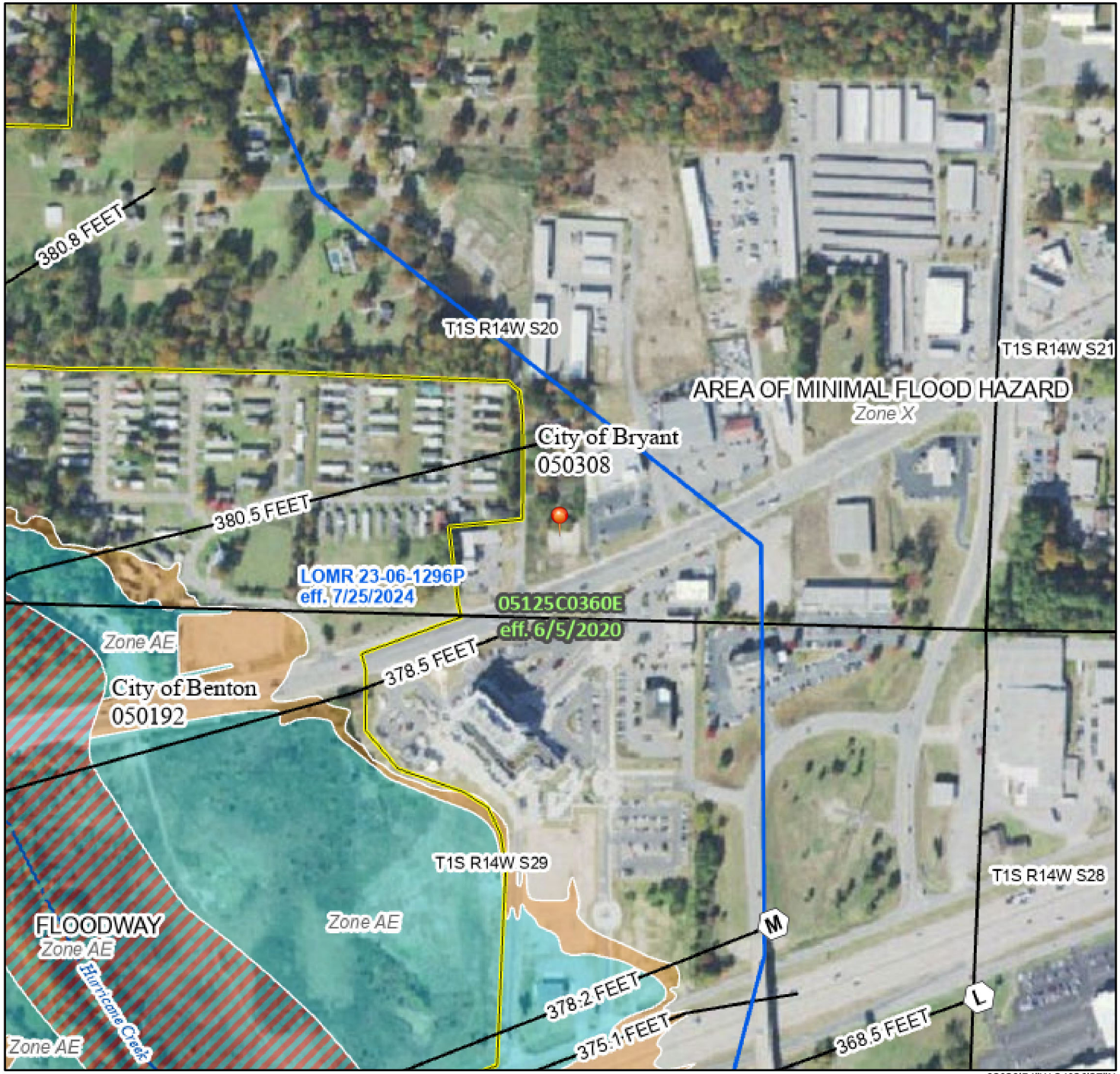
*Tie-break Rule:* Higher

# APPENDIX B:
# FEMA FIRMETTE

# National Flood Hazard Layer FIRMette

FEMA

92°31'32"W 34°37'7"N




92°30'54"W 34°36'37"N

0 250 500 1,000 1,500 2,000 Feet

1:6,000

*Basemap Imagery Source: USGS National Map 2023*

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

**SPECIAL FLOOD HAZARD AREAS**
- Without Base Flood Elevation (BFE) *Zone A, V, A99*
- With BFE or Depth *Zone AE, AO, AH, VE, AR*
- Regulatory Floodway

**OTHER AREAS OF FLOOD HAZARD**
- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X*
- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

**OTHER AREAS**
- NO SCREEN Area of Minimal Flood Hazard *Zone X*
- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

**GENERAL STRUCTURES**
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

**OTHER FEATURES**
- 20.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- 513 Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

**MAP PANELS**
- Digital Data Available
- No Digital Data Available
- Unmapped

N

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/24/2025 at 3:59 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

# APPENDIX C:
# STORM SEWER HYDRAULIC CALCULATIONS

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **Project name:** | | *GDF - BRYANT* | | | **Calculated By:** | | *L.C.W.* | | 100-year Pipe Hydraulics | | | | | | | | | | | | | | | | | | | | | | |
| **Project number:** | | *2024-7775* | | | **Checked By:** | | *G.M.S.* | | ***Bend Coefficients :*** | | | | | | | | | Revisions: | | | | | | | | | | | | | |
| **Project Location:** | | *BRYANT, AR* | | | **Date:** | | *6/25/2025* | | $5^0 = 0.06$ | $20^0 = 0.24$ | $35^0 = 0.4$ | $50^0 = 0.50$ | $65^0 = 0.57$ | $80^0 = 0.65$ | | | | | | | | | | | | | | | | | |
| | **LINE** | | **FLOW LINE ELEVATIONS** | | | | | | $10^0 = 0.11$ | $25^0 = 0.30$ | $40^0 = 0.43$ | $55^0 = 0.52$ | $70^0 = 0.60$ | $85^0 = 0.67$ | | | **HEAD LOSS** | | | | | **Hydraulic Elevations** | | | | | | | | | |
| | | | | | | | | | $15^0 = 0.18$ | $30^0 = 0.35$ | $45^0 = 0.47$ | $60^0 = 0.55$ | $75^0 = 0.62$ | $90^0 = 0.70$ | | | | | | | | | | | **Structure** | **Top/Sill** | **Free** | | | **Velocity** |
| **Structure Number** | **Upper structure** | **Lower structure** | **Upper structure** | **Lower Structure** | **Length (ft)** | **Flowline Grade ft/ft** | **Pipe Size (in.)** | **Full Flow Cap. (cfs)** | **Total (Q) (cfs)** | **Mean Full Flow Vel.(V) (ft/s)** | **Bend Coef.** | **Curve Coef.** | **Velocity Head ($V_h$) (ft)** | **$QV_h$ ($ft^4/s$)** | **Pipe Coef. (n)** | **$H_f$ (ft)** | **Junction (ft)** | **Bend (ft)** | **Curve (ft)** | **Total $H_{mt}$** | **Upper F.L + Dia.** | **Lower H.E. $+H_f$** | **Lower H.E.** | **Upper H.E. + $H_{mt}$** | **Top/Sill Structure Elevation** | **Free Board** | **Structure Number** | **Remarks** | **Mannings Formula (ft/s)** |
| 2.1 | 2.1 | 2.0 | 401.87 | 401.43 | 48.16 | 0.0091 | 18 | 10.05 | 4.45 | 2.52 | 0.00 | 0.00 | 0.10 | 0.44 | 0.013 | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | 403.37 | 403.02 | 402.93 | 403.37 | 408.00 | 4.63 | 2.1 | Outfall Structure | 5.69 |
| 2.0 | 2.0 | | 401.43 | | | | | | | | | | | | | | | | | Top of Pipe = | | | | 402.93 | | | 2.0 | FES | |
| 1.4 | 1.4 | 1.1 | 406.63 | 405.58 | 34.64 | 0.0100 | 12 | 3.57 | 0.37 | 0.47 | 0.00 | 0.00 | 0.00 | 0.00 | 0.013 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 407.63 | 406.95 | 406.95 | 407.63 | 409.83 | 2.20 | 1.4 | Curb Inlet | 4.55 |
| 1.1 | 1.1 | | 405.58 | | | | | | | | | | | | | | | | | From Below = | | | | 406.95 | | | 1.1 | Grate Inlet | |
| 1.3 | 1.3 | 1.2 | 407.16 | 406.58 | 57.72 | 0.0100 | 12 | 3.57 | 0.46 | 0.59 | 0.00 | 0.00 | 0.01 | 0.00 | 0.013 | 0.01 | 0.01 | 0.00 | 0.00 | 0.01 | 408.16 | 407.69 | 407.68 | 408.17 | 410.37 | 2.20 | 1.3 | Curb Inlet | 4.55 |
| 1.2 | 1.2 | 1.1 | 406.58 | 405.58 | 100.12 | 0.0100 | 12 | 3.57 | 1.45 | 1.85 | 0.60 | 0.00 | 0.05 | 0.08 | 0.013 | 0.17 | 0.07 | 0.03 | 0.00 | 0.10 | 407.58 | 407.12 | 406.95 | 407.68 | 409.69 | 2.01 | 1.2 | Grate Inlet | 4.55 |
| 1.1 | 1.1 | 1.0 | 405.58 | 405.00 | 57.93 | 0.0100 | 15 | 6.48 | 3.02 | 2.46 | 0.30 | 0.00 | 0.09 | 0.28 | 0.013 | 0.13 | 0.09 | 0.03 | 0.00 | 0.12 | 406.83 | 406.38 | 406.25 | 406.95 | 408.22 | 1.27 | 1.1 | Grate Inlet | 5.28 |
| 1.0 | 1.0 | | 405.00 | | | | | | | | | | | | | | | | | Top of Pipe = | | | | 406.25 | | | 1.0 | FES | |

**MEAN FULL FLOW VELOCITY:** $V = Q_{ACT}./A_{PIPE}$

**FRICTION LOSS ($H_f$) :** $Hf = 2.87\ n^2\ (LV^2/d^{1.33})$

**VELOCITY HEAD :** $V_h = V^2/2g$

**JUNCTION LOSES (JUNC.) = [ $Q_{out}Vh_{out}$ - Sum ($Q_{in}V_{in}$)]x1.33/[$Q_{out}$]**

**BEND LOSES (BEND) = ($V^h$) * ANGLE COEFFICIENT**

**CURVE LOSS=$V_h$*CURVE COEFFICIENT**

**Note:**

1. IF MORE THAN ONE INCOMING LINE, CALC. EACH BEND LOSS AND ADD TOGETHER.
2. NO STRUCTURE LOSES TO BE CALCULATED AT A DROP
3. IF $QV_{h(in)} > QV_{h(out)}$, NO JUNCTION LOSES TO BE CALCULATED.

**Note(s):**

# APPENDIX D:
# OPEN CHANNEL
# CALCULATIONS

# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Wednesday, Jun 25 2025

## Ditch Section A-A

**Trapezoidal**

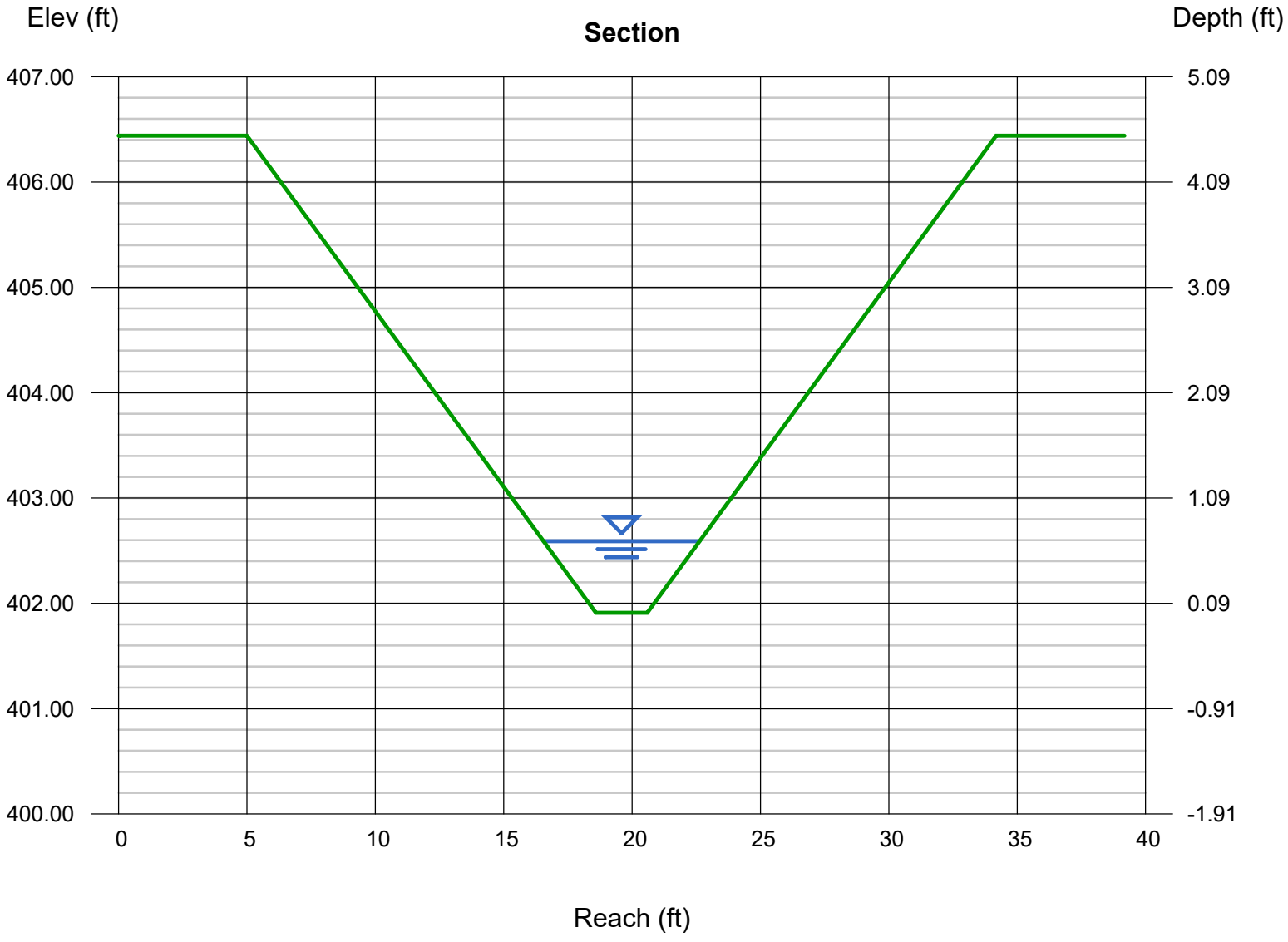
| | |
|---|---|
| Bottom Width (ft) | = 2.00 |
| Side Slopes (z:1) | = 3.00, 3.00 |
| Total Depth (ft) | = 4.53 |
| Invert Elev (ft) | = 401.91 |
| Slope (%) | = 0.83 |
| N-Value | = 0.018 |

**Calculations**

| | |
|---|---|
| Compute by: | Known Q |
| Known Q (cfs) | = 11.62 |

**Highlighted**

| | |
|---|---|
| Depth (ft) | = 0.68 |
| Q (cfs) | = 11.62 |
| Area (sqft) | = 2.75 |
| Velocity (ft/s) | = 4.23 |
| Wetted Perim (ft) | = 6.30 |
| Crit Depth, Yc (ft) | = 0.72 |
| Top Width (ft) | = 6.08 |
| EGL (ft) | = 0.96 |



# Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Wednesday, Jun 25 2025

## Ditch Section B-B

**Trapezoidal**

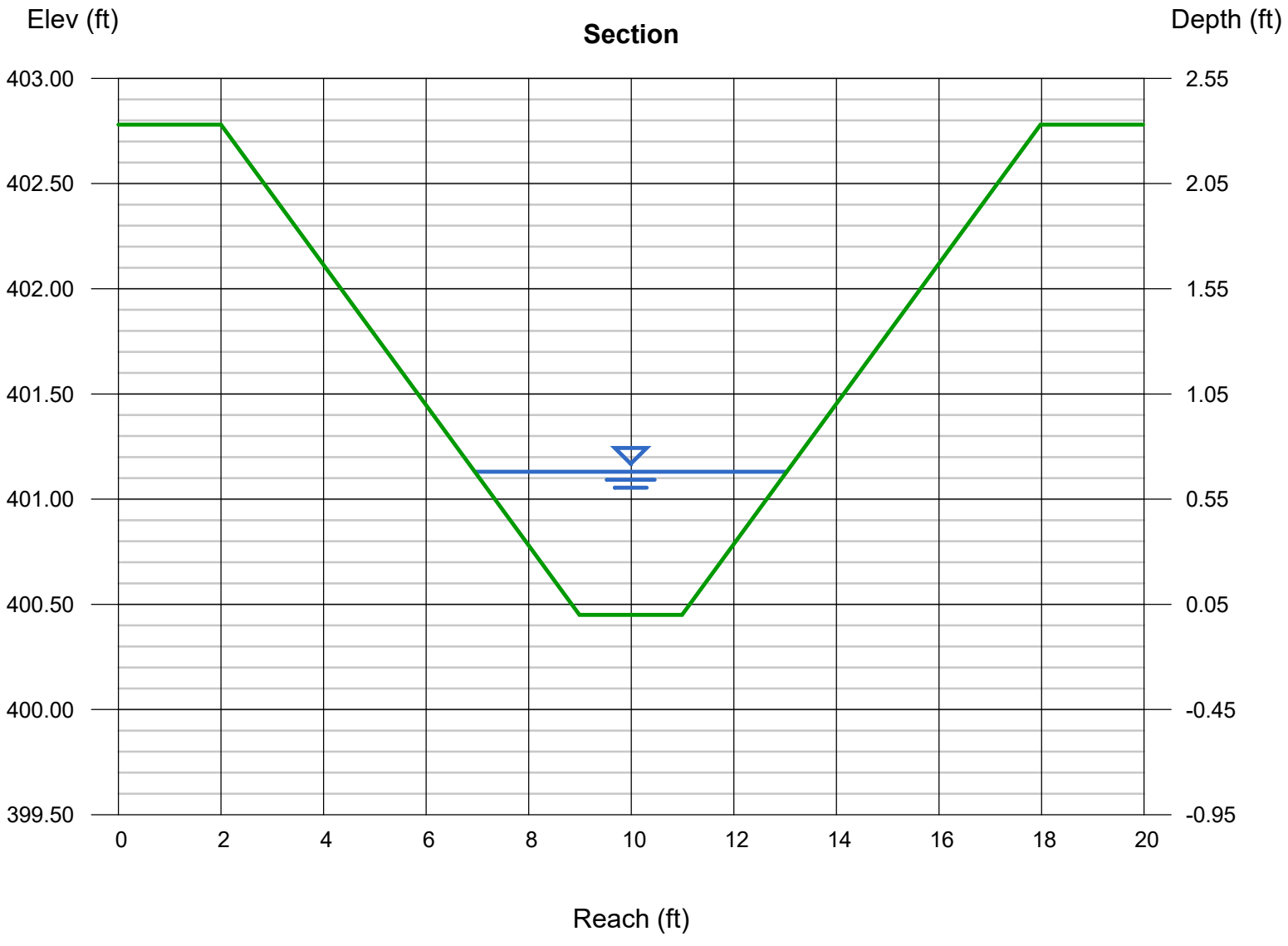
| | |
|---|---|
| Bottom Width (ft) | = 2.00 |
| Side Slopes (z:1) | = 3.00, 3.00 |
| Total Depth (ft) | = 2.33 |
| Invert Elev (ft) | = 400.45 |
| Slope (%) | = 0.83 |
| N-Value | = 0.018 |

**Calculations**

| | |
|---|---|
| Compute by: | Known Q |
| Known Q (cfs) | = 11.62 |

**Highlighted**

| | |
|---|---|
| Depth (ft) | = 0.68 |
| Q (cfs) | = 11.62 |
| Area (sqft) | = 2.75 |
| Velocity (ft/s) | = 4.23 |
| Wetted Perim (ft) | = 6.30 |
| Crit Depth, Yc (ft) | = 0.72 |
| Top Width (ft) | = 6.08 |
| EGL (ft) | = 0.96 |



# APPENDIX E:
# RUNOFF & STORAGE CALCULATIONS
# PRE-DEVELOPED CONDITIONS

# Pre-Development Conditions

| Project Summary | |
|---|---|
| Title | Good Day Farm - Bryant |
| Engineer | Ty Gramling |
| Company | Stock & Associates |
| Date | 6/25/2025 |

| Notes | Pre-Development Conditions |
|---|---|

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# Pre-Development Conditions

Subsection: User Notifications

| | |
|---|---|
| User Notifications? | No user notifications generated. |

# Pre-Development Conditions

Subsection: Master Network Summary

## Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft³/s) |
|---|---|---|---|---|---|
| Pre-Developed | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.190 | 12.100 | 2.30 |
| Pre-Developed | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.340 | 12.100 | 4.16 |
| Pre-Developed | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.425 | 12.100 | 5.19 |
| Pre-Developed | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.533 | 12.100 | 6.49 |
| Pre-Developed | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.573 | 12.100 | 6.96 |
| Offsite | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.020 | 12.133 | 0.23 |
| Offsite | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.037 | 12.100 | 0.45 |
| Offsite | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.047 | 12.100 | 0.57 |
| Offsite | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.060 | 12.100 | 0.73 |
| Offsite | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.065 | 12.100 | 0.79 |

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow (ft³/s) |
|---|---|---|---|---|---|
| Point of Interest | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.210 | 12.100 | 2.53 |
| Point of Interest | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.377 | 12.100 | 4.61 |
| Point of Interest | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.472 | 12.100 | 5.77 |

# Pre-Development Conditions

Subsection: Master Network Summary

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| Point of Interest | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.593 | 12.100 | 7.22 |
| Point of Interest | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.637 | 12.100 | 7.75 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Time-Depth Curve: TypeIII 24hr (4.3 in) | |
|---|---|
| Label | TypeIII 24hr (4.3 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 2 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.000 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 3.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 5.000 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 6.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 6.500 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 7.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 7.500 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 |
| 8.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 8.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 9.000 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 |
| 9.500 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 |
| 10.000 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 |
| 10.500 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 |
| 11.000 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 |
| 11.500 | 1.3 | 1.4 | 1.5 | 1.6 | 1.8 |
| 12.000 | 2.1 | 2.5 | 2.7 | 2.8 | 2.9 |
| 12.500 | 3.0 | 3.1 | 3.1 | 3.2 | 3.2 |
| 13.000 | 3.2 | 3.3 | 3.3 | 3.3 | 3.3 |
| 13.500 | 3.4 | 3.4 | 3.4 | 3.4 | 3.5 |
| 14.000 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 |
| 14.500 | 3.6 | 3.6 | 3.6 | 3.6 | 3.7 |
| 15.000 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| 15.500 | 3.7 | 3.8 | 3.8 | 3.8 | 3.8 |
| 16.000 | 3.8 | 3.8 | 3.8 | 3.8 | 3.9 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 3.9 | 3.9 | 3.9 | 3.9 | 3.9 |
| 17.000 | 3.9 | 3.9 | 3.9 | 3.9 | 3.9 |
| 17.500 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 18.000 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 18.500 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 19.000 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 19.500 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 20.000 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 20.500 | 4.1 | 4.1 | 4.2 | 4.2 | 4.2 |
| 21.000 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 21.500 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 22.000 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 22.500 | 4.2 | 4.2 | 4.2 | 4.3 | 4.3 |
| 23.000 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |
| 23.500 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |
| 24.000 | 4.3 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Time-Depth Curve: TypeIII 24hr (6.0 in) | |
|---|---|
| Label | TypeIII 24hr (6.0 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 10 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 |
| 4.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.000 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 |
| 5.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 6.000 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 |
| 6.500 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 7.000 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 |
| 7.500 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 |
| 8.000 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 |
| 8.500 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 |
| 9.000 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 |
| 9.500 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 |
| 10.000 | 1.1 | 1.2 | 1.2 | 1.2 | 1.3 |
| 10.500 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |
| 11.000 | 1.5 | 1.5 | 1.6 | 1.7 | 1.7 |
| 11.500 | 1.8 | 1.9 | 2.0 | 2.2 | 2.5 |
| 12.000 | 3.0 | 3.5 | 3.8 | 4.0 | 4.1 |
| 12.500 | 4.2 | 4.3 | 4.3 | 4.4 | 4.5 |
| 13.000 | 4.5 | 4.5 | 4.6 | 4.6 | 4.7 |
| 13.500 | 4.7 | 4.7 | 4.8 | 4.8 | 4.8 |
| 14.000 | 4.9 | 4.9 | 4.9 | 5.0 | 5.0 |
| 14.500 | 5.0 | 5.0 | 5.1 | 5.1 | 5.1 |
| 15.000 | 5.1 | 5.1 | 5.2 | 5.2 | 5.2 |
| 15.500 | 5.2 | 5.2 | 5.3 | 5.3 | 5.3 |
| 16.000 | 5.3 | 5.3 | 5.3 | 5.4 | 5.4 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| 17.000 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 17.500 | 5.5 | 5.5 | 5.5 | 5.5 | 5.6 |
| 18.000 | 5.6 | 5.6 | 5.6 | 5.6 | 5.6 |
| 18.500 | 5.6 | 5.6 | 5.6 | 5.6 | 5.7 |
| 19.000 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| 19.500 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| 20.000 | 5.7 | 5.7 | 5.8 | 5.8 | 5.8 |
| 20.500 | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |
| 21.000 | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |
| 21.500 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 22.000 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 22.500 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 23.000 | 5.9 | 6.0 | 6.0 | 6.0 | 6.0 |
| 23.500 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 24.000 | 6.0 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Time-Depth Curve: TypeIII 24hr (6.9 in) | |
|---|---|
| Label | TypeIII 24hr (6.9 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 25 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.500 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.500 | 0.4 | 0.5 | 0.5 | 0.5 | 0.5 |
| 6.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 6.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 7.000 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 |
| 7.500 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 |
| 8.000 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 |
| 8.500 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 |
| 9.000 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 |
| 9.500 | 1.1 | 1.2 | 1.2 | 1.2 | 1.3 |
| 10.000 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |
| 10.500 | 1.5 | 1.5 | 1.6 | 1.6 | 1.7 |
| 11.000 | 1.7 | 1.8 | 1.8 | 1.9 | 2.0 |
| 11.500 | 2.1 | 2.2 | 2.3 | 2.6 | 2.9 |
| 12.000 | 3.4 | 4.0 | 4.3 | 4.6 | 4.7 |
| 12.500 | 4.8 | 4.9 | 5.0 | 5.1 | 5.1 |
| 13.000 | 5.2 | 5.2 | 5.3 | 5.3 | 5.4 |
| 13.500 | 5.4 | 5.4 | 5.5 | 5.5 | 5.6 |
| 14.000 | 5.6 | 5.6 | 5.7 | 5.7 | 5.7 |
| 14.500 | 5.8 | 5.8 | 5.8 | 5.8 | 5.9 |
| 15.000 | 5.9 | 5.9 | 5.9 | 6.0 | 6.0 |
| 15.500 | 6.0 | 6.0 | 6.1 | 6.1 | 6.1 |
| 16.000 | 6.1 | 6.1 | 6.1 | 6.2 | 6.2 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 6.2 | 6.2 | 6.2 | 6.2 | 6.3 |
| 17.000 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |
| 17.500 | 6.3 | 6.4 | 6.4 | 6.4 | 6.4 |
| 18.000 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |
| 18.500 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 19.000 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 19.500 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| 20.000 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| 20.500 | 6.6 | 6.7 | 6.7 | 6.7 | 6.7 |
| 21.000 | 6.7 | 6.7 | 6.7 | 6.7 | 6.7 |
| 21.500 | 6.7 | 6.7 | 6.7 | 6.8 | 6.8 |
| 22.000 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 |
| 22.500 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 |
| 23.000 | 6.8 | 6.8 | 6.9 | 6.9 | 6.9 |
| 23.500 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| 24.000 | 6.9 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Time-Depth Curve: TypeIII 24hr (8.0 in) | |
|---|---|
| Label | TypeIII 24hr (8.0 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 50 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 2.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.000 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 5.500 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 |
| 6.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 6.500 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 |
| 7.000 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 |
| 7.500 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 |
| 8.000 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 |
| 8.500 | 1.0 | 1.1 | 1.1 | 1.1 | 1.1 |
| 9.000 | 1.2 | 1.2 | 1.2 | 1.3 | 1.3 |
| 9.500 | 1.3 | 1.4 | 1.4 | 1.4 | 1.5 |
| 10.000 | 1.5 | 1.6 | 1.6 | 1.6 | 1.7 |
| 10.500 | 1.7 | 1.8 | 1.8 | 1.9 | 1.9 |
| 11.000 | 2.0 | 2.1 | 2.1 | 2.2 | 2.3 |
| 11.500 | 2.4 | 2.5 | 2.7 | 3.0 | 3.3 |
| 12.000 | 4.0 | 4.7 | 5.0 | 5.3 | 5.5 |
| 12.500 | 5.6 | 5.7 | 5.8 | 5.9 | 5.9 |
| 13.000 | 6.0 | 6.1 | 6.1 | 6.2 | 6.2 |
| 13.500 | 6.3 | 6.3 | 6.4 | 6.4 | 6.4 |
| 14.000 | 6.5 | 6.5 | 6.6 | 6.6 | 6.6 |
| 14.500 | 6.7 | 6.7 | 6.7 | 6.8 | 6.8 |
| 15.000 | 6.8 | 6.9 | 6.9 | 6.9 | 6.9 |
| 15.500 | 7.0 | 7.0 | 7.0 | 7.0 | 7.1 |
| 16.000 | 7.1 | 7.1 | 7.1 | 7.1 | 7.2 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 7.2 | 7.2 | 7.2 | 7.2 | 7.3 |
| 17.000 | 7.3 | 7.3 | 7.3 | 7.3 | 7.3 |
| 17.500 | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 |
| 18.000 | 7.4 | 7.4 | 7.4 | 7.5 | 7.5 |
| 18.500 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 |
| 19.000 | 7.5 | 7.6 | 7.6 | 7.6 | 7.6 |
| 19.500 | 7.6 | 7.6 | 7.6 | 7.6 | 7.6 |
| 20.000 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| 20.500 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| 21.000 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 21.500 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 22.000 | 7.8 | 7.9 | 7.9 | 7.9 | 7.9 |
| 22.500 | 7.9 | 7.9 | 7.9 | 7.9 | 7.9 |
| 23.000 | 7.9 | 7.9 | 7.9 | 8.0 | 8.0 |
| 23.500 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| 24.000 | 8.0 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Time-Depth Curve: TypeIII 24hr (8.4 in) | |
|---|---|
| Label | TypeIII 24hr (8.4 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 100 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| 2.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 |
| 4.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.500 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 |
| 5.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 5.500 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 |
| 6.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 |
| 6.500 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |
| 7.000 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| 7.500 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| 8.000 | 1.0 | 1.0 | 1.0 | 1.0 | 1.1 |
| 8.500 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 |
| 9.000 | 1.2 | 1.3 | 1.3 | 1.3 | 1.4 |
| 9.500 | 1.4 | 1.4 | 1.5 | 1.5 | 1.5 |
| 10.000 | 1.6 | 1.6 | 1.7 | 1.7 | 1.8 |
| 10.500 | 1.8 | 1.9 | 1.9 | 2.0 | 2.0 |
| 11.000 | 2.1 | 2.2 | 2.2 | 2.3 | 2.4 |
| 11.500 | 2.5 | 2.6 | 2.9 | 3.1 | 3.5 |
| 12.000 | 4.2 | 4.9 | 5.3 | 5.5 | 5.8 |
| 12.500 | 5.9 | 6.0 | 6.1 | 6.2 | 6.2 |
| 13.000 | 6.3 | 6.4 | 6.4 | 6.5 | 6.5 |
| 13.500 | 6.6 | 6.6 | 6.7 | 6.7 | 6.8 |
| 14.000 | 6.8 | 6.9 | 6.9 | 6.9 | 7.0 |
| 14.500 | 7.0 | 7.0 | 7.1 | 7.1 | 7.1 |
| 15.000 | 7.2 | 7.2 | 7.2 | 7.3 | 7.3 |
| 15.500 | 7.3 | 7.3 | 7.4 | 7.4 | 7.4 |
| 16.000 | 7.4 | 7.5 | 7.5 | 7.5 | 7.5 |

# Pre-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 7.5 | 7.6 | 7.6 | 7.6 | 7.6 |
| 17.000 | 7.6 | 7.7 | 7.7 | 7.7 | 7.7 |
| 17.500 | 7.7 | 7.7 | 7.8 | 7.8 | 7.8 |
| 18.000 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 18.500 | 7.9 | 7.9 | 7.9 | 7.9 | 7.9 |
| 19.000 | 7.9 | 7.9 | 7.9 | 8.0 | 8.0 |
| 19.500 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| 20.000 | 8.0 | 8.0 | 8.1 | 8.1 | 8.1 |
| 20.500 | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 |
| 21.000 | 8.1 | 8.2 | 8.2 | 8.2 | 8.2 |
| 21.500 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 |
| 22.000 | 8.2 | 8.2 | 8.3 | 8.3 | 8.3 |
| 22.500 | 8.3 | 8.3 | 8.3 | 8.3 | 8.3 |
| 23.000 | 8.3 | 8.3 | 8.3 | 8.3 | 8.4 |
| 23.500 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 |
| 24.000 | 8.4 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 68.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.087 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 68.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.087 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 68.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.087 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 68.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.087 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 68.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.087 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 40.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.057 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 40.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.057 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 40.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.057 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 40.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.057 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 40.00 ft |
| Manning's n | 0.240 |
| Slope | 0.078 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.057 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | False |
| Slope | 0.056 ft/ft |
| Average Velocity | 3.82 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #3: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 90.00 ft |
| Is Paved? | False |
| Slope | 0.073 ft/ft |
| Average Velocity | 4.36 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 34.00 ft |
| Is Paved? | False |
| Slope | 0.016 ft/ft |
| Average Velocity | 2.04 ft/s |
| Segment Time of Concentration | 0.005 hours |

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 24.20 ft |
| Manning's n | 0.013 |
| Slope | 0.039 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 9.10 ft/s |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Segment #5: TR-55 Channel Flow | |
|---|---|
| Segment Time of Concentration | 0.001 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Pre-Development Conditions

Subsection: Time of Concentration Calculations
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp<br>V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n<br><br>(Lf / V) / 3600 |
| Where: | R= Hydraulic radius<br>Aq= Flow area, square feet<br>Wp= Wetted perimeter, feet<br>V= Velocity, ft/sec<br>Sf= Slope, ft/ft<br>n= Manning's n<br>Tc= Time of concentration, hours<br>Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface:<br>V = 16.1345 * (Sf**0.5)<br><br>Paved Surface:<br>V = 20.3282 * (Sf**0.5)<br><br>(Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec<br>Sf= Slope, ft/ft<br>Tc= Time of concentration, hours<br>Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours<br>n= Manning's n<br>Lf= Flow length, feet<br>P= 2yr, 24hr Rain depth, inches<br>Sf= Slope, % |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Fair condition; grass cover 50% to 75% - Soil B | 69.000 | 1.214 | 0.0 | 0.0 | 69.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.148 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.361 | (N/A) | (N/A) | 72.147 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Fair condition; grass cover 50% to 75% - Soil B | 69.000 | 1.214 | 0.0 | 0.0 | 69.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.148 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.361 | (N/A) | (N/A) | 72.147 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Fair condition; grass cover 50% to 75% - Soil B | 69.000 | 1.214 | 0.0 | 0.0 | 69.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.148 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.361 | (N/A) | (N/A) | 72.147 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Fair condition; grass cover 50% to 75% - Soil B | 69.000 | 1.214 | 0.0 | 0.0 | 69.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.148 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.361 | (N/A) | (N/A) | 72.147 |

# Pre-Development Conditions

Subsection: Runoff CN-Area
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Fair condition; grass cover 50% to 75% - Soil B | 69.000 | 1.214 | 0.0 | 0.0 | 69.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.148 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.361 | (N/A) | (N/A) | 72.147 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method (Computational Notes)

### Definition of Terms

| | |
|---|---|
| At | Total area (acres): At = Ai+Ap |
| Ai | Impervious area (acres) |
| Ap | Pervious area (acres) |
| CNi | Runoff curve number for impervious area |
| CNp | Runoff curve number for pervious area |
| fLoss | f loss constant infiltration (depth/time) |
| gKs | Saturated Hydraulic Conductivity (depth/time) |
| Md | Volumetric Moisture Deficit |
| Psi | Capillary Suction (length) |
| hK | Horton Infiltration Decay Rate (time^-1) |
| fo | Initial Infiltration Rate (depth/time) |
| fc | Ultimate(capacity)Infiltration Rate (depth/time) |
| Ia | Initial Abstraction (length) |
| dt | Computational increment (duration of unit excess rainfall)<br>Default dt is smallest value of 0.1333Tc, rtm, and th<br>(Smallest dt is then adjusted to match up with Tp) |
| UDdt | User specified override computational main time increment<br>(only used if UDdt is => .1333Tc) |
| D(t) | Point on distribution curve (fraction of P) for time step t |
| K | 2 / (1 + (Tr/Tp)): default K = 0.75: (for Tr/Tp = 1.67) |
| Ks | Hydrograph shape factor = Unit Conversions * K: = ((1hr/3600sec) * (1ft/12in) * ((5280ft)**2/sq.mi)) * K<br>Default Ks = 645.333 * 0.75 = 484 |
| Lag | Lag time from center of excess runoff (dt) to Tp: Lag = 0.6Tc |
| P | Total precipitation depth, inches |
| Pa(t) | Accumulated rainfall at time step t |
| Pi(t) | Incremental rainfall at time step t |
| qp | Peak discharge (cfs) for 1in. runoff, for 1hr, for 1 sq.mi. = (Ks * A * Q) / Tp (where Q = 1in. runoff, A=sq.mi.) |
| Qu(t) | Unit hydrograph ordinate (cfs) at time step t |
| Q(t) | Final hydrograph ordinate (cfs) at time step t |
| Rai(t) | Accumulated runoff (inches) at time step t for impervious area |
| Rap(t) | Accumulated runoff (inches) at time step t for pervious area |
| Rii(t) | Incremental runoff (inches) at time step t for impervious area |
| Rip(t) | Incremental runoff (inches) at time step t for pervious area |
| R(t) | Incremental weighted total runoff (inches) |
| Rtm | Time increment for rainfall table |
| Si | S for impervious area: Si = (1000/CNi) - 10 |
| Sp | S for pervious area: Sp = (1000/CNp) - 10 |
| t | Time step (row) number |
| Tc | Time of concentration |
| Tb | Time (hrs) of entire unit hydrograph: Tb = Tp + Tr |
| Tp | Time (hrs) to peak of a unit hydrograph: Tp = (dt/2) + Lag |
| Tr | Time (hrs) of receding limb of unit hydrograph: Tr = ratio of Tp |

# Pre-Development Conditions

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method
## Computational Notes
## Precipitation

| | |
|---|---|
| Column (1) | Time for time step t |
| Column (2) | D(t) = Point on distribution curve for time step t |
| Column (3) | Pi(t) = Pa(t) - Pa(t-1): Col.(4) - Preceding Col.(4) |
| Column (4) | Pa(t) = D(t) x P: Col.(2) x P |

## Pervious Area Runoff (using SCS Runoff CN Method)

| | |
|---|---|
| Column (5) | Rap(t) = Accumulated pervious runoff for time step t<br>If (Pa(t) is <= 0.2Sp) then use: Rap(t) = 0.0<br>If (Pa(t) is > 0.2Sp) then use:<br><br>Rap(t) = (Col.(4)-0.2Sp)**2 / (Col.(4)+0.8Sp) |
| Column (6) | Rip(t) = Incremental pervious runoff for time step t<br>Rip(t) = Rap(t) - Rap(t-1)<br>Rip(t) = Col.(5) for current row - Col.(5) for preceding row. |

## Impervious Area Runoff

| | |
|---|---|
| Column (7 & 8)... | Did not specify to use impervious areas. |

## Incremental Weighted Runoff

| | |
|---|---|
| Column (9) | R(t) = (Ap/At) x Rip(t) + (Ai/At) x Rii(t)<br>R(t) = (Ap/At) x Col.(6) + (Ai/At) x Col.(8) |

## SCS Unit Hydrograph Method

| | |
|---|---|
| Column (10) | Q(t) is computed with the SCS unit hydrograph method using R(t) and Qu(t). |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.014 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.24 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.133 hours |
| Flow (Peak Interpolated Output) | 0.23 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 1.4 in |
| Runoff Volume (Pervious) | 0.020 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.020 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |
| Computational Time Increment | 0.014 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 2 years
Label: Offsite
Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.85 $ft^3/s$ |
| Unit peak time, Tp | 0.070 hours |
| Unit receding limb, Tr | 0.278 hours |
| Total unit time, Tb | 0.348 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Offsite Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 10.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 11.133 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| 11.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 11.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 11.633 | 0.02 | 0.02 | 0.03 | 0.03 | 0.04 |
| 11.800 | 0.05 | 0.05 | 0.06 | 0.07 | 0.09 |
| 11.967 | 0.13 | 0.16 | 0.19 | 0.21 | 0.23 |
| 12.133 | 0.23 | 0.20 | 0.17 | 0.15 | 0.14 |
| 12.300 | 0.13 | 0.12 | 0.11 | 0.10 | 0.09 |
| 12.467 | 0.08 | 0.07 | 0.06 | 0.06 | 0.05 |
| 12.633 | 0.05 | 0.04 | 0.04 | 0.04 | 0.04 |
| 12.800 | 0.04 | 0.04 | 0.04 | 0.04 | 0.03 |
| 12.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.133 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.300 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.467 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 13.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 13.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 15.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Offsite Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 16.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Offsite Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 23.133 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 24.133 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.014 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.46 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.45 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.037 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.037 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |
| Computational Time Increment | 0.014 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 10 years
Label: Offsite
Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.85 $ft^3/s$ |
| Unit peak time, Tp | 0.070 hours |
| Unit receding limb, Tr | 0.278 hours |
| Total unit time, Tb | 0.348 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Offsite Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.567 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.733 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 11.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 11.567 | 0.04 | 0.04 | 0.05 | 0.06 | 0.07 |
| 11.733 | 0.08 | 0.10 | 0.11 | 0.13 | 0.15 |
| 11.900 | 0.16 | 0.20 | 0.27 | 0.34 | 0.39 |
| 12.067 | 0.42 | 0.45 | 0.45 | 0.39 | 0.32 |
| 12.233 | 0.28 | 0.26 | 0.23 | 0.22 | 0.20 |
| 12.400 | 0.18 | 0.17 | 0.14 | 0.13 | 0.11 |
| 12.567 | 0.10 | 0.09 | 0.08 | 0.08 | 0.07 |
| 12.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 12.900 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 13.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.400 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 |
| 13.567 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 13.733 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 13.900 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.067 | 0.04 | 0.04 | 0.04 | 0.03 | 0.03 |
| 14.233 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.567 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.733 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Offsite Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 14.900 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.067 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.233 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.400 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.733 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.400 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.733 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 17.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Offsite Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 21.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.067 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.014 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.58 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.57 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.3 in |
| Runoff Volume (Pervious) | 0.047 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.047 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |
| Computational Time Increment | 0.014 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 25 years
Label: Offsite
Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.85 $ft^3/s$ |
| Unit peak time, Tp | 0.070 hours |
| Unit receding limb, Tr | 0.278 hours |
| Total unit time, Tb | 0.348 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.033 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.367 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.533 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.700 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.533 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 |
| 10.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11.033 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 11.200 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 11.367 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 11.533 | 0.05 | 0.05 | 0.06 | 0.07 | 0.09 |
| 11.700 | 0.10 | 0.12 | 0.14 | 0.15 | 0.17 |
| 11.867 | 0.20 | 0.22 | 0.26 | 0.35 | 0.44 |
| 12.033 | 0.51 | 0.55 | 0.57 | 0.57 | 0.49 |
| 12.200 | 0.41 | 0.36 | 0.32 | 0.29 | 0.27 |
| 12.367 | 0.25 | 0.22 | 0.21 | 0.18 | 0.16 |
| 12.533 | 0.14 | 0.12 | 0.11 | 0.10 | 0.09 |
| 12.700 | 0.09 | 0.09 | 0.09 | 0.08 | 0.08 |
| 12.867 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 13.033 | 0.07 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.200 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.367 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 13.533 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.700 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.867 | 0.05 | 0.05 | 0.05 | 0.05 | 0.04 |
| 14.033 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.200 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 14.367 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.533 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.700 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.867 | 0.04 | 0.04 | 0.04 | 0.03 | 0.03 |
| 15.033 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.200 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.367 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.533 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.700 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.867 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 |
| 16.033 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.200 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.367 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.033 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.200 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.367 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.033 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 21.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.033 | 0.01 | 0.00 | 0.00 | 0.00 | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.014 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.73 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.73 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.2 in |
| Runoff Volume (Pervious) | 0.060 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.060 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |
| Computational Time Increment | 0.014 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 50 years
Label: Offsite
Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.85 $ft^3/s$ |
| Unit peak time, Tp | 0.070 hours |
| Unit receding limb, Tr | 0.278 hours |
| Total unit time, Tb | 0.348 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Offsite Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.133 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.133 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.633 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 10.800 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| 11.133 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 11.300 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 11.467 | 0.06 | 0.06 | 0.07 | 0.08 | 0.09 |
| 11.633 | 0.10 | 0.12 | 0.14 | 0.16 | 0.18 |
| 11.800 | 0.21 | 0.23 | 0.26 | 0.29 | 0.34 |
| 11.967 | 0.46 | 0.58 | 0.65 | 0.70 | 0.73 |
| 12.133 | 0.72 | 0.61 | 0.51 | 0.45 | 0.40 |
| 12.300 | 0.37 | 0.34 | 0.31 | 0.28 | 0.26 |
| 12.467 | 0.22 | 0.19 | 0.17 | 0.15 | 0.13 |
| 12.633 | 0.12 | 0.12 | 0.11 | 0.11 | 0.11 |
| 12.800 | 0.10 | 0.10 | 0.10 | 0.09 | 0.09 |
| 12.967 | 0.09 | 0.08 | 0.08 | 0.08 | 0.08 |
| 13.133 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 13.300 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 13.467 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 13.633 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Offsite Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.800 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.967 | 0.06 | 0.06 | 0.05 | 0.05 | 0.05 |
| 14.133 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.300 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.467 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.633 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.800 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.967 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.133 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.300 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.467 | 0.04 | 0.04 | 0.04 | 0.04 | 0.03 |
| 15.633 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.800 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.133 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.300 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.467 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.633 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.800 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Offsite Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 |
| 24.133 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.014 hours |
| Time to Peak (Computed) | 12.106 hours |
| Flow (Peak, Computed) | 0.79 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.79 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.6 in |
| Runoff Volume (Pervious) | 0.065 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.065 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.104 hours |
| Computational Time Increment | 0.014 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.85 ft³/s |
| Unit peak time, Tp | 0.070 hours |
| Unit receding limb, Tr | 0.278 hours |
| Total unit time, Tb | 0.348 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Offsite Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.104 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.267 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.433 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.933 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.933 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 10.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| 10.600 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.933 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 |
| 11.100 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 11.267 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 11.433 | 0.06 | 0.07 | 0.07 | 0.07 | 0.08 |
| 11.600 | 0.10 | 0.11 | 0.13 | 0.15 | 0.17 |
| 11.767 | 0.20 | 0.23 | 0.25 | 0.28 | 0.32 |
| 11.933 | 0.37 | 0.50 | 0.63 | 0.70 | 0.75 |
| 12.100 | 0.79 | 0.77 | 0.66 | 0.55 | 0.48 |
| 12.267 | 0.43 | 0.39 | 0.37 | 0.33 | 0.30 |
| 12.433 | 0.27 | 0.24 | 0.21 | 0.19 | 0.16 |
| 12.600 | 0.14 | 0.13 | 0.13 | 0.12 | 0.12 |
| 12.767 | 0.11 | 0.11 | 0.11 | 0.10 | 0.10 |
| 12.933 | 0.10 | 0.09 | 0.09 | 0.09 | 0.09 |
| 13.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 13.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 13.433 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Offsite Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.600 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 13.767 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.933 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 14.100 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 14.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.433 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.600 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.933 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 |
| 15.100 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.267 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.433 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.767 | 0.04 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.933 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.100 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.267 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.433 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.600 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.933 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 17.100 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Offsite Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.600 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 |
| 20.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.100 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 2.33 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 2.30 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 72.000 |
| Area (User Defined) | 1.361 acres |
| Maximum Retention (Pervious) | 3.9 in |
| Maximum Retention (Pervious, 20 percent) | 0.8 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 1.7 in |
| Runoff Volume (Pervious) | 0.190 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.190 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.42 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Pre-Developed Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.933 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.267 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 |
| 10.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| 10.600 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| 10.767 | 0.04 | 0.04 | 0.04 | 0.04 | 0.05 |
| 10.933 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 11.100 | 0.06 | 0.07 | 0.07 | 0.08 | 0.08 |
| 11.267 | 0.09 | 0.09 | 0.10 | 0.11 | 0.11 |
| 11.433 | 0.12 | 0.13 | 0.13 | 0.15 | 0.17 |
| 11.600 | 0.20 | 0.23 | 0.28 | 0.34 | 0.39 |
| 11.767 | 0.46 | 0.54 | 0.60 | 0.70 | 0.80 |
| 11.933 | 0.96 | 1.35 | 1.73 | 1.97 | 2.16 |
| 12.100 | 2.30 | 2.28 | 1.95 | 1.62 | 1.45 |
| 12.267 | 1.31 | 1.21 | 1.13 | 1.02 | 0.93 |
| 12.433 | 0.86 | 0.74 | 0.65 | 0.59 | 0.51 |
| 12.600 | 0.45 | 0.42 | 0.40 | 0.39 | 0.38 |
| 12.767 | 0.37 | 0.36 | 0.35 | 0.33 | 0.32 |
| 12.933 | 0.32 | 0.30 | 0.29 | 0.29 | 0.28 |
| 13.100 | 0.27 | 0.27 | 0.26 | 0.26 | 0.26 |
| 13.267 | 0.25 | 0.25 | 0.25 | 0.25 | 0.24 |
| 13.433 | 0.24 | 0.24 | 0.24 | 0.23 | 0.23 |
| 13.600 | 0.23 | 0.23 | 0.22 | 0.22 | 0.22 |
| 13.767 | 0.21 | 0.21 | 0.21 | 0.21 | 0.20 |
| 13.933 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |
| 14.100 | 0.19 | 0.19 | 0.19 | 0.18 | 0.18 |
| 14.267 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 14.433 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 14.600 | 0.17 | 0.17 | 0.17 | 0.16 | 0.16 |
| 14.767 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 14.933 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 15.100 | 0.15 | 0.15 | 0.14 | 0.14 | 0.14 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Pre-Developed Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 15.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 15.433 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 15.600 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 15.767 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 15.933 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 16.100 | 0.11 | 0.10 | 0.10 | 0.10 | 0.10 |
| 16.267 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 16.433 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 16.600 | 0.10 | 0.09 | 0.09 | 0.09 | 0.09 |
| 16.767 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 16.933 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 17.100 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 17.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 17.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 17.600 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 17.767 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 17.933 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 18.100 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 18.267 | 0.07 | 0.06 | 0.06 | 0.06 | 0.06 |
| 18.433 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 18.600 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 18.767 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 18.933 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.100 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.267 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.433 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.600 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.767 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.933 | 0.06 | 0.06 | 0.06 | 0.05 | 0.05 |
| 20.100 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 20.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 20.433 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 20.600 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 20.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 20.933 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.100 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.433 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.600 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.933 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.100 | 0.05 | 0.05 | 0.05 | 0.05 | 0.04 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Pre-Developed Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 22.267 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 22.433 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 22.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 22.767 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 22.933 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.100 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.267 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.433 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.767 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.933 | 0.04 | 0.04 | 0.04 | 0.03 | 0.02 |
| 24.100 | 0.01 | 0.00 | 0.00 | 0.00 | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 4.18 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 4.16 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 72.000 |
| Area (User Defined) | 1.361 acres |
| Maximum Retention (Pervious) | 3.9 in |
| Maximum Retention (Pervious, 20 percent) | 0.8 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.0 in |
| Runoff Volume (Pervious) | 0.340 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.340 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.42 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 9.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 9.300 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 9.467 | 0.03 | 0.03 | 0.03 | 0.04 | 0.04 |
| 9.633 | 0.04 | 0.04 | 0.04 | 0.04 | 0.05 |
| 9.800 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 9.967 | 0.06 | 0.06 | 0.06 | 0.06 | 0.07 |
| 10.133 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 |
| 10.300 | 0.08 | 0.09 | 0.09 | 0.09 | 0.10 |
| 10.467 | 0.10 | 0.10 | 0.11 | 0.11 | 0.11 |
| 10.633 | 0.12 | 0.12 | 0.13 | 0.13 | 0.13 |
| 10.800 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 |
| 10.967 | 0.16 | 0.16 | 0.17 | 0.18 | 0.18 |
| 11.133 | 0.19 | 0.20 | 0.21 | 0.22 | 0.24 |
| 11.300 | 0.25 | 0.26 | 0.27 | 0.29 | 0.30 |
| 11.467 | 0.31 | 0.33 | 0.35 | 0.41 | 0.47 |
| 11.633 | 0.53 | 0.65 | 0.76 | 0.86 | 1.01 |
| 11.800 | 1.14 | 1.27 | 1.45 | 1.61 | 1.91 |
| 11.967 | 2.62 | 3.29 | 3.70 | 3.97 | 4.16 |
| 12.133 | 4.08 | 3.44 | 2.85 | 2.53 | 2.26 |
| 12.300 | 2.07 | 1.94 | 1.74 | 1.58 | 1.46 |
| 12.467 | 1.26 | 1.09 | 0.99 | 0.86 | 0.76 |
| 12.633 | 0.71 | 0.67 | 0.65 | 0.63 | 0.61 |
| 12.800 | 0.59 | 0.58 | 0.56 | 0.54 | 0.53 |
| 12.967 | 0.50 | 0.49 | 0.47 | 0.46 | 0.45 |
| 13.133 | 0.44 | 0.43 | 0.43 | 0.43 | 0.42 |
| 13.300 | 0.42 | 0.41 | 0.41 | 0.40 | 0.40 |
| 13.467 | 0.39 | 0.39 | 0.38 | 0.38 | 0.37 |
| 13.633 | 0.37 | 0.37 | 0.36 | 0.36 | 0.35 |
| 13.800 | 0.35 | 0.34 | 0.34 | 0.33 | 0.33 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.967 | 0.32 | 0.32 | 0.32 | 0.31 | 0.31 |
| 14.133 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 |
| 14.300 | 0.29 | 0.29 | 0.29 | 0.29 | 0.28 |
| 14.467 | 0.28 | 0.28 | 0.28 | 0.28 | 0.27 |
| 14.633 | 0.27 | 0.27 | 0.27 | 0.26 | 0.26 |
| 14.800 | 0.26 | 0.26 | 0.25 | 0.25 | 0.25 |
| 14.967 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 15.133 | 0.24 | 0.23 | 0.23 | 0.23 | 0.23 |
| 15.300 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 15.467 | 0.21 | 0.21 | 0.21 | 0.21 | 0.20 |
| 15.633 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |
| 15.800 | 0.19 | 0.19 | 0.18 | 0.18 | 0.18 |
| 15.967 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 16.133 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |
| 16.300 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 16.467 | 0.16 | 0.16 | 0.15 | 0.15 | 0.15 |
| 16.633 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 16.800 | 0.15 | 0.15 | 0.14 | 0.14 | 0.14 |
| 16.967 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 17.133 | 0.14 | 0.13 | 0.13 | 0.13 | 0.13 |
| 17.300 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 17.467 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 17.633 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 17.800 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 17.967 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 18.133 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 18.300 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 18.467 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 18.633 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 18.800 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 18.967 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 19.133 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 19.300 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 19.467 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 19.633 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 19.800 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 19.967 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 20.133 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 20.300 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.467 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.633 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.800 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.967 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.133 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.300 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.467 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.633 | 0.08 | 0.07 | 0.07 | 0.07 | 0.07 |
| 21.800 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 21.967 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.133 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.300 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.467 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.633 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.800 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.967 | 0.07 | 0.07 | 0.07 | 0.06 | 0.06 |
| 23.133 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 23.300 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 23.467 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 23.633 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 23.800 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 23.967 | 0.06 | 0.06 | 0.05 | 0.03 | 0.01 |
| 24.133 | 0.01 | 0.00 | 0.00 | 0.00 | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 5.22 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 5.19 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 72.000 |
| Area (User Defined) | 1.361 acres |
| Maximum Retention (Pervious) | 3.9 in |
| Maximum Retention (Pervious, 20 percent) | 0.8 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.7 in |
| Runoff Volume (Pervious) | 0.425 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.425 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 25 years
Label: Pre-Developed
Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.42 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.733 | 0.02 | 0.02 | 0.03 | 0.03 | 0.03 |
| 8.900 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| 9.067 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 9.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 9.400 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 9.567 | 0.07 | 0.07 | 0.07 | 0.07 | 0.08 |
| 9.733 | 0.08 | 0.08 | 0.08 | 0.09 | 0.09 |
| 9.900 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 |
| 10.067 | 0.10 | 0.11 | 0.11 | 0.11 | 0.12 |
| 10.233 | 0.12 | 0.13 | 0.13 | 0.13 | 0.14 |
| 10.400 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 |
| 10.567 | 0.16 | 0.17 | 0.17 | 0.18 | 0.18 |
| 10.733 | 0.19 | 0.19 | 0.20 | 0.20 | 0.21 |
| 10.900 | 0.21 | 0.22 | 0.23 | 0.23 | 0.24 |
| 11.067 | 0.25 | 0.26 | 0.27 | 0.28 | 0.30 |
| 11.233 | 0.31 | 0.33 | 0.34 | 0.36 | 0.37 |
| 11.400 | 0.39 | 0.41 | 0.43 | 0.45 | 0.48 |
| 11.567 | 0.56 | 0.63 | 0.71 | 0.87 | 1.01 |
| 11.733 | 1.14 | 1.33 | 1.50 | 1.65 | 1.88 |
| 11.900 | 2.09 | 2.46 | 3.35 | 4.18 | 4.67 |
| 12.067 | 4.98 | 5.19 | 5.07 | 4.27 | 3.52 |
| 12.233 | 3.12 | 2.78 | 2.55 | 2.38 | 2.14 |
| 12.400 | 1.94 | 1.78 | 1.54 | 1.33 | 1.20 |
| 12.567 | 1.05 | 0.93 | 0.86 | 0.82 | 0.79 |
| 12.733 | 0.77 | 0.74 | 0.72 | 0.70 | 0.68 |
| 12.900 | 0.65 | 0.64 | 0.61 | 0.59 | 0.58 |
| 13.067 | 0.56 | 0.54 | 0.53 | 0.53 | 0.52 |
| 13.233 | 0.52 | 0.51 | 0.50 | 0.50 | 0.49 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.400 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 13.567 | 0.46 | 0.45 | 0.45 | 0.44 | 0.44 |
| 13.733 | 0.43 | 0.43 | 0.42 | 0.42 | 0.41 |
| 13.900 | 0.40 | 0.40 | 0.39 | 0.38 | 0.38 |
| 14.067 | 0.38 | 0.37 | 0.37 | 0.36 | 0.36 |
| 14.233 | 0.36 | 0.36 | 0.35 | 0.35 | 0.35 |
| 14.400 | 0.35 | 0.34 | 0.34 | 0.34 | 0.33 |
| 14.567 | 0.33 | 0.33 | 0.33 | 0.32 | 0.32 |
| 14.733 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 14.900 | 0.30 | 0.30 | 0.30 | 0.30 | 0.29 |
| 15.067 | 0.29 | 0.29 | 0.28 | 0.28 | 0.28 |
| 15.233 | 0.28 | 0.27 | 0.27 | 0.27 | 0.26 |
| 15.400 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 15.567 | 0.25 | 0.24 | 0.24 | 0.24 | 0.24 |
| 15.733 | 0.23 | 0.23 | 0.23 | 0.22 | 0.22 |
| 15.900 | 0.22 | 0.22 | 0.21 | 0.21 | 0.21 |
| 16.067 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 16.233 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 16.400 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 16.567 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 16.733 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 16.900 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 17.067 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 17.233 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 17.400 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 17.567 | 0.15 | 0.14 | 0.14 | 0.14 | 0.14 |
| 17.733 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 17.900 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.067 | 0.13 | 0.13 | 0.13 | 0.13 | 0.12 |
| 18.233 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.400 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.567 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.733 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.067 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.233 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.567 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.900 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 20.067 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.233 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Pre-Developed Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.400 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.567 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.733 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.900 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.067 | 0.10 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.233 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.400 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.567 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.733 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.900 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.067 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.233 | 0.08 | 0.08 | 0.08 | 0.07 | 0.07 |
| 23.400 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.567 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.900 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 24.067 | 0.04 | 0.02 | 0.01 | 0.00 | 0.00 |
| 24.233 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 6.52 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 6.49 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 72.000 |
| Area (User Defined) | 1.361 acres |
| Maximum Retention (Pervious) | 3.9 in |
| Maximum Retention (Pervious, 20 percent) | 0.8 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.7 in |
| Runoff Volume (Pervious) | 0.533 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.533 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 50 years
Label: Pre-Developed
Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.42 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.567 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.900 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 8.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.233 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.400 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 |
| 8.567 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 8.733 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 8.900 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 |
| 9.067 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 |
| 9.233 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 |
| 9.400 | 0.10 | 0.10 | 0.10 | 0.10 | 0.11 |
| 9.567 | 0.11 | 0.11 | 0.11 | 0.12 | 0.12 |
| 9.733 | 0.12 | 0.13 | 0.13 | 0.13 | 0.14 |
| 9.900 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 |
| 10.067 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 |
| 10.233 | 0.18 | 0.19 | 0.19 | 0.20 | 0.20 |
| 10.400 | 0.21 | 0.21 | 0.22 | 0.22 | 0.23 |
| 10.567 | 0.24 | 0.24 | 0.25 | 0.25 | 0.26 |
| 10.733 | 0.27 | 0.27 | 0.28 | 0.29 | 0.29 |
| 10.900 | 0.30 | 0.31 | 0.31 | 0.32 | 0.33 |
| 11.067 | 0.34 | 0.35 | 0.37 | 0.39 | 0.41 |
| 11.233 | 0.42 | 0.45 | 0.47 | 0.48 | 0.51 |
| 11.400 | 0.53 | 0.55 | 0.57 | 0.60 | 0.64 |
| 11.567 | 0.74 | 0.84 | 0.94 | 1.15 | 1.33 |
| 11.733 | 1.49 | 1.74 | 1.96 | 2.15 | 2.43 |
| 11.900 | 2.69 | 3.15 | 4.26 | 5.30 | 5.89 |
| 12.067 | 6.25 | 6.49 | 6.31 | 5.30 | 4.36 |
| 12.233 | 3.85 | 3.42 | 3.13 | 2.92 | 2.62 |
| 12.400 | 2.38 | 2.18 | 1.88 | 1.63 | 1.47 |
| 12.567 | 1.28 | 1.13 | 1.05 | 1.00 | 0.96 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.733 | 0.94 | 0.90 | 0.88 | 0.86 | 0.82 |
| 12.900 | 0.80 | 0.78 | 0.74 | 0.72 | 0.70 |
| 13.067 | 0.68 | 0.66 | 0.65 | 0.64 | 0.63 |
| 13.233 | 0.63 | 0.62 | 0.61 | 0.61 | 0.60 |
| 13.400 | 0.59 | 0.59 | 0.58 | 0.57 | 0.57 |
| 13.567 | 0.56 | 0.55 | 0.54 | 0.54 | 0.53 |
| 13.733 | 0.52 | 0.52 | 0.51 | 0.50 | 0.49 |
| 13.900 | 0.49 | 0.48 | 0.47 | 0.47 | 0.46 |
| 14.067 | 0.45 | 0.45 | 0.45 | 0.44 | 0.44 |
| 14.233 | 0.44 | 0.43 | 0.43 | 0.42 | 0.42 |
| 14.400 | 0.42 | 0.42 | 0.41 | 0.41 | 0.40 |
| 14.567 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 |
| 14.733 | 0.38 | 0.38 | 0.38 | 0.37 | 0.37 |
| 14.900 | 0.37 | 0.36 | 0.36 | 0.36 | 0.35 |
| 15.067 | 0.35 | 0.35 | 0.34 | 0.34 | 0.34 |
| 15.233 | 0.33 | 0.33 | 0.33 | 0.32 | 0.32 |
| 15.400 | 0.32 | 0.31 | 0.31 | 0.30 | 0.30 |
| 15.567 | 0.30 | 0.29 | 0.29 | 0.29 | 0.28 |
| 15.733 | 0.28 | 0.28 | 0.27 | 0.27 | 0.27 |
| 15.900 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 16.067 | 0.25 | 0.24 | 0.24 | 0.24 | 0.24 |
| 16.233 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 16.400 | 0.23 | 0.23 | 0.23 | 0.23 | 0.22 |
| 16.567 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.733 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 16.900 | 0.21 | 0.21 | 0.20 | 0.20 | 0.20 |
| 17.067 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |
| 17.233 | 0.19 | 0.19 | 0.19 | 0.19 | 0.18 |
| 17.400 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 17.567 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 17.733 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |
| 17.900 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 18.067 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.233 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.400 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.567 | 0.15 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.733 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.900 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.067 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.233 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 19.400 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 19.567 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.733 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 19.900 | 0.13 | 0.13 | 0.13 | 0.13 | 0.12 |
| 20.067 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.233 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.400 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.567 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.733 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.900 | 0.12 | 0.12 | 0.11 | 0.11 | 0.11 |
| 21.067 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.233 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.567 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.900 | 0.11 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.067 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.233 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.400 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.567 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.733 | 0.10 | 0.10 | 0.10 | 0.10 | 0.09 |
| 22.900 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.067 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.233 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.400 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.567 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.733 | 0.09 | 0.09 | 0.09 | 0.08 | 0.08 |
| 23.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 24.067 | 0.05 | 0.02 | 0.01 | 0.00 | 0.00 |
| 24.233 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 6.99 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 6.96 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 72.000 |
| Area (User Defined) | 1.361 acres |
| Maximum Retention (Pervious) | 3.9 in |
| Maximum Retention (Pervious, 20 percent) | 0.8 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 5.0 in |
| Runoff Volume (Pervious) | 0.573 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.573 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Pre-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Pre-Developed
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.42 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.361 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.367 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.700 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 7.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.033 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.200 | 0.03 | 0.03 | 0.03 | 0.04 | 0.04 |
| 8.367 | 0.04 | 0.04 | 0.04 | 0.04 | 0.05 |
| 8.533 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 8.700 | 0.06 | 0.06 | 0.06 | 0.06 | 0.07 |
| 8.867 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 |
| 9.033 | 0.08 | 0.08 | 0.09 | 0.09 | 0.09 |
| 9.200 | 0.09 | 0.10 | 0.10 | 0.10 | 0.10 |
| 9.367 | 0.11 | 0.11 | 0.11 | 0.12 | 0.12 |
| 9.533 | 0.12 | 0.13 | 0.13 | 0.13 | 0.14 |
| 9.700 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 |
| 9.867 | 0.16 | 0.16 | 0.16 | 0.17 | 0.17 |
| 10.033 | 0.17 | 0.18 | 0.18 | 0.19 | 0.19 |
| 10.200 | 0.20 | 0.20 | 0.21 | 0.21 | 0.22 |
| 10.367 | 0.23 | 0.23 | 0.24 | 0.24 | 0.25 |
| 10.533 | 0.26 | 0.26 | 0.27 | 0.28 | 0.28 |
| 10.700 | 0.29 | 0.30 | 0.30 | 0.31 | 0.32 |
| 10.867 | 0.33 | 0.33 | 0.34 | 0.35 | 0.36 |
| 11.033 | 0.36 | 0.38 | 0.39 | 0.41 | 0.43 |
| 11.200 | 0.45 | 0.47 | 0.49 | 0.51 | 0.53 |
| 11.367 | 0.56 | 0.58 | 0.60 | 0.63 | 0.66 |
| 11.533 | 0.70 | 0.81 | 0.91 | 1.03 | 1.25 |
| 11.700 | 1.45 | 1.63 | 1.89 | 2.13 | 2.33 |
| 11.867 | 2.63 | 2.91 | 3.41 | 4.60 | 5.71 |
| 12.033 | 6.34 | 6.72 | 6.96 | 6.76 | 5.68 |
| 12.200 | 4.67 | 4.12 | 3.66 | 3.34 | 3.12 |
| 12.367 | 2.80 | 2.54 | 2.33 | 2.01 | 1.74 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.533 | 1.57 | 1.36 | 1.21 | 1.12 | 1.06 |
| 12.700 | 1.02 | 1.00 | 0.96 | 0.93 | 0.91 |
| 12.867 | 0.88 | 0.85 | 0.83 | 0.79 | 0.76 |
| 13.033 | 0.75 | 0.72 | 0.70 | 0.69 | 0.68 |
| 13.200 | 0.67 | 0.67 | 0.66 | 0.65 | 0.64 |
| 13.367 | 0.64 | 0.63 | 0.62 | 0.61 | 0.61 |
| 13.533 | 0.60 | 0.59 | 0.59 | 0.58 | 0.57 |
| 13.700 | 0.56 | 0.56 | 0.55 | 0.54 | 0.53 |
| 13.867 | 0.53 | 0.52 | 0.51 | 0.50 | 0.50 |
| 14.033 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 14.200 | 0.47 | 0.46 | 0.46 | 0.45 | 0.45 |
| 14.367 | 0.45 | 0.44 | 0.44 | 0.44 | 0.43 |
| 14.533 | 0.43 | 0.43 | 0.42 | 0.42 | 0.42 |
| 14.700 | 0.41 | 0.41 | 0.40 | 0.40 | 0.40 |
| 14.867 | 0.39 | 0.39 | 0.39 | 0.38 | 0.38 |
| 15.033 | 0.38 | 0.37 | 0.37 | 0.37 | 0.36 |
| 15.200 | 0.36 | 0.35 | 0.35 | 0.35 | 0.34 |
| 15.367 | 0.34 | 0.34 | 0.33 | 0.33 | 0.32 |
| 15.533 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 15.700 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 15.867 | 0.28 | 0.28 | 0.28 | 0.27 | 0.27 |
| 16.033 | 0.27 | 0.26 | 0.26 | 0.26 | 0.25 |
| 16.200 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| 16.367 | 0.25 | 0.24 | 0.24 | 0.24 | 0.24 |
| 16.533 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 16.700 | 0.23 | 0.23 | 0.23 | 0.22 | 0.22 |
| 16.867 | 0.22 | 0.22 | 0.22 | 0.22 | 0.21 |
| 17.033 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 17.200 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 17.367 | 0.20 | 0.19 | 0.19 | 0.19 | 0.19 |
| 17.533 | 0.19 | 0.19 | 0.18 | 0.18 | 0.18 |
| 17.700 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 17.867 | 0.17 | 0.17 | 0.17 | 0.17 | 0.16 |
| 18.033 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.200 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.367 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 18.533 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.700 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.867 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.033 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.200 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.367 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |

# Pre-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Pre-Developed Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.533 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.700 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.867 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.033 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.200 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.367 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.533 | 0.13 | 0.13 | 0.13 | 0.13 | 0.12 |
| 20.700 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.867 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.033 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.200 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.367 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.533 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.700 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.867 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.033 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.200 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.367 | 0.11 | 0.11 | 0.11 | 0.11 | 0.10 |
| 22.533 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.700 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.867 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.033 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.200 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.367 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.533 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.700 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.867 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 24.033 | 0.08 | 0.05 | 0.02 | 0.01 | 0.00 |
| 24.200 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

# Pre-Development Conditions

Subsection: Addition Summary
Label: Point of Interest
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Summary for Hydrograph Addition at 'Point of Interest'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Pre-Developed |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.020 | 12.133 | 0.23 |
| Flow (From) | Pre-Developed | 0.190 | 12.100 | 2.30 |
| Flow (In) | Point of Interest | 0.210 | 12.100 | 2.53 |

# Pre-Development Conditions

Subsection: Addition Summary
Label: Point of Interest
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Summary for Hydrograph Addition at 'Point of Interest'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Pre-Developed |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.037 | 12.100 | 0.45 |
| Flow (From) | Pre-Developed | 0.340 | 12.100 | 4.16 |
| Flow (In) | Point of Interest | 0.377 | 12.100 | 4.61 |

# Pre-Development Conditions

Subsection: Addition Summary
Label: Point of Interest
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Summary for Hydrograph Addition at 'Point of Interest'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Pre-Developed |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.047 | 12.100 | 0.57 |
| Flow (From) | Pre-Developed | 0.425 | 12.100 | 5.19 |
| Flow (In) | Point of Interest | 0.472 | 12.100 | 5.77 |

# Pre-Development Conditions

Subsection: Addition Summary
Label: Point of Interest
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Summary for Hydrograph Addition at 'Point of Interest'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Pre-Developed |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.060 | 12.100 | 0.73 |
| Flow (From) | Pre-Developed | 0.533 | 12.100 | 6.49 |
| Flow (In) | Point of Interest | 0.593 | 12.100 | 7.22 |

# Pre-Development Conditions

Subsection: Addition Summary
Label: Point of Interest
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Summary for Hydrograph Addition at 'Point of Interest'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Pre-Developed |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.065 | 12.100 | 0.79 |
| Flow (From) | Pre-Developed | 0.573 | 12.100 | 6.96 |
| Flow (In) | Point of Interest | 0.637 | 12.100 | 7.75 |

# Pre-Development Conditions

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# RUNOFF & STORAGE CALCULATIONS
# POST-DEVELOPED CONDITIONS

# Post-Development Conditions

| Project Summary | |
|---|---|
| Title | Good Day Farm - Bryant |
| Engineer | Ty Gramling |
| Company | Stock & Associates |
| Date | 6/25/2025 |

| Notes | Post-Development Conditions |
|---|---|

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## User Notifications

| | |
|---|---|
| Message Id | 20 |
| Scenario | Bryant, AR - Synthetic Curve, 100 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Relaxed headwater convergence for conditions below. Headwater Elevation= 403.59 ft. Tailwater elevation= Free Outfall. Flow= 7.96 ft³/s. HW +/- Convergence 0.02 ft TW +/- Convergence 0.13 ft |
| Source | Warning |
| Message Id | 19 |
| Scenario | Bryant, AR - Synthetic Curve, 100 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Charged riser flow adjusted to weir flow rate to maintain convergence. If adjustments are desired, substitute a user defined outlet rating table for level pool routing. Or, store rating curve(s) in E-Q-TW table, edit, then route with ICPM option. |
| Source | Warning |
| Message Id | 7 |
| Scenario | Bryant, AR - Synthetic Curve, 2 yrs |
| Element Type | Catchment |
| Element Id | 79 |
| Label | Offsite |
| Time | (N/A) |
| Message | The difference between calculated peak flow and interpolated peak flow 1.6 % is greater than 1.5 %. Computed peak flow= 0.24 ft³/s Interp. peak flow= 0.24 ft³/s. Output increment for this catchment may be too large. |
| Source | Warning |
| Message Id | 20 |
| Scenario | Bryant, AR - Synthetic Curve, 2 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Relaxed headwater convergence for conditions below. Headwater Elevation= 403.59 ft. Tailwater elevation= Free Outfall. Flow= 7.96 ft³/s. HW +/- Convergence 0.02 ft TW +/- Convergence 0.13 ft |
| Source | Warning |

## User Notifications

| | |
|---|---|
| Message Id | 19 |
| Scenario | Bryant, AR - Synthetic Curve, 2 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Charged riser flow adjusted to weir flow rate to maintain convergence. If adjustments are desired, substitute a user defined outlet rating table for level pool routing. Or, store rating curve(s) in E-Q-TW table, edit, then route with ICPM option. |
| Source | Warning |
| Message Id | 20 |
| Scenario | Bryant, AR - Synthetic Curve, 10 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Relaxed headwater convergence for conditions below. Headwater Elevation= 403.59 ft. Tailwater elevation= Free Outfall. Flow= 7.96 ft³/s. HW +/- Convergence 0.02 ft TW +/- Convergence 0.13 ft |
| Source | Warning |
| Message Id | 19 |
| Scenario | Bryant, AR - Synthetic Curve, 10 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Charged riser flow adjusted to weir flow rate to maintain convergence. If adjustments are desired, substitute a user defined outlet rating table for level pool routing. Or, store rating curve(s) in E-Q-TW table, edit, then route with ICPM option. |
| Source | Warning |
| Message Id | 20 |
| Scenario | Bryant, AR - Synthetic Curve, 25 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Relaxed headwater convergence for conditions below. Headwater Elevation= 403.59 ft. Tailwater elevation= Free Outfall. Flow= 7.96 ft³/s. HW +/- Convergence 0.02 ft TW +/- Convergence 0.13 ft |
| Source | Warning |

## User Notifications

| | |
|---|---|
| Message Id | 19 |
| Scenario | Bryant, AR - Synthetic Curve, 25 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Charged riser flow adjusted to weir flow rate to maintain convergence. If adjustments are desired, substitute a user defined outlet rating table for level pool routing. Or, store rating curve(s) in E-Q-TW table, edit, then route with ICPM option. |
| Source | Warning |
| Message Id | 20 |
| Scenario | Bryant, AR - Synthetic Curve, 50 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Relaxed headwater convergence for conditions below. Headwater Elevation= 403.59 ft. Tailwater elevation= Free Outfall. Flow= 7.96 ft³/s. HW +/- Convergence 0.02 ft TW +/- Convergence 0.13 ft |
| Source | Warning |
| Message Id | 19 |
| Scenario | Bryant, AR - Synthetic Curve, 50 yrs |
| Element Type | Composite Outlet Structure |
| Element Id | 42 |
| Label | Outfall Structure |
| Time | (N/A) |
| Message | Charged riser flow adjusted to weir flow rate to maintain convergence. If adjustments are desired, substitute a user defined outlet rating table for level pool routing. Or, store rating curve(s) in E-Q-TW table, edit, then route with ICPM option. |
| Source | Warning |

# Post-Development Conditions

Subsection: Master Network Summary

## Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| Site | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.241 | 12.100 | 2.95 |
| Site | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.409 | 12.100 | 4.98 |
| Site | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.502 | 12.100 | 6.09 |
| Site | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.620 | 12.100 | 7.46 |
| Site | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.663 | 12.100 | 7.96 |
| Offsite | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.020 | 12.133 | 0.24 |
| Offsite | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.037 | 12.100 | 0.45 |
| Offsite | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.047 | 12.100 | 0.58 |
| Offsite | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.060 | 12.100 | 0.73 |
| Offsite | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.065 | 12.100 | 0.79 |

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| POI | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.261 | 12.267 | 1.81 |
| POI | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.446 | 12.200 | 3.73 |
| POI | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.550 | 12.167 | 5.83 |

# Post-Development Conditions

Subsection: Master Network Summary

## Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) |
|---|---|---|---|---|---|
| POI | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.680 | 12.167 | 6.44 |
| POI | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.728 | 12.167 | 6.92 |

## Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (hours) | Peak Flow ($ft^3/s$) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ac-ft) |
|---|---|---|---|---|---|---|---|
| Detention Pond (IN) | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.261 | 12.100 | 3.18 | (N/A) | (N/A) |
| Detention Pond (OUT) | Bryant, AR - Synthetic Curve, 2 yrs | 2 | 0.261 | 12.267 | 1.81 | 406.46 | 0.044 |
| Detention Pond (IN) | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.446 | 12.100 | 5.43 | (N/A) | (N/A) |
| Detention Pond (OUT) | Bryant, AR - Synthetic Curve, 10 yrs | 10 | 0.446 | 12.200 | 3.73 | 407.31 | 0.080 |
| Detention Pond (IN) | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.550 | 12.100 | 6.67 | (N/A) | (N/A) |
| Detention Pond (OUT) | Bryant, AR - Synthetic Curve, 25 yrs | 25 | 0.550 | 12.167 | 5.83 | 407.44 | 0.086 |
| Detention Pond (IN) | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.680 | 12.100 | 8.19 | (N/A) | (N/A) |
| Detention Pond (OUT) | Bryant, AR - Synthetic Curve, 50 yrs | 50 | 0.680 | 12.167 | 6.44 | 407.72 | 0.101 |
| Detention Pond (IN) | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.728 | 12.100 | 8.75 | (N/A) | (N/A) |
| Detention Pond (OUT) | Bryant, AR - Synthetic Curve, 100 yrs | 100 | 0.728 | 12.167 | 6.92 | 407.82 | 0.106 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Time-Depth Curve: TypeIII 24hr (4.3 in) | |
|---|---|
| Label | TypeIII 24hr (4.3 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 2 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.000 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 3.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 5.000 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 6.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 6.500 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 7.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 7.500 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 |
| 8.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 8.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 9.000 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 |
| 9.500 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 |
| 10.000 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 |
| 10.500 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 |
| 11.000 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 |
| 11.500 | 1.3 | 1.4 | 1.5 | 1.6 | 1.8 |
| 12.000 | 2.1 | 2.5 | 2.7 | 2.8 | 2.9 |
| 12.500 | 3.0 | 3.1 | 3.1 | 3.2 | 3.2 |
| 13.000 | 3.2 | 3.3 | 3.3 | 3.3 | 3.3 |
| 13.500 | 3.4 | 3.4 | 3.4 | 3.4 | 3.5 |
| 14.000 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 |
| 14.500 | 3.6 | 3.6 | 3.6 | 3.6 | 3.7 |
| 15.000 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| 15.500 | 3.7 | 3.8 | 3.8 | 3.8 | 3.8 |
| 16.000 | 3.8 | 3.8 | 3.8 | 3.8 | 3.9 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 3.9 | 3.9 | 3.9 | 3.9 | 3.9 |
| 17.000 | 3.9 | 3.9 | 3.9 | 3.9 | 3.9 |
| 17.500 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 18.000 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 18.500 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 19.000 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 19.500 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 20.000 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 20.500 | 4.1 | 4.1 | 4.2 | 4.2 | 4.2 |
| 21.000 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 21.500 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 22.000 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 |
| 22.500 | 4.2 | 4.2 | 4.2 | 4.3 | 4.3 |
| 23.000 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |
| 23.500 | 4.3 | 4.3 | 4.3 | 4.3 | 4.3 |
| 24.000 | 4.3 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Time-Depth Curve: TypeIII 24hr (6.0 in) | |
|---|---|
| Label | TypeIII 24hr (6.0 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 10 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 |
| 4.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.000 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 |
| 5.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 6.000 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 |
| 6.500 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 7.000 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 |
| 7.500 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 |
| 8.000 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 |
| 8.500 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 |
| 9.000 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 |
| 9.500 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 |
| 10.000 | 1.1 | 1.2 | 1.2 | 1.2 | 1.3 |
| 10.500 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |
| 11.000 | 1.5 | 1.5 | 1.6 | 1.7 | 1.7 |
| 11.500 | 1.8 | 1.9 | 2.0 | 2.2 | 2.5 |
| 12.000 | 3.0 | 3.5 | 3.8 | 4.0 | 4.1 |
| 12.500 | 4.2 | 4.3 | 4.3 | 4.4 | 4.5 |
| 13.000 | 4.5 | 4.5 | 4.6 | 4.6 | 4.7 |
| 13.500 | 4.7 | 4.7 | 4.8 | 4.8 | 4.8 |
| 14.000 | 4.9 | 4.9 | 4.9 | 5.0 | 5.0 |
| 14.500 | 5.0 | 5.0 | 5.1 | 5.1 | 5.1 |
| 15.000 | 5.1 | 5.1 | 5.2 | 5.2 | 5.2 |
| 15.500 | 5.2 | 5.2 | 5.3 | 5.3 | 5.3 |
| 16.000 | 5.3 | 5.3 | 5.3 | 5.4 | 5.4 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 |
| 17.000 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 17.500 | 5.5 | 5.5 | 5.5 | 5.5 | 5.6 |
| 18.000 | 5.6 | 5.6 | 5.6 | 5.6 | 5.6 |
| 18.500 | 5.6 | 5.6 | 5.6 | 5.6 | 5.7 |
| 19.000 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| 19.500 | 5.7 | 5.7 | 5.7 | 5.7 | 5.7 |
| 20.000 | 5.7 | 5.7 | 5.8 | 5.8 | 5.8 |
| 20.500 | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |
| 21.000 | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |
| 21.500 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 22.000 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 22.500 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 23.000 | 5.9 | 6.0 | 6.0 | 6.0 | 6.0 |
| 23.500 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 24.000 | 6.0 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Time-Depth Curve: TypeIII 24hr (6.9 in) | |
|---|---|
| Label | TypeIII 24hr (6.9 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 25 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.500 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.500 | 0.4 | 0.5 | 0.5 | 0.5 | 0.5 |
| 6.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 6.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 7.000 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 |
| 7.500 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 |
| 8.000 | 0.8 | 0.8 | 0.8 | 0.8 | 0.9 |
| 8.500 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 |
| 9.000 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 |
| 9.500 | 1.1 | 1.2 | 1.2 | 1.2 | 1.3 |
| 10.000 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |
| 10.500 | 1.5 | 1.5 | 1.6 | 1.6 | 1.7 |
| 11.000 | 1.7 | 1.8 | 1.8 | 1.9 | 2.0 |
| 11.500 | 2.1 | 2.2 | 2.3 | 2.6 | 2.9 |
| 12.000 | 3.4 | 4.0 | 4.3 | 4.6 | 4.7 |
| 12.500 | 4.8 | 4.9 | 5.0 | 5.1 | 5.1 |
| 13.000 | 5.2 | 5.2 | 5.3 | 5.3 | 5.4 |
| 13.500 | 5.4 | 5.4 | 5.5 | 5.5 | 5.6 |
| 14.000 | 5.6 | 5.6 | 5.7 | 5.7 | 5.7 |
| 14.500 | 5.8 | 5.8 | 5.8 | 5.8 | 5.9 |
| 15.000 | 5.9 | 5.9 | 5.9 | 6.0 | 6.0 |
| 15.500 | 6.0 | 6.0 | 6.1 | 6.1 | 6.1 |
| 16.000 | 6.1 | 6.1 | 6.1 | 6.2 | 6.2 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 6.2 | 6.2 | 6.2 | 6.2 | 6.3 |
| 17.000 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |
| 17.500 | 6.3 | 6.4 | 6.4 | 6.4 | 6.4 |
| 18.000 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |
| 18.500 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 19.000 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 19.500 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| 20.000 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| 20.500 | 6.6 | 6.7 | 6.7 | 6.7 | 6.7 |
| 21.000 | 6.7 | 6.7 | 6.7 | 6.7 | 6.7 |
| 21.500 | 6.7 | 6.7 | 6.7 | 6.8 | 6.8 |
| 22.000 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 |
| 22.500 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 |
| 23.000 | 6.8 | 6.8 | 6.9 | 6.9 | 6.9 |
| 23.500 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| 24.000 | 6.9 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Time-Depth Curve: TypeIII 24hr (8.0 in) | |
|---|---|
| Label | TypeIII 24hr (8.0 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 50 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 2.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.000 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 5.500 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 |
| 6.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 6.500 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 |
| 7.000 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 |
| 7.500 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 |
| 8.000 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 |
| 8.500 | 1.0 | 1.1 | 1.1 | 1.1 | 1.1 |
| 9.000 | 1.2 | 1.2 | 1.2 | 1.3 | 1.3 |
| 9.500 | 1.3 | 1.4 | 1.4 | 1.4 | 1.5 |
| 10.000 | 1.5 | 1.6 | 1.6 | 1.6 | 1.7 |
| 10.500 | 1.7 | 1.8 | 1.8 | 1.9 | 1.9 |
| 11.000 | 2.0 | 2.1 | 2.1 | 2.2 | 2.3 |
| 11.500 | 2.4 | 2.5 | 2.7 | 3.0 | 3.3 |
| 12.000 | 4.0 | 4.7 | 5.0 | 5.3 | 5.5 |
| 12.500 | 5.6 | 5.7 | 5.8 | 5.9 | 5.9 |
| 13.000 | 6.0 | 6.1 | 6.1 | 6.2 | 6.2 |
| 13.500 | 6.3 | 6.3 | 6.4 | 6.4 | 6.4 |
| 14.000 | 6.5 | 6.5 | 6.6 | 6.6 | 6.6 |
| 14.500 | 6.7 | 6.7 | 6.7 | 6.8 | 6.8 |
| 15.000 | 6.8 | 6.9 | 6.9 | 6.9 | 6.9 |
| 15.500 | 7.0 | 7.0 | 7.0 | 7.0 | 7.1 |
| 16.000 | 7.1 | 7.1 | 7.1 | 7.1 | 7.2 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 7.2 | 7.2 | 7.2 | 7.2 | 7.3 |
| 17.000 | 7.3 | 7.3 | 7.3 | 7.3 | 7.3 |
| 17.500 | 7.4 | 7.4 | 7.4 | 7.4 | 7.4 |
| 18.000 | 7.4 | 7.4 | 7.4 | 7.5 | 7.5 |
| 18.500 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 |
| 19.000 | 7.5 | 7.6 | 7.6 | 7.6 | 7.6 |
| 19.500 | 7.6 | 7.6 | 7.6 | 7.6 | 7.6 |
| 20.000 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| 20.500 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| 21.000 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 21.500 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 22.000 | 7.8 | 7.9 | 7.9 | 7.9 | 7.9 |
| 22.500 | 7.9 | 7.9 | 7.9 | 7.9 | 7.9 |
| 23.000 | 7.9 | 7.9 | 7.9 | 8.0 | 8.0 |
| 23.500 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| 24.000 | 8.0 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Time-Depth Curve: TypeIII 24hr (8.4 in) | |
|---|---|
| Label | TypeIII 24hr (8.4 in) |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 100 years |

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| 2.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 3.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 |
| 4.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.500 | 0.4 | 0.4 | 0.4 | 0.5 | 0.5 |
| 5.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 5.500 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 |
| 6.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 |
| 6.500 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |
| 7.000 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| 7.500 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| 8.000 | 1.0 | 1.0 | 1.0 | 1.0 | 1.1 |
| 8.500 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 |
| 9.000 | 1.2 | 1.3 | 1.3 | 1.3 | 1.4 |
| 9.500 | 1.4 | 1.4 | 1.5 | 1.5 | 1.5 |
| 10.000 | 1.6 | 1.6 | 1.7 | 1.7 | 1.8 |
| 10.500 | 1.8 | 1.9 | 1.9 | 2.0 | 2.0 |
| 11.000 | 2.1 | 2.2 | 2.2 | 2.3 | 2.4 |
| 11.500 | 2.5 | 2.6 | 2.9 | 3.1 | 3.5 |
| 12.000 | 4.2 | 4.9 | 5.3 | 5.5 | 5.8 |
| 12.500 | 5.9 | 6.0 | 6.1 | 6.2 | 6.2 |
| 13.000 | 6.3 | 6.4 | 6.4 | 6.5 | 6.5 |
| 13.500 | 6.6 | 6.6 | 6.7 | 6.7 | 6.8 |
| 14.000 | 6.8 | 6.9 | 6.9 | 6.9 | 7.0 |
| 14.500 | 7.0 | 7.0 | 7.1 | 7.1 | 7.1 |
| 15.000 | 7.2 | 7.2 | 7.2 | 7.3 | 7.3 |
| 15.500 | 7.3 | 7.3 | 7.4 | 7.4 | 7.4 |
| 16.000 | 7.4 | 7.5 | 7.5 | 7.5 | 7.5 |

# Post-Development Conditions

Subsection: Time-Depth Curve
Label: Bryant Arkansas
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**CUMULATIVE RAINFALL (in)**
**Output Time Increment = 0.100 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|---|---|---|---|---|---|
| 16.500 | 7.5 | 7.6 | 7.6 | 7.6 | 7.6 |
| 17.000 | 7.6 | 7.7 | 7.7 | 7.7 | 7.7 |
| 17.500 | 7.7 | 7.7 | 7.8 | 7.8 | 7.8 |
| 18.000 | 7.8 | 7.8 | 7.8 | 7.8 | 7.8 |
| 18.500 | 7.9 | 7.9 | 7.9 | 7.9 | 7.9 |
| 19.000 | 7.9 | 7.9 | 7.9 | 8.0 | 8.0 |
| 19.500 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| 20.000 | 8.0 | 8.0 | 8.1 | 8.1 | 8.1 |
| 20.500 | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 |
| 21.000 | 8.1 | 8.2 | 8.2 | 8.2 | 8.2 |
| 21.500 | 8.2 | 8.2 | 8.2 | 8.2 | 8.2 |
| 22.000 | 8.2 | 8.2 | 8.3 | 8.3 | 8.3 |
| 22.500 | 8.3 | 8.3 | 8.3 | 8.3 | 8.3 |
| 23.000 | 8.3 | 8.3 | 8.3 | 8.3 | 8.4 |
| 23.500 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 |
| 24.000 | 8.4 | (N/A) | (N/A) | (N/A) | (N/A) |

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 55.00 ft |
| Manning's n | 0.240 |
| Slope | 0.094 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.068 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | True |
| Slope | 0.065 ft/ft |
| Average Velocity | 5.18 ft/s |
| Segment Time of Concentration | 0.004 hours |

| Segment #3: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 100.12 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 4.93 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Channel Flow | |
|---|---|
| Flow Area | 1.2 ft² |
| Hydraulic Length | 57.93 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.93 ft |
| Average Velocity | 5.73 ft/s |
| Segment Time of Concentration | 0.003 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 55.00 ft |
| Manning's n | 0.240 |
| Slope | 0.094 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.068 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | True |
| Slope | 0.065 ft/ft |
| Average Velocity | 5.18 ft/s |
| Segment Time of Concentration | 0.004 hours |

| Segment #3: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 100.12 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 4.93 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Channel Flow | |
|---|---|
| Flow Area | 1.2 ft² |
| Hydraulic Length | 57.93 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.93 ft |
| Average Velocity | 5.73 ft/s |
| Segment Time of Concentration | 0.003 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== SCS Channel Flow

| | |
|---|---|
| Tc = | R = Qa / Wp |
| | V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n |
| | (Lf / V) / 3600 |
| Where: | R= Hydraulic radius |
| | Aq= Flow area, square feet |
| | Wp= Wetted perimeter, feet |
| | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | n= Manning's n |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Shallow Concentration Flow

| | |
|---|---|
| Tc = | Unpaved surface: |
| | V = 16.1345 * (Sf**0.5) |
| | Paved Surface: |
| | V = 20.3282 * (Sf**0.5) |
| | (Lf / V) / 3600 |
| Where: | V= Velocity, ft/sec |
| | Sf= Slope, ft/ft |
| | Tc= Time of concentration, hours |
| | Lf= Flow length, feet |

## ==== SCS TR-55 Sheet Flow

| | |
|---|---|
| Tc = | (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4)) |
| Where: | Tc= Time of concentration, hours |
| | n= Manning's n |
| | Lf= Flow length, feet |
| | P= 2yr, 24hr Rain depth, inches |
| | Sf= Slope, % |

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 55.00 ft |
| Manning's n | 0.240 |
| Slope | 0.094 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.068 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | True |
| Slope | 0.065 ft/ft |
| Average Velocity | 5.18 ft/s |
| Segment Time of Concentration | 0.004 hours |

| Segment #3: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 100.12 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 4.93 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Channel Flow | |
|---|---|
| Flow Area | 1.2 ft² |
| Hydraulic Length | 57.93 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.93 ft |
| Average Velocity | 5.73 ft/s |
| Segment Time of Concentration | 0.003 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== SCS Channel Flow

Tc = R = Qa / Wp
V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n

(Lf / V) / 3600

Where:
R= Hydraulic radius
Aq= Flow area, square feet
Wp= Wetted perimeter, feet
V= Velocity, ft/sec
Sf= Slope, ft/ft
n= Manning's n
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:
V = 16.1345 * (Sf**0.5)

Paved Surface:
V = 20.3282 * (Sf**0.5)

(Lf / V) / 3600

Where:
V= Velocity, ft/sec
Sf= Slope, ft/ft
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Sheet Flow

Tc = (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4))

Where:
Tc= Time of concentration, hours
n= Manning's n
Lf= Flow length, feet
P= 2yr, 24hr Rain depth, inches
Sf= Slope, %

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 55.00 ft |
| Manning's n | 0.240 |
| Slope | 0.094 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.068 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | True |
| Slope | 0.065 ft/ft |
| Average Velocity | 5.18 ft/s |
| Segment Time of Concentration | 0.004 hours |

| Segment #3: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 100.12 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 4.93 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Channel Flow | |
|---|---|
| Flow Area | 1.2 ft² |
| Hydraulic Length | 57.93 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.93 ft |
| Average Velocity | 5.73 ft/s |
| Segment Time of Concentration | 0.003 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== SCS Channel Flow

Tc = R = Qa / Wp
V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n

(Lf / V) / 3600

Where:
R= Hydraulic radius
Aq= Flow area, square feet
Wp= Wetted perimeter, feet
V= Velocity, ft/sec
Sf= Slope, ft/ft
n= Manning's n
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:
V = 16.1345 * (Sf**0.5)

Paved Surface:
V = 20.3282 * (Sf**0.5)

(Lf / V) / 3600

Where:
V= Velocity, ft/sec
Sf= Slope, ft/ft
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Sheet Flow

Tc = (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4))

Where:
Tc= Time of concentration, hours
n= Manning's n
Lf= Flow length, feet
P= 2yr, 24hr Rain depth, inches
Sf= Slope, %

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Time of Concentration Results

| Segment #1: TR-55 Sheet Flow | |
|---|---|
| Hydraulic Length | 55.00 ft |
| Manning's n | 0.240 |
| Slope | 0.094 ft/ft |
| 2 Year 24 Hour Depth | 4.3 in |
| Average Velocity | 0.22 ft/s |
| Segment Time of Concentration | 0.068 hours |

| Segment #2: TR-55 Shallow Concentrated Flow | |
|---|---|
| Hydraulic Length | 80.00 ft |
| Is Paved? | True |
| Slope | 0.065 ft/ft |
| Average Velocity | 5.18 ft/s |
| Segment Time of Concentration | 0.004 hours |

| Segment #3: TR-55 Channel Flow | |
|---|---|
| Flow Area | 0.8 ft² |
| Hydraulic Length | 100.12 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.14 ft |
| Average Velocity | 4.93 ft/s |
| Segment Time of Concentration | 0.006 hours |

| Segment #4: TR-55 Channel Flow | |
|---|---|
| Flow Area | 1.2 ft² |
| Hydraulic Length | 57.93 ft |
| Manning's n | 0.012 |
| Slope | 0.010 ft/ft |
| Wetted Perimeter | 3.93 ft |
| Average Velocity | 5.73 ft/s |
| Segment Time of Concentration | 0.003 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## ==== SCS Channel Flow

Tc = R = Qa / Wp
V = (1.49 * (R**(2/3)) * (Sf**-0.5)) / n

(Lf / V) / 3600

Where:
R= Hydraulic radius
Aq= Flow area, square feet
Wp= Wetted perimeter, feet
V= Velocity, ft/sec
Sf= Slope, ft/ft
n= Manning's n
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:
V = 16.1345 * (Sf**0.5)

Paved Surface:
V = 20.3282 * (Sf**0.5)

(Lf / V) / 3600

Where:
V= Velocity, ft/sec
Sf= Slope, ft/ft
Tc= Time of concentration, hours
Lf= Flow length, feet

## ==== SCS TR-55 Sheet Flow

Tc = (0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4))

Where:
Tc= Time of concentration, hours
n= Manning's n
Lf= Flow length, feet
P= 2yr, 24hr Rain depth, inches
Sf= Slope, %

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Time of Concentration Results

| Segment #1: User Defined Tc | |
|---|---|
| Time of Concentration | 0.100 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== User Defined

| | |
|---|---|
| Tc = | Value entered by user |
| Where: | Tc= Time of concentration, hours |

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Time of Concentration Results

| Segment #1: User Defined Tc | |
|---|---|
| Time of Concentration | 0.100 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== User Defined

| | |
|---|---|
| Tc = | Value entered by user |
| Where: | Tc= Time of concentration, hours |

Subsection: Time of Concentration Calculations
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Time of Concentration Results

| Segment #1: User Defined Tc | |
|---|---|
| Time of Concentration | 0.100 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== User Defined

| | |
|---|---|
| Tc = | Value entered by user |
| Where: | Tc= Time of concentration, hours |

Time of Concentration Results

| Segment #1: User Defined Tc | |
|---|---|
| Time of Concentration | 0.100 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== User Defined

| | |
|---|---|
| Tc = | Value entered by user |
| Where: | Tc= Time of concentration, hours |

# Post-Development Conditions

Subsection: Time of Concentration Calculations
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Time of Concentration Results

| Segment #1: User Defined Tc | |
|---|---|
| Time of Concentration | 0.100 hours |

| Time of Concentration (Composite) | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |

## ==== User Defined

| | |
|---|---|
| Tc = | Value entered by user |
| Where: | Tc= Time of concentration, hours |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.140 | 0.0 | 0.0 | 61.000 |
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil B | 98.000 | 0.030 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 0.170 | (N/A) | (N/A) | 67.529 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Proposed Impervious Coverage | 98.000 | 0.610 | 0.0 | 0.0 | 98.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.800 | 0.0 | 0.0 | 61.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.410 | (N/A) | (N/A) | 77.007 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Proposed Impervious Coverage | 98.000 | 0.610 | 0.0 | 0.0 | 98.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.800 | 0.0 | 0.0 | 61.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.410 | (N/A) | (N/A) | 77.007 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Proposed Impervious Coverage | 98.000 | 0.610 | 0.0 | 0.0 | 98.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.800 | 0.0 | 0.0 | 61.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.410 | (N/A) | (N/A) | 77.007 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Proposed Impervious Coverage | 98.000 | 0.610 | 0.0 | 0.0 | 98.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.800 | 0.0 | 0.0 | 61.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.410 | (N/A) | (N/A) | 77.007 |

# Post-Development Conditions

Subsection: Runoff CN-Area
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Runoff Curve Number Data

| Soil/Surface Description | CN | Area (acres) | C (%) | UC (%) | Adjusted CN |
|---|---|---|---|---|---|
| Proposed Impervious Coverage | 98.000 | 0.610 | 0.0 | 0.0 | 98.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil B | 61.000 | 0.800 | 0.0 | 0.0 | 61.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 1.410 | (N/A) | (N/A) | 77.007 |

## Unit Hydrograph Method (Computational Notes)

### Definition of Terms

| | |
|---|---|
| At | Total area (acres): At = Ai+Ap |
| Ai | Impervious area (acres) |
| Ap | Pervious area (acres) |
| CNi | Runoff curve number for impervious area |
| CNp | Runoff curve number for pervious area |
| fLoss | f loss constant infiltration (depth/time) |
| gKs | Saturated Hydraulic Conductivity (depth/time) |
| Md | Volumetric Moisture Deficit |
| Psi | Capillary Suction (length) |
| hK | Horton Infiltration Decay Rate (time^-1) |
| fo | Initial Infiltration Rate (depth/time) |
| fc | Ultimate(capacity)Infiltration Rate (depth/time) |
| Ia | Initial Abstraction (length) |
| dt | Computational increment (duration of unit excess rainfall)<br>Default dt is smallest value of 0.1333Tc, rtm, and th<br>(Smallest dt is then adjusted to match up with Tp) |
| UDdt | User specified override computational main time increment<br>(only used if UDdt is => .1333Tc) |
| D(t) | Point on distribution curve (fraction of P) for time step t |
| K | 2 / (1 + (Tr/Tp)): default K = 0.75: (for Tr/Tp = 1.67) |
| Ks | Hydrograph shape factor = Unit Conversions * K: = ((1hr/3600sec) * (1ft/12in) * ((5280ft)**2/sq.mi)) * K<br>Default Ks = 645.333 * 0.75 = 484 |
| Lag | Lag time from center of excess runoff (dt) to Tp: Lag = 0.6Tc |
| P | Total precipitation depth, inches |
| Pa(t) | Accumulated rainfall at time step t |
| Pi(t) | Incremental rainfall at time step t |
| qp | Peak discharge (cfs) for 1in. runoff, for 1hr, for 1 sq.mi. = (Ks * A * Q) / Tp (where Q = 1in. runoff, A=sq.mi.) |
| Qu(t) | Unit hydrograph ordinate (cfs) at time step t |
| Q(t) | Final hydrograph ordinate (cfs) at time step t |
| Rai(t) | Accumulated runoff (inches) at time step t for impervious area |
| Rap(t) | Accumulated runoff (inches) at time step t for pervious area |
| Rii(t) | Incremental runoff (inches) at time step t for impervious area |
| Rip(t) | Incremental runoff (inches) at time step t for pervious area |
| R(t) | Incremental weighted total runoff (inches) |
| Rtm | Time increment for rainfall table |
| Si | S for impervious area: Si = (1000/CNi) - 10 |
| Sp | S for pervious area: Sp = (1000/CNp) - 10 |
| t | Time step (row) number |
| Tc | Time of concentration |
| Tb | Time (hrs) of entire unit hydrograph: Tb = Tp + Tr |
| Tp | Time (hrs) to peak of a unit hydrograph: Tp = (dt/2) + Lag |
| Tr | Time (hrs) of receding limb of unit hydrograph: Tr = ratio of Tp |

# Post-Development Conditions

Subsection: Unit Hydrograph Equations

## Unit Hydrograph Method
## Computational Notes
## Precipitation

| | |
|---|---|
| Column (1) | Time for time step t |
| Column (2) | D(t) = Point on distribution curve for time step t |
| Column (3) | Pi(t) = Pa(t) - Pa(t-1): Col.(4) - Preceding Col.(4) |
| Column (4) | Pa(t) = D(t) x P: Col.(2) x P |

## Pervious Area Runoff (using SCS Runoff CN Method)

| | |
|---|---|
| Column (5) | Rap(t) = Accumulated pervious runoff for time step t<br>If (Pa(t) is <= 0.2Sp) then use: Rap(t) = 0.0<br>If (Pa(t) is > 0.2Sp) then use:<br><br>Rap(t) = (Col.(4)-0.2Sp)**2 / (Col.(4)+0.8Sp) |
| Column (6) | Rip(t) = Incremental pervious runoff for time step t<br>Rip(t) = Rap(t) - Rap(t-1)<br>Rip(t) = Col.(5) for current row - Col.(5) for preceding row. |

## Impervious Area Runoff

| | |
|---|---|
| Column (7 & 8)... | Did not specify to use impervious areas. |

## Incremental Weighted Runoff

| | |
|---|---|
| Column (9) | R(t) = (Ap/At) x Rip(t) + (Ai/At) x Rii(t)<br>R(t) = (Ap/At) x Col.(6) + (Ai/At) x Col.(8) |

## SCS Unit Hydrograph Method

| | |
|---|---|
| Column (10) | Q(t) is computed with the SCS unit hydrograph method using R(t) and Qu(t). |

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.24 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.133 hours |
| Flow (Peak Interpolated Output) | 0.24 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 1.4 in |
| Runoff Volume (Pervious) | 0.020 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.020 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 2 years
Label: Offsite
Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.93 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 10.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 11.133 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| 11.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 11.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 11.633 | 0.02 | 0.02 | 0.03 | 0.03 | 0.04 |
| 11.800 | 0.05 | 0.05 | 0.06 | 0.07 | 0.09 |
| 11.967 | 0.13 | 0.17 | 0.20 | 0.22 | 0.23 |
| 12.133 | 0.24 | 0.20 | 0.17 | 0.15 | 0.14 |
| 12.300 | 0.13 | 0.12 | 0.11 | 0.10 | 0.09 |
| 12.467 | 0.08 | 0.07 | 0.06 | 0.06 | 0.05 |
| 12.633 | 0.05 | 0.04 | 0.04 | 0.04 | 0.04 |
| 12.800 | 0.04 | 0.04 | 0.04 | 0.04 | 0.03 |
| 12.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.133 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.300 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.467 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 13.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 13.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 13.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 14.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 15.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 15.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 16.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 16.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 22.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Offsite Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 23.133 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 23.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 24.133 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 0.46 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.45 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.6 in |
| Runoff Volume (Pervious) | 0.037 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.037 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 10 years
Label: Offsite
Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.93 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.567 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.733 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 11.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| 11.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 11.567 | 0.04 | 0.04 | 0.05 | 0.06 | 0.07 |
| 11.733 | 0.08 | 0.10 | 0.11 | 0.13 | 0.15 |
| 11.900 | 0.17 | 0.20 | 0.27 | 0.35 | 0.40 |
| 12.067 | 0.43 | 0.45 | 0.45 | 0.38 | 0.32 |
| 12.233 | 0.28 | 0.25 | 0.23 | 0.22 | 0.20 |
| 12.400 | 0.18 | 0.16 | 0.14 | 0.12 | 0.11 |
| 12.567 | 0.10 | 0.09 | 0.08 | 0.08 | 0.07 |
| 12.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 12.900 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 13.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.400 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 |
| 13.567 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 13.733 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 13.900 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.067 | 0.04 | 0.04 | 0.04 | 0.03 | 0.03 |
| 14.233 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.567 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 14.733 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Offsite Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 14.900 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.067 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.233 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.400 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.733 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 15.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.400 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.733 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 17.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 17.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Offsite Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 21.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.067 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.067 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.58 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.58 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.3 in |
| Runoff Volume (Pervious) | 0.047 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.047 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 25 years
Label: Offsite
Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.93 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.033 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.367 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.533 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.533 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 |
| 10.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 11.033 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 11.200 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 11.367 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 11.533 | 0.05 | 0.06 | 0.06 | 0.07 | 0.09 |
| 11.700 | 0.10 | 0.12 | 0.14 | 0.16 | 0.17 |
| 11.867 | 0.20 | 0.22 | 0.26 | 0.36 | 0.45 |
| 12.033 | 0.51 | 0.55 | 0.58 | 0.57 | 0.48 |
| 12.200 | 0.40 | 0.35 | 0.32 | 0.29 | 0.27 |
| 12.367 | 0.24 | 0.22 | 0.20 | 0.18 | 0.15 |
| 12.533 | 0.14 | 0.12 | 0.11 | 0.10 | 0.09 |
| 12.700 | 0.09 | 0.09 | 0.09 | 0.08 | 0.08 |
| 12.867 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 13.033 | 0.07 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.200 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.367 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 13.533 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.700 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 13.867 | 0.05 | 0.05 | 0.05 | 0.05 | 0.04 |
| 14.033 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.200 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 14.367 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.533 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.700 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.867 | 0.04 | 0.04 | 0.04 | 0.03 | 0.03 |
| 15.033 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.200 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.367 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.533 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.700 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.867 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 |
| 16.033 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.200 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.367 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.033 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.200 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.367 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.700 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.033 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 18.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 19.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Offsite Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 21.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.533 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.700 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.033 | 0.01 | 0.00 | 0.00 | 0.00 | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.74 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.73 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.2 in |
| Runoff Volume (Pervious) | 0.060 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.060 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 50 years
Label: Offsite
Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.93 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.467 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.633 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.967 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.133 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 10.133 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.633 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 10.800 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| 11.133 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 11.300 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 11.467 | 0.06 | 0.06 | 0.07 | 0.08 | 0.09 |
| 11.633 | 0.10 | 0.12 | 0.14 | 0.16 | 0.19 |
| 11.800 | 0.21 | 0.23 | 0.26 | 0.29 | 0.34 |
| 11.967 | 0.47 | 0.59 | 0.66 | 0.70 | 0.73 |
| 12.133 | 0.72 | 0.60 | 0.50 | 0.44 | 0.39 |
| 12.300 | 0.36 | 0.34 | 0.30 | 0.28 | 0.25 |
| 12.467 | 0.22 | 0.19 | 0.17 | 0.15 | 0.13 |
| 12.633 | 0.12 | 0.12 | 0.11 | 0.11 | 0.11 |
| 12.800 | 0.10 | 0.10 | 0.10 | 0.09 | 0.09 |
| 12.967 | 0.09 | 0.08 | 0.08 | 0.08 | 0.08 |
| 13.133 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 13.300 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 13.467 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 13.633 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Offsite Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.800 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.967 | 0.06 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.133 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.300 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.467 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.633 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.800 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 14.967 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.133 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.300 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.467 | 0.04 | 0.04 | 0.04 | 0.04 | 0.03 |
| 15.633 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.800 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.967 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.133 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.300 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.467 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.633 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.800 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 16.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.967 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.133 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.300 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.467 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.633 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.800 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Offsite Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.133 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.300 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.467 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.633 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.800 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.967 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 |
| 24.133 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.80 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.79 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 68.000 |
| Area (User Defined) | 0.170 acres |
| Maximum Retention (Pervious) | 4.7 in |
| Maximum Retention (Pervious, 20 percent) | 0.9 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.6 in |
| Runoff Volume (Pervious) | 0.065 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.065 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Offsite
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 1.93 ft³/s |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 0.170 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.267 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.433 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.933 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.933 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 10.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| 10.600 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.933 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 |
| 11.100 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 11.267 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 11.433 | 0.06 | 0.07 | 0.07 | 0.07 | 0.09 |
| 11.600 | 0.10 | 0.11 | 0.13 | 0.15 | 0.17 |
| 11.767 | 0.20 | 0.23 | 0.25 | 0.29 | 0.32 |
| 11.933 | 0.38 | 0.51 | 0.64 | 0.71 | 0.76 |
| 12.100 | 0.79 | 0.77 | 0.65 | 0.54 | 0.48 |
| 12.267 | 0.42 | 0.39 | 0.36 | 0.33 | 0.30 |
| 12.433 | 0.27 | 0.23 | 0.20 | 0.18 | 0.16 |
| 12.600 | 0.14 | 0.13 | 0.12 | 0.12 | 0.12 |
| 12.767 | 0.11 | 0.11 | 0.11 | 0.10 | 0.10 |
| 12.933 | 0.10 | 0.09 | 0.09 | 0.09 | 0.08 |
| 13.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 13.267 | 0.08 | 0.08 | 0.08 | 0.07 | 0.07 |
| 13.433 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.600 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 13.767 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 13.933 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 14.100 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 14.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.433 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.600 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 14.933 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 |
| 15.100 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.267 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.433 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 15.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 15.933 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.100 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.267 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.433 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.600 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 16.933 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 17.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 17.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 18.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 19.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 20.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Offsite Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.600 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 |
| 20.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 20.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 21.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 22.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 23.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.100 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.120 hours |
| Flow (Peak, Computed) | 2.97 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 2.95 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 1.410 acres |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 2.0 in |
| Runoff Volume (Pervious) | 0.241 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.241 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 2 years
Label: Site
Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.98 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Site Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| | |
|---|---|
| Storm Event | TypeIII 24hr (4.3 in) |
| Return Event | 2 years |
| Duration | 80.000 hours |
| Depth | 4.3 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 8.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.067 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 |
| 9.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.400 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 |
| 9.567 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 9.733 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 9.900 | 0.03 | 0.03 | 0.03 | 0.04 | 0.04 |
| 10.067 | 0.04 | 0.04 | 0.04 | 0.04 | 0.05 |
| 10.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 10.400 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 |
| 10.567 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 |
| 10.733 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 |
| 10.900 | 0.10 | 0.10 | 0.10 | 0.11 | 0.11 |
| 11.067 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 |
| 11.233 | 0.15 | 0.16 | 0.17 | 0.17 | 0.18 |
| 11.400 | 0.19 | 0.20 | 0.21 | 0.22 | 0.24 |
| 11.567 | 0.28 | 0.32 | 0.36 | 0.44 | 0.52 |
| 11.733 | 0.59 | 0.69 | 0.79 | 0.88 | 1.00 |
| 11.900 | 1.12 | 1.33 | 1.83 | 2.31 | 2.61 |
| 12.067 | 2.80 | 2.95 | 2.90 | 2.45 | 2.03 |
| 12.233 | 1.81 | 1.61 | 1.48 | 1.39 | 1.25 |
| 12.400 | 1.14 | 1.05 | 0.90 | 0.78 | 0.71 |
| 12.567 | 0.62 | 0.55 | 0.51 | 0.48 | 0.47 |
| 12.733 | 0.45 | 0.44 | 0.43 | 0.42 | 0.40 |
| 12.900 | 0.39 | 0.38 | 0.36 | 0.35 | 0.34 |
| 13.067 | 0.33 | 0.32 | 0.32 | 0.31 | 0.31 |
| 13.233 | 0.31 | 0.30 | 0.30 | 0.30 | 0.29 |
| 13.400 | 0.29 | 0.29 | 0.28 | 0.28 | 0.28 |
| 13.567 | 0.27 | 0.27 | 0.27 | 0.26 | 0.26 |
| 13.733 | 0.26 | 0.25 | 0.25 | 0.25 | 0.24 |
| 13.900 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 14.067 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Site Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 14.233 | 0.22 | 0.21 | 0.21 | 0.21 | 0.21 |
| 14.400 | 0.21 | 0.21 | 0.20 | 0.20 | 0.20 |
| 14.567 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |
| 14.733 | 0.19 | 0.19 | 0.19 | 0.19 | 0.18 |
| 14.900 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 15.067 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 15.233 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 15.400 | 0.16 | 0.16 | 0.15 | 0.15 | 0.15 |
| 15.567 | 0.15 | 0.15 | 0.15 | 0.14 | 0.14 |
| 15.733 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 15.900 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 16.067 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 16.233 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 16.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 16.567 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 16.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.10 |
| 16.900 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.067 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.233 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 17.400 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 17.567 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 17.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 17.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.233 | 0.08 | 0.08 | 0.07 | 0.07 | 0.07 |
| 18.400 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 18.567 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 18.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 18.900 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 19.067 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 19.233 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 19.400 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 19.567 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 19.733 | 0.07 | 0.06 | 0.06 | 0.06 | 0.06 |
| 19.900 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.067 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.400 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.567 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.733 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 20.900 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 21.067 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 2 years
Label: Site Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 21.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 21.400 | 0.06 | 0.06 | 0.06 | 0.06 | 0.05 |
| 21.567 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.733 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 21.900 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.400 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.567 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.733 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 22.900 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.400 | 0.05 | 0.05 | 0.05 | 0.04 | 0.04 |
| 23.567 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.733 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 23.900 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 24.067 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 5.01 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 4.98 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 1.410 acres |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 3.5 in |
| Runoff Volume (Pervious) | 0.409 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.409 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.98 ft³/s |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.0 in) |
| Return Event | 10 years |
| Duration | 80.000 hours |
| Depth | 6.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.533 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.700 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 |
| 7.867 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.200 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.367 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| 8.533 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.700 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.867 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 9.033 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 |
| 9.200 | 0.06 | 0.06 | 0.06 | 0.06 | 0.07 |
| 9.367 | 0.07 | 0.07 | 0.07 | 0.07 | 0.08 |
| 9.533 | 0.08 | 0.08 | 0.08 | 0.09 | 0.09 |
| 9.700 | 0.09 | 0.09 | 0.09 | 0.10 | 0.10 |
| 9.867 | 0.10 | 0.10 | 0.11 | 0.11 | 0.11 |
| 10.033 | 0.11 | 0.12 | 0.12 | 0.12 | 0.13 |
| 10.200 | 0.13 | 0.13 | 0.14 | 0.14 | 0.15 |
| 10.367 | 0.15 | 0.16 | 0.16 | 0.16 | 0.17 |
| 10.533 | 0.17 | 0.18 | 0.18 | 0.19 | 0.19 |
| 10.700 | 0.20 | 0.20 | 0.21 | 0.21 | 0.22 |
| 10.867 | 0.22 | 0.23 | 0.23 | 0.24 | 0.24 |
| 11.033 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 11.200 | 0.31 | 0.32 | 0.34 | 0.35 | 0.37 |
| 11.367 | 0.39 | 0.40 | 0.42 | 0.44 | 0.45 |
| 11.533 | 0.49 | 0.57 | 0.64 | 0.72 | 0.88 |
| 11.700 | 1.02 | 1.14 | 1.33 | 1.49 | 1.64 |
| 11.867 | 1.86 | 2.05 | 2.41 | 3.27 | 4.06 |
| 12.033 | 4.52 | 4.80 | 4.98 | 4.85 | 4.07 |
| 12.200 | 3.35 | 2.97 | 2.63 | 2.41 | 2.25 |
| 12.367 | 2.02 | 1.83 | 1.68 | 1.45 | 1.26 |
| 12.533 | 1.13 | 0.99 | 0.87 | 0.81 | 0.77 |
| 12.700 | 0.74 | 0.72 | 0.70 | 0.68 | 0.66 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Site Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.867 | 0.63 | 0.61 | 0.60 | 0.57 | 0.55 |
| 13.033 | 0.54 | 0.52 | 0.51 | 0.50 | 0.49 |
| 13.200 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 13.367 | 0.46 | 0.46 | 0.45 | 0.45 | 0.44 |
| 13.533 | 0.44 | 0.43 | 0.42 | 0.42 | 0.41 |
| 13.700 | 0.41 | 0.40 | 0.40 | 0.39 | 0.39 |
| 13.867 | 0.38 | 0.38 | 0.37 | 0.37 | 0.36 |
| 14.033 | 0.36 | 0.35 | 0.35 | 0.34 | 0.34 |
| 14.200 | 0.34 | 0.34 | 0.33 | 0.33 | 0.33 |
| 14.367 | 0.33 | 0.32 | 0.32 | 0.32 | 0.31 |
| 14.533 | 0.31 | 0.31 | 0.31 | 0.31 | 0.30 |
| 14.700 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 14.867 | 0.29 | 0.28 | 0.28 | 0.28 | 0.28 |
| 15.033 | 0.27 | 0.27 | 0.27 | 0.27 | 0.26 |
| 15.200 | 0.26 | 0.26 | 0.25 | 0.25 | 0.25 |
| 15.367 | 0.25 | 0.24 | 0.24 | 0.24 | 0.24 |
| 15.533 | 0.23 | 0.23 | 0.23 | 0.23 | 0.22 |
| 15.700 | 0.22 | 0.22 | 0.21 | 0.21 | 0.21 |
| 15.867 | 0.21 | 0.20 | 0.20 | 0.20 | 0.19 |
| 16.033 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 16.200 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 16.367 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 16.533 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 16.700 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |
| 16.867 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 17.033 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 17.200 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 17.367 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 17.533 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 17.700 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 17.867 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.033 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 18.200 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 18.367 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 18.533 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 18.700 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 18.867 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.033 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.200 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 19.367 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 19.533 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 19.700 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 10 years
Label: Site Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.867 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.033 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.200 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 20.367 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 20.533 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 20.700 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 20.867 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.033 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.200 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.367 | 0.09 | 0.09 | 0.09 | 0.08 | 0.08 |
| 21.533 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.700 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.367 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.533 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 22.700 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 22.867 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.033 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.200 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.367 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.533 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.700 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 23.867 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 24.033 | 0.06 | 0.04 | 0.02 | 0.01 | 0.00 |
| 24.200 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 6.12 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 6.09 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 1.410 acres |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 4.3 in |
| Runoff Volume (Pervious) | 0.502 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.502 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Return Event: 25 years
Label: Site
Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.98 $ft^3/s$ |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (6.9 in) |
| Return Event | 25 years |
| Duration | 80.000 hours |
| Depth | 6.9 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.933 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.100 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 |
| 7.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.600 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.767 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.933 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.100 | 0.03 | 0.03 | 0.03 | 0.03 | 0.04 |
| 8.267 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.433 | 0.04 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.600 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.767 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.933 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.100 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 |
| 9.267 | 0.10 | 0.10 | 0.10 | 0.10 | 0.11 |
| 9.433 | 0.11 | 0.11 | 0.11 | 0.12 | 0.12 |
| 9.600 | 0.12 | 0.13 | 0.13 | 0.13 | 0.13 |
| 9.767 | 0.14 | 0.14 | 0.14 | 0.15 | 0.15 |
| 9.933 | 0.15 | 0.16 | 0.16 | 0.16 | 0.17 |
| 10.100 | 0.17 | 0.17 | 0.18 | 0.18 | 0.19 |
| 10.267 | 0.19 | 0.20 | 0.20 | 0.21 | 0.21 |
| 10.433 | 0.22 | 0.23 | 0.23 | 0.24 | 0.24 |
| 10.600 | 0.25 | 0.25 | 0.26 | 0.27 | 0.27 |
| 10.767 | 0.28 | 0.28 | 0.29 | 0.30 | 0.30 |
| 10.933 | 0.31 | 0.32 | 0.32 | 0.33 | 0.34 |
| 11.100 | 0.36 | 0.37 | 0.39 | 0.41 | 0.42 |
| 11.267 | 0.44 | 0.46 | 0.48 | 0.50 | 0.52 |
| 11.433 | 0.54 | 0.57 | 0.59 | 0.63 | 0.73 |
| 11.600 | 0.82 | 0.92 | 1.12 | 1.30 | 1.45 |
| 11.767 | 1.69 | 1.89 | 2.07 | 2.33 | 2.57 |
| 11.933 | 3.01 | 4.06 | 5.03 | 5.57 | 5.89 |
| 12.100 | 6.09 | 5.91 | 4.95 | 4.07 | 3.59 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Site Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.267 | 3.18 | 2.91 | 2.71 | 2.43 | 2.20 |
| 12.433 | 2.02 | 1.74 | 1.51 | 1.36 | 1.18 |
| 12.600 | 1.05 | 0.97 | 0.92 | 0.89 | 0.86 |
| 12.767 | 0.83 | 0.81 | 0.79 | 0.76 | 0.74 |
| 12.933 | 0.72 | 0.69 | 0.66 | 0.65 | 0.62 |
| 13.100 | 0.61 | 0.60 | 0.59 | 0.58 | 0.58 |
| 13.267 | 0.57 | 0.56 | 0.56 | 0.55 | 0.54 |
| 13.433 | 0.54 | 0.53 | 0.53 | 0.52 | 0.51 |
| 13.600 | 0.51 | 0.50 | 0.49 | 0.49 | 0.48 |
| 13.767 | 0.47 | 0.47 | 0.46 | 0.45 | 0.45 |
| 13.933 | 0.44 | 0.44 | 0.43 | 0.42 | 0.42 |
| 14.100 | 0.41 | 0.41 | 0.41 | 0.40 | 0.40 |
| 14.267 | 0.40 | 0.39 | 0.39 | 0.39 | 0.38 |
| 14.433 | 0.38 | 0.38 | 0.37 | 0.37 | 0.37 |
| 14.600 | 0.37 | 0.36 | 0.36 | 0.36 | 0.35 |
| 14.767 | 0.35 | 0.35 | 0.34 | 0.34 | 0.34 |
| 14.933 | 0.33 | 0.33 | 0.33 | 0.33 | 0.32 |
| 15.100 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 15.267 | 0.30 | 0.30 | 0.30 | 0.29 | 0.29 |
| 15.433 | 0.29 | 0.28 | 0.28 | 0.28 | 0.27 |
| 15.600 | 0.27 | 0.27 | 0.26 | 0.26 | 0.26 |
| 15.767 | 0.25 | 0.25 | 0.25 | 0.24 | 0.24 |
| 15.933 | 0.24 | 0.23 | 0.23 | 0.23 | 0.23 |
| 16.100 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.267 | 0.22 | 0.21 | 0.21 | 0.21 | 0.21 |
| 16.433 | 0.21 | 0.21 | 0.21 | 0.21 | 0.20 |
| 16.600 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 16.767 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 16.933 | 0.19 | 0.19 | 0.18 | 0.18 | 0.18 |
| 17.100 | 0.18 | 0.18 | 0.18 | 0.18 | 0.17 |
| 17.267 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 17.433 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 17.600 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 17.767 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 17.933 | 0.15 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.100 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 18.433 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.600 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.933 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 19.100 | 0.13 | 0.13 | 0.13 | 0.12 | 0.12 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 25 years
Label: Site Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.267 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.433 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.767 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.933 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.100 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.267 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.600 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.767 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.933 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 21.100 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.267 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.433 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.600 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.767 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.933 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 22.100 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.267 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.433 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.600 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.767 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.933 | 0.09 | 0.09 | 0.09 | 0.09 | 0.08 |
| 23.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.600 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.767 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.933 | 0.08 | 0.08 | 0.08 | 0.07 | 0.04 |
| 24.100 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 7.48 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 7.46 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 1.410 acres |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 5.3 in |
| Runoff Volume (Pervious) | 0.620 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.620 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.98 ft³/s |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.0 in) |
| Return Event | 50 years |
| Duration | 80.000 hours |
| Depth | 8.0 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.267 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.433 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 |
| 6.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.267 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.433 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 7.767 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 7.933 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.100 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.267 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.433 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.600 | 0.09 | 0.09 | 0.09 | 0.09 | 0.10 |
| 8.767 | 0.10 | 0.10 | 0.10 | 0.11 | 0.11 |
| 8.933 | 0.11 | 0.12 | 0.12 | 0.12 | 0.12 |
| 9.100 | 0.13 | 0.13 | 0.13 | 0.14 | 0.14 |
| 9.267 | 0.14 | 0.15 | 0.15 | 0.15 | 0.16 |
| 9.433 | 0.16 | 0.16 | 0.17 | 0.17 | 0.17 |
| 9.600 | 0.18 | 0.18 | 0.18 | 0.19 | 0.19 |
| 9.767 | 0.19 | 0.20 | 0.20 | 0.21 | 0.21 |
| 9.933 | 0.21 | 0.22 | 0.22 | 0.23 | 0.23 |
| 10.100 | 0.24 | 0.24 | 0.25 | 0.25 | 0.26 |
| 10.267 | 0.27 | 0.27 | 0.28 | 0.29 | 0.29 |
| 10.433 | 0.30 | 0.31 | 0.31 | 0.32 | 0.33 |
| 10.600 | 0.33 | 0.34 | 0.35 | 0.36 | 0.36 |
| 10.767 | 0.37 | 0.38 | 0.39 | 0.39 | 0.40 |
| 10.933 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 |
| 11.100 | 0.47 | 0.48 | 0.51 | 0.53 | 0.55 |
| 11.267 | 0.58 | 0.60 | 0.62 | 0.65 | 0.68 |
| 11.433 | 0.70 | 0.73 | 0.76 | 0.81 | 0.94 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Site Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 11.600 | 1.05 | 1.18 | 1.43 | 1.65 | 1.84 |
| 11.767 | 2.14 | 2.39 | 2.61 | 2.93 | 3.23 |
| 11.933 | 3.76 | 5.05 | 6.23 | 6.86 | 7.24 |
| 12.100 | 7.46 | 7.21 | 6.03 | 4.95 | 4.36 |
| 12.267 | 3.86 | 3.52 | 3.28 | 2.94 | 2.66 |
| 12.433 | 2.44 | 2.10 | 1.82 | 1.64 | 1.43 |
| 12.600 | 1.26 | 1.17 | 1.11 | 1.07 | 1.04 |
| 12.767 | 1.00 | 0.97 | 0.95 | 0.91 | 0.88 |
| 12.933 | 0.86 | 0.82 | 0.79 | 0.77 | 0.75 |
| 13.100 | 0.73 | 0.72 | 0.71 | 0.70 | 0.69 |
| 13.267 | 0.68 | 0.67 | 0.67 | 0.66 | 0.65 |
| 13.433 | 0.65 | 0.64 | 0.63 | 0.62 | 0.61 |
| 13.600 | 0.61 | 0.60 | 0.59 | 0.58 | 0.58 |
| 13.767 | 0.57 | 0.56 | 0.55 | 0.54 | 0.54 |
| 13.933 | 0.53 | 0.52 | 0.51 | 0.51 | 0.50 |
| 14.100 | 0.49 | 0.49 | 0.48 | 0.48 | 0.48 |
| 14.267 | 0.47 | 0.47 | 0.47 | 0.46 | 0.46 |
| 14.433 | 0.46 | 0.45 | 0.45 | 0.44 | 0.44 |
| 14.600 | 0.44 | 0.43 | 0.43 | 0.42 | 0.42 |
| 14.767 | 0.42 | 0.41 | 0.41 | 0.41 | 0.40 |
| 14.933 | 0.40 | 0.39 | 0.39 | 0.39 | 0.38 |
| 15.100 | 0.38 | 0.38 | 0.37 | 0.37 | 0.36 |
| 15.267 | 0.36 | 0.36 | 0.35 | 0.35 | 0.34 |
| 15.433 | 0.34 | 0.34 | 0.33 | 0.33 | 0.33 |
| 15.600 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 15.767 | 0.30 | 0.30 | 0.30 | 0.29 | 0.29 |
| 15.933 | 0.28 | 0.28 | 0.28 | 0.27 | 0.27 |
| 16.100 | 0.27 | 0.26 | 0.26 | 0.26 | 0.26 |
| 16.267 | 0.26 | 0.26 | 0.25 | 0.25 | 0.25 |
| 16.433 | 0.25 | 0.25 | 0.25 | 0.24 | 0.24 |
| 16.600 | 0.24 | 0.24 | 0.24 | 0.24 | 0.23 |
| 16.767 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| 16.933 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 17.100 | 0.22 | 0.21 | 0.21 | 0.21 | 0.21 |
| 17.267 | 0.21 | 0.20 | 0.20 | 0.20 | 0.20 |
| 17.433 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 17.600 | 0.19 | 0.19 | 0.19 | 0.18 | 0.18 |
| 17.767 | 0.18 | 0.18 | 0.18 | 0.18 | 0.17 |
| 17.933 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 18.100 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.267 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.433 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 50 years
Label: Site Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 18.600 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.767 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.933 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.100 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.267 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.433 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.600 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.767 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.933 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 20.100 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.267 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.433 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.600 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.933 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.100 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.267 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.433 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.767 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 21.933 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.100 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.267 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.600 | 0.11 | 0.11 | 0.11 | 0.10 | 0.10 |
| 22.767 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.933 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.100 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.267 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.433 | 0.10 | 0.10 | 0.10 | 0.09 | 0.09 |
| 23.600 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.767 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.933 | 0.09 | 0.09 | 0.09 | 0.08 | 0.05 |
| 24.100 | 0.02 | 0.01 | 0.00 | 0.00 | 0.00 |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

| | |
|---|---|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 7.98 ft³/s |
| Output Increment | 0.033 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 7.96 ft³/s |

| Drainage Area | |
|---|---|
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 1.410 acres |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| Cumulative Runoff | |
|---|---|
| Cumulative Runoff Depth (Pervious) | 5.6 in |
| Runoff Volume (Pervious) | 0.663 ac-ft |

| Hydrograph Volume (Area under Hydrograph curve) | |
|---|---|
| Volume | 0.663 ac-ft |

| SCS Unit Hydrograph Parameters | |
|---|---|
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |

# Post-Development Conditions

Subsection: Unit Hydrograph Summary
Label: Site
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| SCS Unit Hydrograph Parameters | |
|---|---|
| Receding/Rising, Tr/Tp | 1.670 |
| Unit peak, qp | 15.98 ft³/s |
| Unit peak time, Tp | 0.067 hours |
| Unit receding limb, Tr | 0.267 hours |
| Total unit time, Tb | 0.333 hours |

| | |
|---|---|
| Storm Event | TypeIII 24hr (8.4 in) |
| Return Event | 100 years |
| Duration | 80.000 hours |
| Depth | 8.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 1.410 acres |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.233 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 |
| 6.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.733 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 6.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.067 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.233 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.400 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 7.567 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 7.733 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 7.900 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.067 | 0.06 | 0.06 | 0.07 | 0.07 | 0.07 |
| 8.233 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.400 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 |
| 8.567 | 0.10 | 0.10 | 0.10 | 0.11 | 0.11 |
| 8.733 | 0.11 | 0.11 | 0.12 | 0.12 | 0.12 |
| 8.900 | 0.13 | 0.13 | 0.13 | 0.13 | 0.14 |
| 9.067 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 |
| 9.233 | 0.16 | 0.16 | 0.16 | 0.17 | 0.17 |
| 9.400 | 0.17 | 0.18 | 0.18 | 0.19 | 0.19 |
| 9.567 | 0.19 | 0.20 | 0.20 | 0.20 | 0.21 |
| 9.733 | 0.21 | 0.22 | 0.22 | 0.22 | 0.23 |
| 9.900 | 0.23 | 0.24 | 0.24 | 0.25 | 0.25 |
| 10.067 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 |
| 10.233 | 0.29 | 0.29 | 0.30 | 0.31 | 0.31 |
| 10.400 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 |
| 10.567 | 0.36 | 0.37 | 0.37 | 0.38 | 0.39 |
| 10.733 | 0.40 | 0.41 | 0.41 | 0.42 | 0.43 |
| 10.900 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 |
| 11.067 | 0.49 | 0.51 | 0.53 | 0.55 | 0.58 |
| 11.233 | 0.60 | 0.63 | 0.66 | 0.68 | 0.71 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Site Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 11.400 | 0.74 | 0.76 | 0.79 | 0.82 | 0.88 |
| 11.567 | 1.02 | 1.14 | 1.28 | 1.55 | 1.79 |
| 11.733 | 1.99 | 2.30 | 2.57 | 2.81 | 3.15 |
| 11.900 | 3.46 | 4.03 | 5.41 | 6.67 | 7.34 |
| 12.067 | 7.73 | 7.96 | 7.69 | 6.43 | 5.26 |
| 12.233 | 4.64 | 4.10 | 3.74 | 3.49 | 3.12 |
| 12.400 | 2.82 | 2.59 | 2.23 | 1.93 | 1.74 |
| 12.567 | 1.51 | 1.34 | 1.24 | 1.18 | 1.13 |
| 12.733 | 1.10 | 1.06 | 1.03 | 1.01 | 0.97 |
| 12.900 | 0.94 | 0.91 | 0.87 | 0.84 | 0.82 |
| 13.067 | 0.79 | 0.77 | 0.76 | 0.75 | 0.74 |
| 13.233 | 0.73 | 0.72 | 0.72 | 0.71 | 0.70 |
| 13.400 | 0.69 | 0.68 | 0.67 | 0.67 | 0.66 |
| 13.567 | 0.65 | 0.64 | 0.64 | 0.63 | 0.62 |
| 13.733 | 0.61 | 0.60 | 0.59 | 0.59 | 0.58 |
| 13.900 | 0.57 | 0.56 | 0.55 | 0.54 | 0.54 |
| 14.067 | 0.53 | 0.52 | 0.52 | 0.51 | 0.51 |
| 14.233 | 0.51 | 0.50 | 0.50 | 0.49 | 0.49 |
| 14.400 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 14.567 | 0.47 | 0.46 | 0.46 | 0.45 | 0.45 |
| 14.733 | 0.45 | 0.44 | 0.44 | 0.43 | 0.43 |
| 14.900 | 0.43 | 0.42 | 0.42 | 0.41 | 0.41 |
| 15.067 | 0.41 | 0.40 | 0.40 | 0.39 | 0.39 |
| 15.233 | 0.39 | 0.38 | 0.38 | 0.37 | 0.37 |
| 15.400 | 0.37 | 0.36 | 0.36 | 0.35 | 0.35 |
| 15.567 | 0.34 | 0.34 | 0.34 | 0.33 | 0.33 |
| 15.733 | 0.32 | 0.32 | 0.32 | 0.31 | 0.31 |
| 15.900 | 0.30 | 0.30 | 0.30 | 0.29 | 0.29 |
| 16.067 | 0.29 | 0.28 | 0.28 | 0.28 | 0.28 |
| 16.233 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |
| 16.400 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 |
| 16.567 | 0.26 | 0.25 | 0.25 | 0.25 | 0.25 |
| 16.733 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 16.900 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 17.067 | 0.23 | 0.23 | 0.23 | 0.22 | 0.22 |
| 17.233 | 0.22 | 0.22 | 0.22 | 0.22 | 0.21 |
| 17.400 | 0.21 | 0.21 | 0.21 | 0.21 | 0.20 |
| 17.567 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 17.733 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 17.900 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.067 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 18.233 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |

# Post-Development Conditions

Subsection: Unit Hydrograph (Hydrograph Table) Return Event: 100 years
Label: Site Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 18.400 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 18.567 | 0.17 | 0.17 | 0.17 | 0.17 | 0.16 |
| 18.733 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.900 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.067 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.233 | 0.16 | 0.16 | 0.15 | 0.15 | 0.15 |
| 19.400 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.567 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.733 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 19.900 | 0.15 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.067 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.233 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.400 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.567 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 20.733 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.900 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.067 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.233 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.400 | 0.13 | 0.13 | 0.13 | 0.12 | 0.12 |
| 21.567 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.733 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.067 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.233 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 22.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.567 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.900 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.067 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 23.233 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.400 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.567 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.733 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.900 | 0.10 | 0.10 | 0.09 | 0.09 | 0.08 |
| 24.067 | 0.05 | 0.02 | 0.01 | 0.00 | 0.00 |
| 24.233 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

## Summary for Hydrograph Addition at 'POI'

| Upstream Link | Upstream Node |
|---|---|
| Outlet | Detention Pond |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Outlet | 0.261 | 12.267 | 1.81 |
| Flow (In) | POI | 0.261 | 12.267 | 1.81 |

## Summary for Hydrograph Addition at 'POI'

| Upstream Link | Upstream Node |
|---|---|
| Outlet | Detention Pond |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Outlet | 0.446 | 12.200 | 3.73 |
| Flow (In) | POI | 0.446 | 12.200 | 3.73 |

## Summary for Hydrograph Addition at 'POI'

| Upstream Link | Upstream Node |
|---|---|
| Outlet | Detention Pond |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Outlet | 0.550 | 12.167 | 5.83 |
| Flow (In) | POI | 0.550 | 12.167 | 5.83 |

## Summary for Hydrograph Addition at 'POI'

| Upstream Link | Upstream Node |
|---|---|
| Outlet | Detention Pond |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Outlet | 0.680 | 12.167 | 6.44 |
| Flow (In) | POI | 0.680 | 12.167 | 6.44 |

# Post-Development Conditions

Subsection: Addition Summary
Label: POI
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Summary for Hydrograph Addition at 'POI'

| Upstream Link | Upstream Node |
|---|---|
| Outlet | Detention Pond |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Outlet | 0.728 | 12.167 | 6.92 |
| Flow (In) | POI | 0.728 | 12.167 | 6.92 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 8.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 9.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 9.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.01 |
| 9.333 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 9.500 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 9.667 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 9.833 | 405.02 | 405.02 | 405.02 | 405.03 | 405.03 |
| 10.000 | 405.03 | 405.03 | 405.03 | 405.03 | 405.04 |
| 10.167 | 405.04 | 405.04 | 405.04 | 405.04 | 405.04 |
| 10.333 | 405.05 | 405.05 | 405.05 | 405.05 | 405.05 |
| 10.500 | 405.06 | 405.06 | 405.06 | 405.06 | 405.07 |
| 10.667 | 405.07 | 405.07 | 405.08 | 405.08 | 405.08 |
| 10.833 | 405.08 | 405.09 | 405.09 | 405.09 | 405.10 |
| 11.000 | 405.10 | 405.10 | 405.11 | 405.11 | 405.12 |
| 11.167 | 405.12 | 405.13 | 405.14 | 405.15 | 405.16 |
| 11.333 | 405.17 | 405.18 | 405.19 | 405.21 | 405.22 |
| 11.500 | 405.23 | 405.25 | 405.26 | 405.28 | 405.30 |
| 11.667 | 405.32 | 405.35 | 405.38 | 405.41 | 405.45 |
| 11.833 | 405.49 | 405.53 | 405.57 | 405.61 | 405.68 |
| 12.000 | 405.79 | 405.92 | 406.05 | 406.17 | 406.30 |
| 12.167 | 406.39 | 406.44 | 406.46 | 406.46 | 406.46 |
| 12.333 | 406.44 | 406.41 | 406.38 | 406.34 | 406.30 |
| 12.500 | 406.24 | 406.18 | 406.12 | 406.04 | 405.97 |
| 12.667 | 405.90 | 405.84 | 405.78 | 405.73 | 405.68 |
| 12.833 | 405.63 | 405.59 | 405.56 | 405.53 | 405.51 |
| 13.000 | 405.49 | 405.47 | 405.46 | 405.45 | 405.44 |
| 13.167 | 405.43 | 405.42 | 405.41 | 405.41 | 405.40 |
| 13.333 | 405.40 | 405.39 | 405.39 | 405.39 | 405.38 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.500 | 405.38 | 405.38 | 405.37 | 405.37 | 405.37 |
| 13.667 | 405.37 | 405.37 | 405.36 | 405.36 | 405.36 |
| 13.833 | 405.36 | 405.36 | 405.35 | 405.35 | 405.35 |
| 14.000 | 405.35 | 405.35 | 405.34 | 405.34 | 405.34 |
| 14.167 | 405.34 | 405.34 | 405.34 | 405.33 | 405.33 |
| 14.333 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 14.500 | 405.33 | 405.33 | 405.32 | 405.32 | 405.32 |
| 14.667 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 14.833 | 405.32 | 405.32 | 405.32 | 405.31 | 405.31 |
| 15.000 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 15.167 | 405.31 | 405.31 | 405.31 | 405.30 | 405.30 |
| 15.333 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 15.500 | 405.30 | 405.30 | 405.30 | 405.29 | 405.29 |
| 15.667 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 15.833 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 16.000 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 16.167 | 405.27 | 405.27 | 405.26 | 405.26 | 405.26 |
| 16.333 | 405.26 | 405.26 | 405.26 | 405.26 | 405.25 |
| 16.500 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 16.667 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 16.833 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 17.000 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 17.167 | 405.24 | 405.23 | 405.23 | 405.23 | 405.23 |
| 17.333 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 17.500 | 405.23 | 405.23 | 405.23 | 405.22 | 405.22 |
| 17.667 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 17.833 | 405.22 | 405.22 | 405.22 | 405.22 | 405.21 |
| 18.000 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 18.167 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 18.333 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 18.500 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 18.667 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 18.833 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 19.000 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 19.167 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 19.333 | 405.20 | 405.20 | 405.19 | 405.19 | 405.19 |
| 19.500 | 405.19 | 405.19 | 405.19 | 405.19 | 405.19 |
| 19.667 | 405.19 | 405.19 | 405.19 | 405.19 | 405.18 |
| 19.833 | 405.18 | 405.18 | 405.18 | 405.18 | 405.18 |
| 20.000 | 405.18 | 405.18 | 405.18 | 405.17 | 405.17 |
| 20.167 | 405.17 | 405.17 | 405.17 | 405.17 | 405.17 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.333 | 405.17 | 405.16 | 405.16 | 405.16 | 405.16 |
| 20.500 | 405.16 | 405.16 | 405.16 | 405.15 | 405.15 |
| 20.667 | 405.15 | 405.15 | 405.15 | 405.15 | 405.14 |
| 20.833 | 405.14 | 405.14 | 405.14 | 405.14 | 405.14 |
| 21.000 | 405.13 | 405.13 | 405.13 | 405.13 | 405.13 |
| 21.167 | 405.13 | 405.12 | 405.12 | 405.12 | 405.12 |
| 21.333 | 405.12 | 405.11 | 405.11 | 405.11 | 405.11 |
| 21.500 | 405.10 | 405.10 | 405.10 | 405.10 | 405.10 |
| 21.667 | 405.09 | 405.09 | 405.09 | 405.09 | 405.09 |
| 21.833 | 405.09 | 405.09 | 405.08 | 405.08 | 405.08 |
| 22.000 | 405.08 | 405.08 | 405.08 | 405.08 | 405.08 |
| 22.167 | 405.08 | 405.08 | 405.08 | 405.08 | 405.08 |
| 22.333 | 405.08 | 405.08 | 405.07 | 405.07 | 405.07 |
| 22.500 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 22.667 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 22.833 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 23.000 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 23.167 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 23.333 | 405.07 | 405.07 | 405.07 | 405.07 | 405.06 |
| 23.500 | 405.06 | 405.06 | 405.06 | 405.06 | 405.06 |
| 23.667 | 405.06 | 405.06 | 405.06 | 405.06 | 405.06 |
| 23.833 | 405.06 | 405.06 | 405.06 | 405.06 | 405.06 |
| 24.000 | 405.06 | 405.06 | 405.06 | 405.06 | 405.05 |
| 24.167 | 405.05 | 405.04 | 405.04 | 405.04 | 405.03 |
| 24.333 | 405.03 | 405.03 | 405.02 | 405.02 | 405.02 |
| 24.500 | 405.02 | 405.02 | 405.02 | 405.01 | 405.01 |
| 24.667 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 24.833 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 27.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 34.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 40.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 47.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 54.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 61.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 68.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 75.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 80.000 | 405.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.01 |
| 8.000 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 8.167 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 8.333 | 405.01 | 405.02 | 405.02 | 405.02 | 405.02 |
| 8.500 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 8.667 | 405.03 | 405.03 | 405.03 | 405.03 | 405.03 |
| 8.833 | 405.03 | 405.03 | 405.04 | 405.04 | 405.04 |
| 9.000 | 405.04 | 405.04 | 405.05 | 405.05 | 405.05 |
| 9.167 | 405.05 | 405.05 | 405.05 | 405.06 | 405.06 |
| 9.333 | 405.06 | 405.06 | 405.07 | 405.07 | 405.07 |
| 9.500 | 405.07 | 405.07 | 405.08 | 405.08 | 405.08 |
| 9.667 | 405.08 | 405.09 | 405.09 | 405.09 | 405.09 |
| 9.833 | 405.10 | 405.10 | 405.10 | 405.11 | 405.11 |
| 10.000 | 405.11 | 405.12 | 405.12 | 405.13 | 405.13 |
| 10.167 | 405.14 | 405.14 | 405.15 | 405.16 | 405.17 |
| 10.333 | 405.17 | 405.18 | 405.19 | 405.20 | 405.21 |
| 10.500 | 405.22 | 405.23 | 405.23 | 405.24 | 405.25 |
| 10.667 | 405.26 | 405.26 | 405.27 | 405.28 | 405.28 |
| 10.833 | 405.29 | 405.30 | 405.30 | 405.31 | 405.31 |
| 11.000 | 405.32 | 405.32 | 405.33 | 405.33 | 405.34 |
| 11.167 | 405.34 | 405.35 | 405.35 | 405.36 | 405.37 |
| 11.333 | 405.37 | 405.38 | 405.39 | 405.40 | 405.41 |
| 11.500 | 405.41 | 405.42 | 405.44 | 405.46 | 405.48 |
| 11.667 | 405.51 | 405.54 | 405.58 | 405.63 | 405.68 |
| 11.833 | 405.74 | 405.81 | 405.89 | 405.99 | 406.12 |
| 12.000 | 406.31 | 406.52 | 406.74 | 406.96 | 407.15 |
| 12.167 | 407.28 | 407.31 | 407.30 | 407.28 | 407.26 |
| 12.333 | 407.24 | 407.22 | 407.20 | 407.18 | 407.15 |
| 12.500 | 407.10 | 407.05 | 406.99 | 406.92 | 406.85 |
| 12.667 | 406.77 | 406.69 | 406.62 | 406.54 | 406.46 |
| 12.833 | 406.39 | 406.31 | 406.24 | 406.17 | 406.09 |
| 13.000 | 406.02 | 405.95 | 405.89 | 405.83 | 405.78 |
| 13.167 | 405.73 | 405.69 | 405.65 | 405.61 | 405.58 |
| 13.333 | 405.55 | 405.54 | 405.52 | 405.51 | 405.50 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.500 | 405.49 | 405.49 | 405.48 | 405.47 | 405.47 |
| 13.667 | 405.46 | 405.46 | 405.46 | 405.45 | 405.45 |
| 13.833 | 405.44 | 405.44 | 405.44 | 405.43 | 405.43 |
| 14.000 | 405.43 | 405.43 | 405.42 | 405.42 | 405.42 |
| 14.167 | 405.41 | 405.41 | 405.41 | 405.41 | 405.41 |
| 14.333 | 405.40 | 405.40 | 405.40 | 405.40 | 405.40 |
| 14.500 | 405.40 | 405.39 | 405.39 | 405.39 | 405.39 |
| 14.667 | 405.39 | 405.39 | 405.38 | 405.38 | 405.38 |
| 14.833 | 405.38 | 405.38 | 405.38 | 405.38 | 405.37 |
| 15.000 | 405.37 | 405.37 | 405.37 | 405.37 | 405.37 |
| 15.167 | 405.36 | 405.36 | 405.36 | 405.36 | 405.36 |
| 15.333 | 405.36 | 405.36 | 405.35 | 405.35 | 405.35 |
| 15.500 | 405.35 | 405.35 | 405.35 | 405.34 | 405.34 |
| 15.667 | 405.34 | 405.34 | 405.34 | 405.34 | 405.34 |
| 15.833 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 16.000 | 405.33 | 405.32 | 405.32 | 405.32 | 405.32 |
| 16.167 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 16.333 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 16.500 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 16.667 | 405.31 | 405.31 | 405.31 | 405.30 | 405.30 |
| 16.833 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 17.000 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 17.167 | 405.30 | 405.29 | 405.29 | 405.29 | 405.29 |
| 17.333 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 17.500 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 17.667 | 405.28 | 405.28 | 405.28 | 405.27 | 405.27 |
| 17.833 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 18.000 | 405.27 | 405.26 | 405.26 | 405.26 | 405.26 |
| 18.167 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 18.333 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 18.500 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 18.667 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 18.833 | 405.25 | 405.25 | 405.24 | 405.24 | 405.24 |
| 19.000 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 19.167 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 19.333 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 19.500 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 19.667 | 405.24 | 405.23 | 405.23 | 405.23 | 405.23 |
| 19.833 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 20.000 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 20.167 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.333 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 20.500 | 405.23 | 405.23 | 405.23 | 405.22 | 405.22 |
| 20.667 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 20.833 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 21.000 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 21.167 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 21.333 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 21.500 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 21.667 | 405.22 | 405.21 | 405.21 | 405.21 | 405.21 |
| 21.833 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 22.000 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 22.167 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 22.333 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 22.500 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 22.667 | 405.21 | 405.21 | 405.21 | 405.21 | 405.20 |
| 22.833 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 23.000 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 23.167 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 23.333 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 23.500 | 405.20 | 405.20 | 405.20 | 405.20 | 405.20 |
| 23.667 | 405.20 | 405.19 | 405.19 | 405.19 | 405.19 |
| 23.833 | 405.19 | 405.19 | 405.19 | 405.19 | 405.19 |
| 24.000 | 405.19 | 405.19 | 405.18 | 405.18 | 405.17 |
| 24.167 | 405.16 | 405.15 | 405.14 | 405.13 | 405.13 |
| 24.333 | 405.12 | 405.11 | 405.10 | 405.09 | 405.08 |
| 24.500 | 405.07 | 405.07 | 405.06 | 405.06 | 405.05 |
| 24.667 | 405.05 | 405.04 | 405.04 | 405.04 | 405.03 |
| 24.833 | 405.03 | 405.03 | 405.02 | 405.02 | 405.02 |
| 25.000 | 405.02 | 405.02 | 405.02 | 405.01 | 405.01 |
| 25.167 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.333 | 405.01 | 405.01 | 405.01 | 405.01 | 405.00 |
| 25.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 27.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 34.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 40.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 47.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 54.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 61.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 68.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 75.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 80.000 | 405.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 7.333 | 405.00 | 405.01 | 405.01 | 405.01 | 405.01 |
| 7.500 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 7.667 | 405.01 | 405.01 | 405.01 | 405.02 | 405.02 |
| 7.833 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 8.000 | 405.02 | 405.02 | 405.02 | 405.03 | 405.03 |
| 8.167 | 405.03 | 405.03 | 405.03 | 405.03 | 405.03 |
| 8.333 | 405.03 | 405.04 | 405.04 | 405.04 | 405.04 |
| 8.500 | 405.04 | 405.04 | 405.05 | 405.05 | 405.05 |
| 8.667 | 405.05 | 405.05 | 405.06 | 405.06 | 405.06 |
| 8.833 | 405.06 | 405.06 | 405.07 | 405.07 | 405.07 |
| 9.000 | 405.07 | 405.08 | 405.08 | 405.08 | 405.08 |
| 9.167 | 405.09 | 405.09 | 405.09 | 405.09 | 405.10 |
| 9.333 | 405.10 | 405.10 | 405.11 | 405.11 | 405.11 |
| 9.500 | 405.12 | 405.12 | 405.13 | 405.13 | 405.14 |
| 9.667 | 405.14 | 405.15 | 405.16 | 405.16 | 405.17 |
| 9.833 | 405.18 | 405.19 | 405.19 | 405.20 | 405.21 |
| 10.000 | 405.22 | 405.23 | 405.23 | 405.24 | 405.25 |
| 10.167 | 405.25 | 405.26 | 405.26 | 405.27 | 405.28 |
| 10.333 | 405.28 | 405.29 | 405.29 | 405.30 | 405.30 |
| 10.500 | 405.31 | 405.31 | 405.32 | 405.32 | 405.33 |
| 10.667 | 405.33 | 405.33 | 405.34 | 405.34 | 405.35 |
| 10.833 | 405.35 | 405.35 | 405.36 | 405.36 | 405.36 |
| 11.000 | 405.37 | 405.37 | 405.38 | 405.38 | 405.39 |
| 11.167 | 405.39 | 405.40 | 405.40 | 405.41 | 405.42 |
| 11.333 | 405.43 | 405.44 | 405.45 | 405.46 | 405.47 |
| 11.500 | 405.48 | 405.49 | 405.51 | 405.53 | 405.55 |
| 11.667 | 405.58 | 405.62 | 405.68 | 405.74 | 405.82 |
| 11.833 | 405.90 | 405.99 | 406.09 | 406.21 | 406.38 |
| 12.000 | 406.61 | 406.87 | 407.13 | 407.33 | 407.43 |
| 12.167 | 407.44 | 407.41 | 407.37 | 407.33 | 407.31 |
| 12.333 | 407.28 | 407.26 | 407.24 | 407.22 | 407.20 |
| 12.500 | 407.17 | 407.13 | 407.08 | 407.02 | 406.96 |
| 12.667 | 406.89 | 406.83 | 406.76 | 406.69 | 406.62 |
| 12.833 | 406.55 | 406.48 | 406.41 | 406.34 | 406.27 |
| 13.000 | 406.20 | 406.14 | 406.07 | 406.00 | 405.94 |
| 13.167 | 405.88 | 405.83 | 405.79 | 405.75 | 405.71 |
| 13.333 | 405.68 | 405.64 | 405.62 | 405.59 | 405.57 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.500 | 405.55 | 405.54 | 405.53 | 405.52 | 405.51 |
| 13.667 | 405.51 | 405.50 | 405.50 | 405.50 | 405.49 |
| 13.833 | 405.49 | 405.48 | 405.48 | 405.48 | 405.47 |
| 14.000 | 405.47 | 405.47 | 405.46 | 405.46 | 405.46 |
| 14.167 | 405.45 | 405.45 | 405.45 | 405.44 | 405.44 |
| 14.333 | 405.44 | 405.44 | 405.44 | 405.43 | 405.43 |
| 14.500 | 405.43 | 405.43 | 405.43 | 405.42 | 405.42 |
| 14.667 | 405.42 | 405.42 | 405.42 | 405.42 | 405.41 |
| 14.833 | 405.41 | 405.41 | 405.41 | 405.41 | 405.41 |
| 15.000 | 405.40 | 405.40 | 405.40 | 405.40 | 405.40 |
| 15.167 | 405.40 | 405.39 | 405.39 | 405.39 | 405.39 |
| 15.333 | 405.39 | 405.38 | 405.38 | 405.38 | 405.38 |
| 15.500 | 405.38 | 405.38 | 405.37 | 405.37 | 405.37 |
| 15.667 | 405.37 | 405.37 | 405.36 | 405.36 | 405.36 |
| 15.833 | 405.36 | 405.36 | 405.35 | 405.35 | 405.35 |
| 16.000 | 405.35 | 405.35 | 405.35 | 405.34 | 405.34 |
| 16.167 | 405.34 | 405.34 | 405.34 | 405.34 | 405.34 |
| 16.333 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 16.500 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 16.667 | 405.33 | 405.32 | 405.32 | 405.32 | 405.32 |
| 16.833 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 17.000 | 405.32 | 405.32 | 405.32 | 405.31 | 405.31 |
| 17.167 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 17.333 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 17.500 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 17.667 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 17.833 | 405.30 | 405.29 | 405.29 | 405.29 | 405.29 |
| 18.000 | 405.29 | 405.29 | 405.29 | 405.29 | 405.28 |
| 18.167 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 18.333 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 18.500 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 18.667 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 18.833 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 19.000 | 405.27 | 405.27 | 405.27 | 405.26 | 405.26 |
| 19.167 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 19.333 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 19.500 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 19.667 | 405.26 | 405.26 | 405.26 | 405.25 | 405.25 |
| 19.833 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 20.000 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 20.167 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.333 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 20.500 | 405.25 | 405.24 | 405.24 | 405.24 | 405.24 |
| 20.667 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 20.833 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 21.000 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 21.167 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 21.333 | 405.24 | 405.24 | 405.24 | 405.24 | 405.23 |
| 21.500 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 21.667 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 21.833 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 22.000 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 22.167 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 22.333 | 405.23 | 405.22 | 405.22 | 405.22 | 405.22 |
| 22.500 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 22.667 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 22.833 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 23.000 | 405.22 | 405.22 | 405.22 | 405.22 | 405.22 |
| 23.167 | 405.22 | 405.22 | 405.22 | 405.22 | 405.21 |
| 23.333 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 23.500 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 23.667 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 23.833 | 405.21 | 405.21 | 405.21 | 405.21 | 405.21 |
| 24.000 | 405.21 | 405.21 | 405.20 | 405.20 | 405.19 |
| 24.167 | 405.18 | 405.17 | 405.17 | 405.16 | 405.15 |
| 24.333 | 405.14 | 405.13 | 405.12 | 405.11 | 405.10 |
| 24.500 | 405.09 | 405.09 | 405.08 | 405.07 | 405.06 |
| 24.667 | 405.06 | 405.05 | 405.05 | 405.04 | 405.04 |
| 24.833 | 405.04 | 405.03 | 405.03 | 405.03 | 405.03 |
| 25.000 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 25.167 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.333 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.500 | 405.01 | 405.01 | 405.00 | 405.00 | 405.00 |
| 25.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 27.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 34.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 40.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 47.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 54.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 61.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 68.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 75.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 80.000 | 405.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.667 | 405.00 | 405.00 | 405.01 | 405.01 | 405.01 |
| 6.833 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 7.000 | 405.01 | 405.01 | 405.01 | 405.01 | 405.02 |
| 7.167 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 7.333 | 405.02 | 405.02 | 405.02 | 405.03 | 405.03 |
| 7.500 | 405.03 | 405.03 | 405.03 | 405.03 | 405.03 |
| 7.667 | 405.03 | 405.03 | 405.04 | 405.04 | 405.04 |
| 7.833 | 405.04 | 405.04 | 405.04 | 405.04 | 405.05 |
| 8.000 | 405.05 | 405.05 | 405.05 | 405.05 | 405.05 |
| 8.167 | 405.06 | 405.06 | 405.06 | 405.06 | 405.06 |
| 8.333 | 405.06 | 405.07 | 405.07 | 405.07 | 405.07 |
| 8.500 | 405.08 | 405.08 | 405.08 | 405.08 | 405.09 |
| 8.667 | 405.09 | 405.09 | 405.09 | 405.10 | 405.10 |
| 8.833 | 405.10 | 405.11 | 405.11 | 405.11 | 405.12 |
| 9.000 | 405.12 | 405.13 | 405.13 | 405.14 | 405.15 |
| 9.167 | 405.15 | 405.16 | 405.17 | 405.17 | 405.18 |
| 9.333 | 405.19 | 405.20 | 405.21 | 405.22 | 405.22 |
| 9.500 | 405.23 | 405.24 | 405.24 | 405.25 | 405.26 |
| 9.667 | 405.26 | 405.27 | 405.27 | 405.28 | 405.28 |
| 9.833 | 405.29 | 405.29 | 405.30 | 405.30 | 405.31 |
| 10.000 | 405.31 | 405.31 | 405.32 | 405.32 | 405.32 |
| 10.167 | 405.33 | 405.33 | 405.33 | 405.34 | 405.34 |
| 10.333 | 405.34 | 405.35 | 405.35 | 405.35 | 405.36 |
| 10.500 | 405.36 | 405.37 | 405.37 | 405.37 | 405.38 |
| 10.667 | 405.38 | 405.38 | 405.39 | 405.39 | 405.40 |
| 10.833 | 405.40 | 405.41 | 405.41 | 405.41 | 405.42 |
| 11.000 | 405.42 | 405.43 | 405.43 | 405.44 | 405.44 |
| 11.167 | 405.45 | 405.46 | 405.47 | 405.48 | 405.49 |
| 11.333 | 405.50 | 405.51 | 405.52 | 405.53 | 405.54 |
| 11.500 | 405.55 | 405.56 | 405.58 | 405.60 | 405.63 |
| 11.667 | 405.67 | 405.74 | 405.81 | 405.90 | 405.99 |
| 11.833 | 406.09 | 406.21 | 406.34 | 406.50 | 406.70 |
| 12.000 | 406.97 | 407.25 | 407.44 | 407.56 | 407.67 |
| 12.167 | 407.72 | 407.70 | 407.65 | 407.57 | 407.46 |
| 12.333 | 407.37 | 407.32 | 407.29 | 407.26 | 407.24 |
| 12.500 | 407.21 | 407.19 | 407.15 | 407.11 | 407.06 |
| 12.667 | 407.00 | 406.94 | 406.88 | 406.82 | 406.76 |
| 12.833 | 406.70 | 406.64 | 406.58 | 406.51 | 406.45 |
| 13.000 | 406.38 | 406.32 | 406.26 | 406.20 | 406.14 |
| 13.167 | 406.08 | 406.02 | 405.96 | 405.91 | 405.87 |
| 13.333 | 405.83 | 405.79 | 405.76 | 405.73 | 405.70 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.500 | 405.67 | 405.65 | 405.63 | 405.61 | 405.59 |
| 13.667 | 405.57 | 405.56 | 405.55 | 405.54 | 405.54 |
| 13.833 | 405.53 | 405.53 | 405.52 | 405.52 | 405.51 |
| 14.000 | 405.51 | 405.51 | 405.50 | 405.50 | 405.50 |
| 14.167 | 405.50 | 405.49 | 405.49 | 405.49 | 405.49 |
| 14.333 | 405.48 | 405.48 | 405.48 | 405.48 | 405.47 |
| 14.500 | 405.47 | 405.47 | 405.47 | 405.47 | 405.46 |
| 14.667 | 405.46 | 405.46 | 405.46 | 405.46 | 405.45 |
| 14.833 | 405.45 | 405.45 | 405.45 | 405.45 | 405.44 |
| 15.000 | 405.44 | 405.44 | 405.44 | 405.43 | 405.43 |
| 15.167 | 405.43 | 405.43 | 405.43 | 405.42 | 405.42 |
| 15.333 | 405.42 | 405.42 | 405.42 | 405.41 | 405.41 |
| 15.500 | 405.41 | 405.41 | 405.41 | 405.40 | 405.40 |
| 15.667 | 405.40 | 405.40 | 405.39 | 405.39 | 405.39 |
| 15.833 | 405.39 | 405.39 | 405.38 | 405.38 | 405.38 |
| 16.000 | 405.38 | 405.37 | 405.37 | 405.37 | 405.37 |
| 16.167 | 405.37 | 405.37 | 405.36 | 405.36 | 405.36 |
| 16.333 | 405.36 | 405.36 | 405.36 | 405.36 | 405.35 |
| 16.500 | 405.35 | 405.35 | 405.35 | 405.35 | 405.35 |
| 16.667 | 405.35 | 405.35 | 405.35 | 405.35 | 405.34 |
| 16.833 | 405.34 | 405.34 | 405.34 | 405.34 | 405.34 |
| 17.000 | 405.34 | 405.34 | 405.34 | 405.34 | 405.33 |
| 17.167 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 17.333 | 405.33 | 405.33 | 405.33 | 405.33 | 405.32 |
| 17.500 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 17.667 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 17.833 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 18.000 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 18.167 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 18.333 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 18.500 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 18.667 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 18.833 | 405.30 | 405.30 | 405.29 | 405.29 | 405.29 |
| 19.000 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 19.167 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 19.333 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 19.500 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 19.667 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 19.833 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 20.000 | 405.28 | 405.28 | 405.28 | 405.27 | 405.27 |
| 20.167 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.333 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 20.500 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 20.667 | 405.27 | 405.27 | 405.27 | 405.27 | 405.26 |
| 20.833 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.000 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.167 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.333 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.500 | 405.26 | 405.26 | 405.26 | 405.25 | 405.25 |
| 21.667 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 21.833 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.000 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.167 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.333 | 405.25 | 405.24 | 405.24 | 405.24 | 405.24 |
| 22.500 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 22.667 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 22.833 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 23.000 | 405.24 | 405.24 | 405.24 | 405.24 | 405.23 |
| 23.167 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 23.333 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 23.500 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 23.667 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 23.833 | 405.23 | 405.23 | 405.23 | 405.22 | 405.22 |
| 24.000 | 405.22 | 405.22 | 405.22 | 405.21 | 405.21 |
| 24.167 | 405.20 | 405.19 | 405.18 | 405.17 | 405.16 |
| 24.333 | 405.15 | 405.14 | 405.14 | 405.13 | 405.12 |
| 24.500 | 405.11 | 405.10 | 405.09 | 405.08 | 405.08 |
| 24.667 | 405.07 | 405.06 | 405.06 | 405.05 | 405.05 |
| 24.833 | 405.04 | 405.04 | 405.04 | 405.03 | 405.03 |
| 25.000 | 405.03 | 405.02 | 405.02 | 405.02 | 405.02 |
| 25.167 | 405.02 | 405.02 | 405.01 | 405.01 | 405.01 |
| 25.333 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.500 | 405.01 | 405.01 | 405.01 | 405.01 | 405.00 |
| 25.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 27.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 34.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 40.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 47.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 54.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 61.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 68.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 75.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 80.000 | 405.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 0.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 0.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 1.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 2.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 3.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 4.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 5.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 6.500 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 6.667 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 6.833 | 405.01 | 405.01 | 405.01 | 405.02 | 405.02 |
| 7.000 | 405.02 | 405.02 | 405.02 | 405.02 | 405.02 |
| 7.167 | 405.02 | 405.02 | 405.03 | 405.03 | 405.03 |
| 7.333 | 405.03 | 405.03 | 405.03 | 405.03 | 405.03 |
| 7.500 | 405.04 | 405.04 | 405.04 | 405.04 | 405.04 |
| 7.667 | 405.04 | 405.04 | 405.05 | 405.05 | 405.05 |
| 7.833 | 405.05 | 405.05 | 405.05 | 405.05 | 405.06 |
| 8.000 | 405.06 | 405.06 | 405.06 | 405.06 | 405.06 |
| 8.167 | 405.07 | 405.07 | 405.07 | 405.07 | 405.07 |
| 8.333 | 405.08 | 405.08 | 405.08 | 405.08 | 405.09 |
| 8.500 | 405.09 | 405.09 | 405.09 | 405.10 | 405.10 |
| 8.667 | 405.10 | 405.11 | 405.11 | 405.11 | 405.12 |
| 8.833 | 405.12 | 405.13 | 405.13 | 405.14 | 405.15 |
| 9.000 | 405.15 | 405.16 | 405.17 | 405.18 | 405.18 |
| 9.167 | 405.19 | 405.20 | 405.21 | 405.22 | 405.22 |
| 9.333 | 405.23 | 405.24 | 405.25 | 405.25 | 405.26 |
| 9.500 | 405.26 | 405.27 | 405.27 | 405.28 | 405.28 |
| 9.667 | 405.29 | 405.30 | 405.30 | 405.30 | 405.31 |
| 9.833 | 405.31 | 405.32 | 405.32 | 405.32 | 405.33 |
| 10.000 | 405.33 | 405.33 | 405.33 | 405.34 | 405.34 |
| 10.167 | 405.34 | 405.35 | 405.35 | 405.35 | 405.36 |
| 10.333 | 405.36 | 405.36 | 405.37 | 405.37 | 405.37 |
| 10.500 | 405.38 | 405.38 | 405.39 | 405.39 | 405.39 |
| 10.667 | 405.40 | 405.40 | 405.41 | 405.41 | 405.42 |
| 10.833 | 405.42 | 405.42 | 405.43 | 405.43 | 405.44 |
| 11.000 | 405.44 | 405.45 | 405.45 | 405.46 | 405.46 |
| 11.167 | 405.47 | 405.48 | 405.49 | 405.50 | 405.51 |
| 11.333 | 405.52 | 405.53 | 405.54 | 405.55 | 405.56 |
| 11.500 | 405.57 | 405.58 | 405.60 | 405.63 | 405.66 |
| 11.667 | 405.71 | 405.78 | 405.86 | 405.95 | 406.06 |
| 11.833 | 406.17 | 406.30 | 406.44 | 406.61 | 406.83 |
| 12.000 | 407.11 | 407.37 | 407.52 | 407.64 | 407.76 |
| 12.167 | 407.82 | 407.80 | 407.74 | 407.66 | 407.57 |
| 12.333 | 407.46 | 407.36 | 407.31 | 407.28 | 407.25 |
| 12.500 | 407.23 | 407.20 | 407.17 | 407.13 | 407.08 |
| 12.667 | 407.03 | 406.98 | 406.92 | 406.87 | 406.81 |
| 12.833 | 406.75 | 406.69 | 406.63 | 406.57 | 406.51 |
| 13.000 | 406.45 | 406.39 | 406.32 | 406.27 | 406.21 |
| 13.167 | 406.15 | 406.09 | 406.03 | 405.98 | 405.93 |
| 13.333 | 405.89 | 405.85 | 405.81 | 405.78 | 405.75 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 13.500 | 405.72 | 405.70 | 405.67 | 405.65 | 405.63 |
| 13.667 | 405.61 | 405.59 | 405.58 | 405.57 | 405.56 |
| 13.833 | 405.55 | 405.54 | 405.54 | 405.53 | 405.53 |
| 14.000 | 405.52 | 405.52 | 405.52 | 405.51 | 405.51 |
| 14.167 | 405.51 | 405.50 | 405.50 | 405.50 | 405.50 |
| 14.333 | 405.50 | 405.50 | 405.49 | 405.49 | 405.49 |
| 14.500 | 405.49 | 405.48 | 405.48 | 405.48 | 405.48 |
| 14.667 | 405.48 | 405.47 | 405.47 | 405.47 | 405.47 |
| 14.833 | 405.47 | 405.46 | 405.46 | 405.46 | 405.46 |
| 15.000 | 405.45 | 405.45 | 405.45 | 405.45 | 405.45 |
| 15.167 | 405.44 | 405.44 | 405.44 | 405.44 | 405.43 |
| 15.333 | 405.43 | 405.43 | 405.43 | 405.43 | 405.42 |
| 15.500 | 405.42 | 405.42 | 405.42 | 405.41 | 405.41 |
| 15.667 | 405.41 | 405.41 | 405.41 | 405.40 | 405.40 |
| 15.833 | 405.40 | 405.40 | 405.39 | 405.39 | 405.39 |
| 16.000 | 405.39 | 405.38 | 405.38 | 405.38 | 405.38 |
| 16.167 | 405.38 | 405.37 | 405.37 | 405.37 | 405.37 |
| 16.333 | 405.37 | 405.37 | 405.37 | 405.36 | 405.36 |
| 16.500 | 405.36 | 405.36 | 405.36 | 405.36 | 405.36 |
| 16.667 | 405.36 | 405.36 | 405.35 | 405.35 | 405.35 |
| 16.833 | 405.35 | 405.35 | 405.35 | 405.35 | 405.35 |
| 17.000 | 405.35 | 405.35 | 405.34 | 405.34 | 405.34 |
| 17.167 | 405.34 | 405.34 | 405.34 | 405.34 | 405.34 |
| 17.333 | 405.34 | 405.33 | 405.33 | 405.33 | 405.33 |
| 17.500 | 405.33 | 405.33 | 405.33 | 405.33 | 405.33 |
| 17.667 | 405.33 | 405.32 | 405.32 | 405.32 | 405.32 |
| 17.833 | 405.32 | 405.32 | 405.32 | 405.32 | 405.32 |
| 18.000 | 405.32 | 405.31 | 405.31 | 405.31 | 405.31 |
| 18.167 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 18.333 | 405.31 | 405.31 | 405.31 | 405.31 | 405.31 |
| 18.500 | 405.31 | 405.31 | 405.30 | 405.30 | 405.30 |
| 18.667 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 18.833 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 19.000 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 19.167 | 405.30 | 405.30 | 405.30 | 405.30 | 405.30 |
| 19.333 | 405.30 | 405.30 | 405.30 | 405.30 | 405.29 |
| 19.500 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 19.667 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 19.833 | 405.29 | 405.29 | 405.29 | 405.29 | 405.29 |
| 20.000 | 405.29 | 405.28 | 405.28 | 405.28 | 405.28 |
| 20.167 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 20.333 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 20.500 | 405.28 | 405.28 | 405.28 | 405.28 | 405.28 |
| 20.667 | 405.28 | 405.27 | 405.27 | 405.27 | 405.27 |
| 20.833 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 21.000 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 21.167 | 405.27 | 405.27 | 405.27 | 405.27 | 405.27 |
| 21.333 | 405.27 | 405.27 | 405.27 | 405.26 | 405.26 |
| 21.500 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.667 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 21.833 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 22.000 | 405.26 | 405.26 | 405.26 | 405.26 | 405.26 |
| 22.167 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.333 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.500 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.667 | 405.25 | 405.25 | 405.25 | 405.25 | 405.25 |
| 22.833 | 405.25 | 405.25 | 405.24 | 405.24 | 405.24 |
| 23.000 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 23.167 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 23.333 | 405.24 | 405.24 | 405.24 | 405.24 | 405.24 |
| 23.500 | 405.24 | 405.24 | 405.24 | 405.24 | 405.23 |
| 23.667 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 23.833 | 405.23 | 405.23 | 405.23 | 405.23 | 405.23 |
| 24.000 | 405.23 | 405.23 | 405.23 | 405.22 | 405.21 |
| 24.167 | 405.20 | 405.19 | 405.18 | 405.18 | 405.17 |
| 24.333 | 405.16 | 405.15 | 405.14 | 405.13 | 405.12 |
| 24.500 | 405.11 | 405.10 | 405.10 | 405.09 | 405.08 |
| 24.667 | 405.07 | 405.07 | 405.06 | 405.05 | 405.05 |
| 24.833 | 405.05 | 405.04 | 405.04 | 405.03 | 405.03 |
| 25.000 | 405.03 | 405.03 | 405.02 | 405.02 | 405.02 |
| 25.167 | 405.02 | 405.02 | 405.01 | 405.01 | 405.01 |
| 25.333 | 405.01 | 405.01 | 405.01 | 405.01 | 405.01 |
| 25.500 | 405.01 | 405.01 | 405.01 | 405.01 | 405.00 |
| 25.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 25.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 26.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 27.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 27.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 28.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 29.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 30.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 31.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 32.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 33.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 34.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 34.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 35.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 36.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 37.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 38.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 39.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 40.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 40.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 41.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 42.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 43.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 44.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 45.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 46.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 47.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 47.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 48.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 49.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 50.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 51.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 52.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 53.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 54.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 54.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 55.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 56.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 57.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 58.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 59.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 60.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 61.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 61.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 62.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 63.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 64.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 65.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 66.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 67.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 68.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 68.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 69.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 70.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 71.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 72.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 73.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 74.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |

# Post-Development Conditions

Subsection: Time vs. Elevation
Label: Detention Pond (OUT)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Time vs. Elevation (ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---|---|---|---|---|---|
| 75.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 75.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 76.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 77.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 78.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.000 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.167 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.333 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.500 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.667 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 79.833 | 405.00 | 405.00 | 405.00 | 405.00 | 405.00 |
| 80.000 | 405.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 6.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 10.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 10.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 10.333 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 10.500 | 0.001 | 0.001 | 0.001 | 0.001 | 0.002 |
| 10.667 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 10.833 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 11.000 | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 |
| 11.167 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 |
| 11.333 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 |
| 11.500 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 |
| 11.667 | 0.008 | 0.009 | 0.009 | 0.010 | 0.011 |
| 11.833 | 0.012 | 0.013 | 0.015 | 0.016 | 0.018 |
| 12.000 | 0.021 | 0.025 | 0.029 | 0.034 | 0.038 |
| 12.167 | 0.041 | 0.043 | 0.044 | 0.044 | 0.044 |
| 12.333 | 0.043 | 0.042 | 0.041 | 0.040 | 0.038 |
| 12.500 | 0.036 | 0.034 | 0.032 | 0.029 | 0.027 |
| 12.667 | 0.025 | 0.023 | 0.021 | 0.019 | 0.018 |
| 12.833 | 0.016 | 0.015 | 0.014 | 0.013 | 0.013 |
| 13.000 | 0.012 | 0.012 | 0.012 | 0.011 | 0.011 |
| 13.167 | 0.011 | 0.010 | 0.010 | 0.010 | 0.010 |
| 13.333 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 13.500 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 13.667 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 13.833 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 14.000 | 0.009 | 0.009 | 0.008 | 0.008 | 0.008 |
| 14.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 14.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 14.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 14.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 14.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 15.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 15.167 | 0.008 | 0.008 | 0.007 | 0.007 | 0.007 |
| 15.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 15.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 15.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 15.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 16.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 16.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 16.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 16.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 16.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 16.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 17.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 17.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 17.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.005 |
| 17.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 17.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 17.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 18.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 19.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 19.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 19.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 19.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 19.667 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 |
| 19.833 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 20.000 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 20.167 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 20.333 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 20.500 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 20.667 | 0.004 | 0.004 | 0.004 | 0.003 | 0.003 |
| 20.833 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 21.000 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 21.167 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 21.333 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 21.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 21.667 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 21.833 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.000 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.167 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.333 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.667 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 22.833 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 23.000 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 23.167 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 23.333 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 23.500 | 0.002 | 0.001 | 0.001 | 0.001 | 0.001 |
| 23.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 23.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.333 | 0.001 | 0.001 | 0.001 | 0.001 | 0.000 |
| 24.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 24.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 24.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 27.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 34.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 40.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 47.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 54.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 61.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 68.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 75.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80.000 | 0.000 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 6.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8.500 | 0.000 | 0.000 | 0.001 | 0.001 | 0.001 |
| 8.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 9.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 9.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 9.333 | 0.001 | 0.001 | 0.002 | 0.002 | 0.002 |
| 9.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 9.667 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 9.833 | 0.002 | 0.002 | 0.002 | 0.003 | 0.003 |
| 10.000 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 10.167 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 |
| 10.333 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 |
| 10.500 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 |
| 10.667 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 |
| 10.833 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 |
| 11.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 11.167 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 |
| 11.333 | 0.009 | 0.009 | 0.010 | 0.010 | 0.010 |
| 11.500 | 0.010 | 0.011 | 0.011 | 0.011 | 0.012 |
| 11.667 | 0.013 | 0.014 | 0.015 | 0.016 | 0.018 |
| 11.833 | 0.020 | 0.022 | 0.024 | 0.027 | 0.032 |
| 12.000 | 0.038 | 0.046 | 0.055 | 0.064 | 0.073 |
| 12.167 | 0.079 | 0.080 | 0.080 | 0.079 | 0.078 |
| 12.333 | 0.077 | 0.076 | 0.075 | 0.074 | 0.072 |
| 12.500 | 0.070 | 0.068 | 0.065 | 0.062 | 0.059 |
| 12.667 | 0.056 | 0.053 | 0.050 | 0.047 | 0.044 |
| 12.833 | 0.041 | 0.038 | 0.036 | 0.033 | 0.031 |
| 13.000 | 0.028 | 0.026 | 0.024 | 0.022 | 0.021 |
| 13.167 | 0.019 | 0.018 | 0.017 | 0.016 | 0.015 |
| 13.333 | 0.014 | 0.014 | 0.013 | 0.013 | 0.013 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 13.500 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 13.667 | 0.012 | 0.012 | 0.011 | 0.011 | 0.011 |
| 13.833 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 14.000 | 0.011 | 0.011 | 0.011 | 0.010 | 0.010 |
| 14.167 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 14.333 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 14.500 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 14.667 | 0.010 | 0.010 | 0.010 | 0.010 | 0.009 |
| 14.833 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.167 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.333 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.500 | 0.009 | 0.009 | 0.009 | 0.008 | 0.008 |
| 15.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 15.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.667 | 0.008 | 0.007 | 0.007 | 0.007 | 0.007 |
| 16.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.833 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 |
| 18.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 18.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 18.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 18.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 18.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 18.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.005 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 20.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 20.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 20.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 20.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 21.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.004 |
| 24.000 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 24.167 | 0.004 | 0.004 | 0.003 | 0.003 | 0.003 |
| 24.333 | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 |
| 24.500 | 0.002 | 0.002 | 0.001 | 0.001 | 0.001 |
| 24.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.000 |
| 25.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 27.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 34.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 40.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 47.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 54.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 61.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 68.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 75.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80.000 | 0.000 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 6.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 |
| 8.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.333 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.500 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.833 | 0.001 | 0.001 | 0.002 | 0.002 | 0.002 |
| 9.000 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 9.167 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 9.333 | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 |
| 9.500 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 9.667 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 |
| 9.833 | 0.004 | 0.004 | 0.005 | 0.005 | 0.005 |
| 10.000 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 |
| 10.167 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 |
| 10.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 10.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 10.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.009 |
| 10.833 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 11.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.010 |
| 11.167 | 0.010 | 0.010 | 0.010 | 0.010 | 0.011 |
| 11.333 | 0.011 | 0.011 | 0.011 | 0.012 | 0.012 |
| 11.500 | 0.012 | 0.012 | 0.013 | 0.013 | 0.014 |
| 11.667 | 0.015 | 0.016 | 0.018 | 0.020 | 0.022 |
| 11.833 | 0.025 | 0.027 | 0.031 | 0.035 | 0.041 |
| 12.000 | 0.050 | 0.060 | 0.072 | 0.081 | 0.086 |
| 12.167 | 0.086 | 0.085 | 0.083 | 0.081 | 0.080 |
| 12.333 | 0.079 | 0.078 | 0.077 | 0.076 | 0.075 |
| 12.500 | 0.073 | 0.072 | 0.069 | 0.067 | 0.064 |
| 12.667 | 0.061 | 0.058 | 0.056 | 0.053 | 0.050 |
| 12.833 | 0.047 | 0.045 | 0.042 | 0.039 | 0.037 |
| 13.000 | 0.035 | 0.032 | 0.030 | 0.028 | 0.026 |
| 13.167 | 0.024 | 0.022 | 0.021 | 0.020 | 0.019 |
| 13.333 | 0.018 | 0.017 | 0.016 | 0.015 | 0.015 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 13.500 | 0.014 | 0.014 | 0.013 | 0.013 | 0.013 |
| 13.667 | 0.013 | 0.013 | 0.013 | 0.013 | 0.012 |
| 13.833 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.000 | 0.012 | 0.012 | 0.012 | 0.012 | 0.011 |
| 14.167 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 14.333 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 14.500 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 14.667 | 0.011 | 0.010 | 0.010 | 0.010 | 0.010 |
| 14.833 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.167 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.333 | 0.010 | 0.010 | 0.009 | 0.009 | 0.009 |
| 15.500 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.667 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 15.833 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.000 | 0.009 | 0.009 | 0.009 | 0.008 | 0.008 |
| 16.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 16.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.007 |
| 17.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 17.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.833 | 0.007 | 0.007 | 0.006 | 0.006 | 0.006 |
| 19.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 19.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 20.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.000 | 0.006 | 0.006 | 0.006 | 0.005 | 0.005 |
| 22.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 22.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.500 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.667 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 24.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 24.167 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 24.333 | 0.003 | 0.003 | 0.003 | 0.003 | 0.002 |
| 24.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 24.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 25.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 27.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 34.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 40.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 47.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 54.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 61.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 68.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 75.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80.000 | 0.000 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 6.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.333 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.500 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.333 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.667 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.833 | 0.002 | 0.003 | 0.003 | 0.003 | 0.003 |
| 9.000 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 9.167 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 9.333 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 9.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 9.667 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 |
| 9.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 |
| 10.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 10.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 10.333 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 |
| 10.500 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 10.667 | 0.009 | 0.010 | 0.010 | 0.010 | 0.010 |
| 10.833 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 11.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 11.167 | 0.011 | 0.012 | 0.012 | 0.012 | 0.012 |
| 11.333 | 0.013 | 0.013 | 0.013 | 0.013 | 0.014 |
| 11.500 | 0.014 | 0.014 | 0.015 | 0.015 | 0.016 |
| 11.667 | 0.018 | 0.019 | 0.022 | 0.024 | 0.027 |
| 11.833 | 0.031 | 0.035 | 0.040 | 0.045 | 0.053 |
| 12.000 | 0.065 | 0.077 | 0.087 | 0.092 | 0.098 |
| 12.167 | 0.101 | 0.100 | 0.097 | 0.093 | 0.087 |
| 12.333 | 0.083 | 0.081 | 0.079 | 0.078 | 0.077 |
| 12.500 | 0.075 | 0.074 | 0.073 | 0.071 | 0.068 |
| 12.667 | 0.066 | 0.063 | 0.061 | 0.058 | 0.056 |
| 12.833 | 0.053 | 0.051 | 0.048 | 0.046 | 0.043 |
| 13.000 | 0.041 | 0.039 | 0.037 | 0.035 | 0.032 |
| 13.167 | 0.030 | 0.028 | 0.027 | 0.025 | 0.024 |
| 13.333 | 0.022 | 0.021 | 0.020 | 0.019 | 0.018 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 13.500 | 0.018 | 0.017 | 0.016 | 0.016 | 0.015 |
| 13.667 | 0.015 | 0.014 | 0.014 | 0.014 | 0.014 |
| 13.833 | 0.014 | 0.013 | 0.013 | 0.013 | 0.013 |
| 14.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 14.167 | 0.013 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.333 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.500 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.667 | 0.012 | 0.012 | 0.012 | 0.011 | 0.011 |
| 14.833 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.167 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.333 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.500 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.667 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.833 | 0.010 | 0.010 | 0.010 | 0.009 | 0.009 |
| 16.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.167 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.333 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.500 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.667 | 0.009 | 0.009 | 0.009 | 0.009 | 0.008 |
| 16.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 18.000 | 0.008 | 0.008 | 0.008 | 0.007 | 0.007 |
| 18.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 20.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.500 | 0.007 | 0.007 | 0.007 | 0.006 | 0.006 |
| 20.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 20.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.667 | 0.006 | 0.005 | 0.005 | 0.005 | 0.005 |
| 23.833 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 24.000 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 24.167 | 0.005 | 0.005 | 0.004 | 0.004 | 0.004 |
| 24.333 | 0.004 | 0.003 | 0.003 | 0.003 | 0.003 |
| 24.500 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 |
| 24.667 | 0.002 | 0.001 | 0.001 | 0.001 | 0.001 |
| 24.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 25.000 | 0.001 | 0.001 | 0.001 | 0.000 | 0.000 |
| 25.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 27.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 34.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 40.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 47.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 54.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

## Time vs. Volume (ac-ft)

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 61.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 68.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 75.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80.000 | 0.000 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 0.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 6.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 |
| 7.167 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.333 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.500 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.667 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 7.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 8.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.002 |
| 8.167 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.333 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.500 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 8.667 | 0.002 | 0.003 | 0.003 | 0.003 | 0.003 |
| 8.833 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 |
| 9.000 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 9.167 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 |
| 9.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 9.500 | 0.006 | 0.007 | 0.007 | 0.007 | 0.007 |
| 9.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.008 |
| 9.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 10.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 10.167 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 |
| 10.333 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 10.500 | 0.009 | 0.009 | 0.010 | 0.010 | 0.010 |
| 10.667 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 10.833 | 0.010 | 0.011 | 0.011 | 0.011 | 0.011 |
| 11.000 | 0.011 | 0.011 | 0.011 | 0.012 | 0.012 |
| 11.167 | 0.012 | 0.012 | 0.012 | 0.013 | 0.013 |
| 11.333 | 0.013 | 0.014 | 0.014 | 0.014 | 0.014 |
| 11.500 | 0.015 | 0.015 | 0.015 | 0.016 | 0.017 |
| 11.667 | 0.019 | 0.021 | 0.023 | 0.026 | 0.030 |
| 11.833 | 0.033 | 0.038 | 0.043 | 0.049 | 0.058 |
| 12.000 | 0.071 | 0.083 | 0.090 | 0.097 | 0.103 |
| 12.167 | 0.106 | 0.105 | 0.101 | 0.097 | 0.093 |
| 12.333 | 0.087 | 0.083 | 0.080 | 0.079 | 0.077 |
| 12.500 | 0.076 | 0.075 | 0.074 | 0.072 | 0.070 |
| 12.667 | 0.067 | 0.065 | 0.062 | 0.060 | 0.058 |
| 12.833 | 0.055 | 0.053 | 0.051 | 0.048 | 0.046 |
| 13.000 | 0.043 | 0.041 | 0.039 | 0.037 | 0.035 |
| 13.167 | 0.033 | 0.031 | 0.029 | 0.027 | 0.026 |
| 13.333 | 0.024 | 0.023 | 0.022 | 0.021 | 0.020 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 13.500 | 0.019 | 0.018 | 0.018 | 0.017 | 0.016 |
| 13.667 | 0.016 | 0.015 | 0.015 | 0.015 | 0.014 |
| 13.833 | 0.014 | 0.014 | 0.014 | 0.014 | 0.013 |
| 14.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 14.167 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 14.333 | 0.013 | 0.013 | 0.012 | 0.012 | 0.012 |
| 14.500 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.667 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 14.833 | 0.012 | 0.012 | 0.012 | 0.012 | 0.011 |
| 15.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.167 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.333 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 15.500 | 0.011 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.667 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 15.833 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 16.000 | 0.010 | 0.010 | 0.009 | 0.009 | 0.009 |
| 16.167 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.333 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.500 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.667 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 16.833 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 17.000 | 0.009 | 0.009 | 0.008 | 0.008 | 0.008 |
| 17.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.333 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.500 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.667 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 17.833 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 18.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 18.167 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 18.333 | 0.008 | 0.008 | 0.008 | 0.007 | 0.007 |
| 18.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 18.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 19.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.167 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 20.333 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.500 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.667 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 20.833 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 21.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 21.167 | 0.007 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 21.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 22.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.167 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.333 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.500 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.667 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 23.833 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 24.000 | 0.006 | 0.006 | 0.005 | 0.005 | 0.005 |
| 24.167 | 0.005 | 0.005 | 0.004 | 0.004 | 0.004 |
| 24.333 | 0.004 | 0.004 | 0.003 | 0.003 | 0.003 |
| 24.500 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 |
| 24.667 | 0.002 | 0.002 | 0.001 | 0.001 | 0.001 |
| 24.833 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 |
| 25.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.000 |
| 25.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 25.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 26.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 27.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 28.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 32.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 33.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 34.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 34.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 40.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 40.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 41.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 42.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 43.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 44.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 45.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 46.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 47.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 47.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 48.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 49.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 50.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 51.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 52.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 53.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 54.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 54.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 55.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 56.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 57.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 58.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 59.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 60.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 61.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 61.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 62.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 63.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 64.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 65.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 66.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 67.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 68.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 68.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 69.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 70.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 71.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 72.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 73.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 74.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

# Post-Development Conditions

Subsection: Time vs. Volume
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**Time vs. Volume (ac-ft)**

**Output Time increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---|---|---|---|---|---|
| 75.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 75.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 76.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 77.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 78.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.167 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.333 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.667 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 79.833 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 80.000 | 0.000 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Elevation-Area Volume Curve
Return Event: 2 years
Label: Detention Pond
Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| Elevation (ft) | Planimeter ($ft^2$) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|---|---|---|---|---|---|
| 405.00 | 0.0 | 0.023 | 0.000 | 0.000 | 0.000 |
| 406.00 | 0.0 | 0.033 | 0.083 | 0.028 | 0.028 |
| 407.00 | 0.0 | 0.044 | 0.114 | 0.038 | 0.066 |
| 408.00 | 0.0 | 0.057 | 0.150 | 0.050 | 0.116 |
| 409.00 | 0.0 | 0.070 | 0.189 | 0.063 | 0.179 |
| 410.00 | 0.0 | 0.084 | 0.231 | 0.077 | 0.256 |

## Pond Volume Equations

*** Incremental volume computed by the Conic Method for Reservoir Volumes.**

**Volume = (1/3) * (EL2 - El1) * (Area1 + Area2 + sqr(Area1 * Area2))**

| | | |
|---|---|---|
| where: | EL1, EL2 | Lower and upper elevations of the increment |
| | Area1, Area2 | Areas computed for EL1, EL2, respectively |
| | Volume | Incremental volume between EL1 and EL2 |

# Post-Development Conditions

Subsection: Elevation-Area Volume Curve
Return Event: 10 years
Label: Detention Pond
Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| Elevation (ft) | Planimeter ($ft^2$) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|---|---|---|---|---|---|
| 405.00 | 0.0 | 0.023 | 0.000 | 0.000 | 0.000 |
| 406.00 | 0.0 | 0.033 | 0.083 | 0.028 | 0.028 |
| 407.00 | 0.0 | 0.044 | 0.114 | 0.038 | 0.066 |
| 408.00 | 0.0 | 0.057 | 0.150 | 0.050 | 0.116 |
| 409.00 | 0.0 | 0.070 | 0.189 | 0.063 | 0.179 |
| 410.00 | 0.0 | 0.084 | 0.231 | 0.077 | 0.256 |

Subsection: Volume Equations
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Pond Volume Equations

*** Incremental volume computed by the Conic Method for Reservoir Volumes.**

**Volume = (1/3) * (EL2 - El1) * (Area1 + Area2 + sqr(Area1 * Area2))**

| | | |
|---|---|---|
| where: | EL1, EL2 | Lower and upper elevations of the increment |
| | Area1, Area2 | Areas computed for EL1, EL2, respectively |
| | Volume | Incremental volume between EL1 and EL2 |

# Post-Development Conditions

Subsection: Elevation-Area Volume Curve
Return Event: 25 years
Label: Detention Pond
Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| Elevation (ft) | Planimeter ($ft^2$) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|---|---|---|---|---|---|
| 405.00 | 0.0 | 0.023 | 0.000 | 0.000 | 0.000 |
| 406.00 | 0.0 | 0.033 | 0.083 | 0.028 | 0.028 |
| 407.00 | 0.0 | 0.044 | 0.114 | 0.038 | 0.066 |
| 408.00 | 0.0 | 0.057 | 0.150 | 0.050 | 0.116 |
| 409.00 | 0.0 | 0.070 | 0.189 | 0.063 | 0.179 |
| 410.00 | 0.0 | 0.084 | 0.231 | 0.077 | 0.256 |

## Pond Volume Equations

*** Incremental volume computed by the Conic Method for Reservoir Volumes.**

**Volume = (1/3) * (EL2 - El1) * (Area1 + Area2 + sqr(Area1 * Area2))**

| | | |
|---|---|---|
| where: | EL1, EL2 | Lower and upper elevations of the increment |
| | Area1, Area2 | Areas computed for EL1, EL2, respectively |
| | Volume | Incremental volume between EL1 and EL2 |

# Post-Development Conditions

Subsection: Elevation-Area Volume Curve
Return Event: 50 years
Label: Detention Pond
Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| Elevation (ft) | Planimeter ($ft^2$) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|---|---|---|---|---|---|
| 405.00 | 0.0 | 0.023 | 0.000 | 0.000 | 0.000 |
| 406.00 | 0.0 | 0.033 | 0.083 | 0.028 | 0.028 |
| 407.00 | 0.0 | 0.044 | 0.114 | 0.038 | 0.066 |
| 408.00 | 0.0 | 0.057 | 0.150 | 0.050 | 0.116 |
| 409.00 | 0.0 | 0.070 | 0.189 | 0.063 | 0.179 |
| 410.00 | 0.0 | 0.084 | 0.231 | 0.077 | 0.256 |

## Pond Volume Equations

*** Incremental volume computed by the Conic Method for Reservoir Volumes.**

**Volume = (1/3) * (EL2 - El1) * (Area1 + Area2 + sqr(Area1 * Area2))**

| | | |
|---|---|---|
| where: | EL1, EL2 | Lower and upper elevations of the increment |
| | Area1, Area2 | Areas computed for EL1, EL2, respectively |
| | Volume | Incremental volume between EL1 and EL2 |

# Post-Development Conditions

Subsection: Elevation-Area Volume Curve
Return Event: 100 years
Label: Detention Pond
Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

| Elevation (ft) | Planimeter ($ft^2$) | Area (acres) | A1+A2+sqr (A1*A2) (acres) | Volume (ac-ft) | Volume (Total) (ac-ft) |
|---|---|---|---|---|---|
| 405.00 | 0.0 | 0.023 | 0.000 | 0.000 | 0.000 |
| 406.00 | 0.0 | 0.033 | 0.083 | 0.028 | 0.028 |
| 407.00 | 0.0 | 0.044 | 0.114 | 0.038 | 0.066 |
| 408.00 | 0.0 | 0.057 | 0.150 | 0.050 | 0.116 |
| 409.00 | 0.0 | 0.070 | 0.189 | 0.063 | 0.179 |
| 410.00 | 0.0 | 0.084 | 0.231 | 0.077 | 0.256 |

## Pond Volume Equations

*** Incremental volume computed by the Conic Method for Reservoir Volumes.**

**Volume = (1/3) * (EL2 - El1) * (Area1 + Area2 + sqr(Area1 * Area2))**

| | | |
|---|---|---|
| where: | EL1, EL2 | Lower and upper elevations of the increment |
| | Area1, Area2 | Areas computed for EL1, EL2, respectively |
| | Volume | Incremental volume between EL1 and EL2 |

| Requested Pond Water Surface Elevations | |
|---|---|
| Minimum (Headwater) | 405.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 410.00 ft |

## Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|---|---|---|---|---|---|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 407.20 | 407.53 |
| Orifice-Area | Orifice - 1 | Forward | Culvert - 1 | 407.20 | 410.00 |
| Inlet Box | Riser - 1 | Forward | Culvert - 1 | 407.80 | 410.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 405.00 | 410.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 401.87 | 410.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

| Structure ID: Culvert - 1<br>Structure Type: Culvert-Circular | |
|---|---|
| Number of Barrels | 1 |
| Diameter | 18.0 in |
| Length | 38.78 ft |
| Length (Computed Barrel) | 38.78 ft |
| Slope (Computed) | 0.011 ft/ft |

| Outlet Control Data | |
|---|---|
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.018 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| Inlet Control Data | |
|---|---|
| Equation Form | Form 1 |
| K | 0.0045 |
| M | 2.0000 |
| C | 0.0317 |
| Y | 0.6900 |
| T1 ratio (HW/D) | 1.089 |
| T2 ratio (HW/D) | 1.192 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.
Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control,
interpolate between flows at T1 & T2...

| | | | |
|---|---|---|---|
| T1 Elevation | 403.50 ft | T1 Flow | 7.58 ft³/s |
| T2 Elevation | 403.66 ft | T2 Flow | 8.66 ft³/s |

# Post-Development Conditions

Subsection: Outlet Input Data
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Structure ID: Riser - 1<br>Structure Type: Inlet Box | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.82 ft |
| Orifice Area | 16.0 ft² |
| Orifice Coefficient | 0.600 |
| Weir Length | 16.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| Structure ID: Orifice - 1<br>Structure Type: Orifice-Area | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Orifice Area | 1.3 ft² |
| Top Elevation | 407.53 ft |
| Datum Elevation | 407.36 ft |
| Orifice Coefficient | 0.600 |

| Structure ID: Weir - 1<br>Structure Type: Rectangular Weir | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Weir Length | 4.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |

| Structure ID: Orifice - 2<br>Structure Type: Orifice-Circular | |
|---|---|
| Number of Openings | 1 |
| Elevation | 405.00 ft |
| Orifice Diameter | 8.0 in |
| Orifice Coefficient | 0.600 |

| Structure ID: TW<br>Structure Type: TW Setup, DS Channel | |
|---|---|
| Tailwater Type | Free Outfall |

| Convergence Tolerances |
|---|

| Convergence Tolerances | |
|---|---|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.100 $ft^3/s$ |
| Flow Tolerance (Maximum) | 10.000 $ft^3/s$ |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | 402.00 | Free Outfall | Free Outfall | 0.00 | 0.05 | (N/A) | 0.00 |
| 405.20 | 0.08 | 402.00 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |
| 405.30 | 0.18 | 402.13 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |
| 405.40 | 0.48 | 402.20 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.50 | 0.68 | 402.27 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.60 | 0.88 | 402.34 | Free Outfall | Free Outfall | 0.00 | 0.09 | (N/A) | 0.00 |
| 405.70 | 1.00 | 402.40 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |
| 405.80 | 1.11 | 402.44 | Free Outfall | Free Outfall | 0.00 | 0.03 | (N/A) | 0.00 |
| 405.90 | 1.28 | 402.47 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 406.00 | 1.45 | 402.51 | Free Outfall | Free Outfall | 0.00 | 0.08 | (N/A) | 0.00 |
| 406.10 | 1.55 | 402.54 | Free Outfall | Free Outfall | 0.00 | 0.08 | (N/A) | 0.00 |
| 406.20 | 1.55 | 402.54 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 406.30 | 1.55 | 402.54 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.40 | 1.73 | 402.58 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 406.50 | 1.85 | 402.61 | Free Outfall | Free Outfall | 0.00 | 0.04 | (N/A) | 0.00 |
| 406.60 | 1.85 | 402.61 | Free Outfall | Free Outfall | 0.00 | 0.04 | (N/A) | 0.00 |
| 406.70 | 1.85 | 402.61 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.80 | 2.03 | 402.65 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 406.90 | 2.03 | 402.65 | Free Outfall | Free Outfall | 0.00 | 0.08 | (N/A) | 0.00 |
| 407.00 | 2.17 | 402.68 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.10 | 2.17 | 402.68 | Free Outfall | Free Outfall | 0.00 | 0.06 | (N/A) | 0.00 |
| 407.20 | 2.17 | 402.68 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.30 | 3.70 | 402.94 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.40 | 5.10 | 403.17 | Free Outfall | Free Outfall | 0.00 | 0.03 | (N/A) | 0.00 |
| 407.50 | 6.77 | 403.41 | Free Outfall | Free Outfall | 0.00 | 0.03 | (N/A) | 0.00 |
| 407.60 | 5.61 | 403.25 | Free Outfall | Free Outfall | 0.00 | 0.03 | (N/A) | 0.00 |
| 407.70 | 6.37 | 403.35 | Free Outfall | Free Outfall | 0.00 | 0.08 | (N/A) | 0.00 |
| 407.80 | 6.77 | 403.41 | Free Outfall | Free Outfall | 0.00 | 0.09 | (N/A) | 0.00 |
| 407.90 | 8.77 | 403.70 | Free Outfall | Free Outfall | 0.00 | 0.11 | (N/A) | 0.00 |
| 408.00 | 12.12 | 404.39 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.10 | 15.45 | 405.32 | Free Outfall | Free Outfall | 0.00 | 0.70 | (N/A) | 0.00 |
| 408.20 | 19.51 | 406.76 | Free Outfall | Free Outfall | 0.00 | 0.47 | (N/A) | 0.00 |
| 408.30 | 22.26 | 407.93 | Free Outfall | Free Outfall | 0.00 | 0.39 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | Message |
|---|---|---|---|---|---|---|---|---|---|
| 408.40 | 23.08 | 408.30 | Free Outfall | Free Outfall | 0.00 | 1.72 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.50 | 23.50 | 408.50 | Free Outfall | Free Outfall | 0.00 | 4.62 | (N/A) | 0.00 | CRIT.DEPTH CONTROL Vh= .032ft Dcr= .094ft CRIT.DEPTH Hev= .00ft |
| 408.60 | 23.70 | 408.60 | Free Outfall | Free Outfall | 0.00 | 10.64 | (N/A) | 0.00 | CRIT.DEPTH CONTROL Vh= .032ft Dcr= .094ft CRIT.DEPTH Hev= .00ft |
| 408.70 | 23.91 | 408.70 | Free Outfall | Free Outfall | 0.00 | 17.07 | (N/A) | 0.00 | CRIT.DEPTH CONTROL Vh= .064ft Dcr= .187ft CRIT.DEPTH Hev= .00ft |
| 408.80 | 24.12 | 408.80 | Free Outfall | Free Outfall | 0.00 | 23.88 | (N/A) | 0.00 | FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| 408.90 | 24.32 | 408.90 | Free Outfall | Free Outfall | 0.00 | 31.06 | (N/A) | 0.00 | |
| 409.00 | 24.52 | 409.00 | Free Outfall | Free Outfall | 0.00 | 38.58 | (N/A) | 0.00 | |
| 409.10 | 24.72 | 409.10 | Free Outfall | Free Outfall | 0.00 | 46.43 | (N/A) | 0.00 | |
| 409.20 | 24.92 | 409.20 | Free Outfall | Free Outfall | 0.00 | 54.59 | (N/A) | 0.00 | |
| 409.30 | 25.12 | 409.30 | Free Outfall | Free Outfall | 0.00 | 63.06 | (N/A) | 0.00 | |
| 409.40 | 25.31 | 409.40 | Free Outfall | Free Outfall | 0.00 | 71.83 | (N/A) | 0.00 | |
| 409.50 | 25.50 | 409.50 | Free Outfall | Free Outfall | 0.00 | 74.90 | (N/A) | 0.00 | |
| 409.60 | 25.70 | 409.60 | Free Outfall | Free Outfall | 0.00 | 77.62 | (N/A) | 0.00 | |
| 409.70 | 25.89 | 409.70 | Free Outfall | Free Outfall | 0.00 | 80.26 | (N/A) | 0.00 | |
| 409.80 | 26.08 | 409.80 | Free Outfall | Free Outfall | 0.00 | 82.83 | (N/A) | 0.00 | |
| 409.90 | 26.27 | 409.90 | Free Outfall | Free Outfall | 0.00 | 85.33 | (N/A) | 0.00 | |
| 410.00 | 26.45 | 410.00 | Free Outfall | Free Outfall | 0.00 | 87.77 | (N/A) | 0.00 | |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
| --- |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| INLET CONTROL... Equ.1: HW =.47 dc=.328 Ac=.2857 |
| CRIT.DEPTH CONTROL Vh= .133ft Dcr= .375ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .142ft Dcr= .398ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .151ft Dcr= .422ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .160ft Dcr= .445ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .170ft Dcr= .469ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .170ft Dcr= .469ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| CRIT.DEPTH CONTROL Vh= .179ft Dcr= .492ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .189ft Dcr= .515ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .189ft Dcr= .515ft CRIT.DEPTH Hev= .00ft |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| CRIT.DEPTH CONTROL Vh= .198ft Dcr= .539ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .198ft Dcr= .539ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .208ft Dcr= .562ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .208ft Dcr= .562ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| CRIT.DEPTH CONTROL Vh= .357ft Dcr= .867ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .448ft Dcr= 1.007ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .385ft Dcr= .914ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .423ft Dcr= .972ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .448ft Dcr= 1.007ft CRIT.DEPTH Hev= .00ft |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .571ft Dcr= 1.148ft |
| CRIT.DEPTH Hev= .00ft |
| INLET CONTROL... Submerged: HW =2.52 |
| INLET CONTROL... Submerged: HW =3.45 |
| INLET CONTROL... Submerged: HW =4.89 |
| INLET CONTROL... Submerged: HW =6.06 |
| INLET CONTROL... Submerged: HW =6.43 |
| INLET CONTROL... Submerged: HW =6.63 |
| INLET CONTROL... Submerged: HW =6.73 |
| INLET CONTROL... Submerged: HW =6.83 |
| INLET CONTROL... Submerged: HW =6.93 |
| INLET CONTROL... Submerged: HW =7.03 |
| INLET CONTROL... Submerged: HW =7.13 |
| INLET CONTROL... Submerged: HW =7.23 |
| INLET CONTROL... Submerged: HW =7.33 |
| INLET CONTROL... Submerged: HW =7.43 |
| INLET CONTROL... Submerged: HW =7.53 |
| INLET CONTROL... Submerged: HW =7.63 |
| INLET CONTROL... Submerged: HW =7.73 |
| INLET CONTROL... Submerged: HW =7.83 |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)
---
Mannings open channel maximum capacity: 12.04 ft³/s
Upstream ID = Weir - 1, Orifice - 1, Riser - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
| --- |
| INLET CONTROL... Submerged: HW =7.93 |
| INLET CONTROL... Submerged: HW =8.03 |
| INLET CONTROL... Submerged: HW =8.13 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Inlet Box)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.20 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.30 | 0.00 | 0.00 | 0.00 | 402.13 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.40 | 0.00 | 0.00 | 0.00 | 402.20 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.50 | 0.00 | 0.00 | 0.00 | 402.27 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.60 | 0.00 | 0.00 | 0.00 | 402.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.70 | 0.00 | 0.00 | 0.00 | 402.40 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.80 | 0.00 | 0.00 | 0.00 | 402.44 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.90 | 0.00 | 0.00 | 0.00 | 402.47 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.00 | 0.00 | 0.00 | 0.00 | 402.51 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.10 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.20 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.30 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.40 | 0.00 | 0.00 | 0.00 | 402.58 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.50 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.60 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.70 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.80 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.90 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.00 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.10 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.20 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.30 | 0.00 | 0.00 | 0.00 | 402.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.40 | 0.00 | 0.00 | 0.00 | 403.17 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.50 | 0.00 | 0.00 | 0.00 | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.60 | 0.00 | 0.00 | 0.00 | 403.25 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.70 | 0.00 | 0.00 | 0.00 | 403.35 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.80 | 0.00 | 0.00 | 0.00 | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.90 | 1.52 | 407.90 | Free Outfall | 403.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.00 | 4.29 | 408.00 | Free Outfall | 404.39 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.10 | 7.89 | 408.10 | Free Outfall | 405.32 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.20 | 12.14 | 408.20 | Free Outfall | 406.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.30 | 16.97 | 408.30 | 407.93 | 407.93 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.40 | 22.31 | 408.40 | 408.30 | 408.30 | 0.00 | 0.00 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Inlet Box)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | Message |
|---|---|---|---|---|---|---|---|---|---|
| 408.50 | 28.11 | 408.50 | 408.50 | 408.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.60 | 34.35 | 408.60 | 408.60 | 408.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.70 | 40.98 | 408.70 | 408.70 | 408.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.80 | 48.00 | 408.80 | 408.80 | 408.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.90 | 55.38 | 408.90 | 408.90 | 408.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.00 | 63.10 | 409.00 | 409.00 | 409.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.10 | 71.15 | 409.10 | 409.10 | 409.10 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.20 | 79.51 | 409.20 | 409.20 | 409.20 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.30 | 88.18 | 409.30 | 409.30 | 409.30 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.40 | 97.15 | 409.40 | 409.40 | 409.40 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.50 | 100.41 | 409.50 | 409.50 | 409.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.60 | 103.32 | 409.60 | 409.60 | 409.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.70 | 106.15 | 409.70 | 409.70 | 409.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.80 | 108.91 | 409.80 | 409.80 | 409.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.90 | 111.60 | 409.90 | 409.90 | 409.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 410.00 | 114.22 | 410.00 | 410.00 | 410.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Inlet Box)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| Weir: H =0.1ft |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Inlet Box)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| Weir: H =0.2ft |
| Weir: H =0.3ft |
| Weir: H =0.4ft |
| FULLY CHARGED RISER: ADJUSTED TO WEIR: H =0.5ft |
| FULLY CHARGED RISER: ADJUSTED TO WEIR: H =0.6ft |
| FULLY CHARGED RISER: ADJUSTED TO WEIR: H =0.7ft |
| FULLY CHARGED RISER: ADJUSTED TO WEIR: H =0.8ft |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Inlet Box)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |
| FULLY CHARGED RISER, DOWNSTREAM CONTROL: Kev=0. Hev=0.000 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 1 (Orifice-Area)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.20 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.30 | 0.00 | 0.00 | 0.00 | 402.13 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.40 | 0.00 | 0.00 | 0.00 | 402.20 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.50 | 0.00 | 0.00 | 0.00 | 402.27 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.60 | 0.00 | 0.00 | 0.00 | 402.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.70 | 0.00 | 0.00 | 0.00 | 402.40 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.80 | 0.00 | 0.00 | 0.00 | 402.44 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.90 | 0.00 | 0.00 | 0.00 | 402.47 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.00 | 0.00 | 0.00 | 0.00 | 402.51 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.10 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.20 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.30 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.40 | 0.00 | 0.00 | 0.00 | 402.58 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.50 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.60 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.70 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.80 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.90 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.00 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.10 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.20 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.30 | 0.79 | 407.30 | Free Outfall | 402.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.40 | 1.59 | 407.40 | Free Outfall | 403.17 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.50 | 2.38 | 407.50 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.60 | 3.11 | 407.60 | Free Outfall | 403.25 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.70 | 3.70 | 407.70 | Free Outfall | 403.35 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.80 | 4.21 | 407.80 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.90 | 4.67 | 407.90 | Free Outfall | 403.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.00 | 5.08 | 408.00 | Free Outfall | 404.39 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.10 | 5.47 | 408.10 | Free Outfall | 405.32 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.20 | 5.82 | 408.20 | Free Outfall | 406.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.30 | 3.88 | 408.30 | 407.93 | 407.93 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.40 | 1.97 | 408.40 | 408.30 | 408.30 | 0.00 | 0.00 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 1 (Orifice-Area)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | Message |
|---|---|---|---|---|---|---|---|---|---|
| 408.50 | 0.00 | 408.50 | 408.50 | 408.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.60 | 0.00 | 408.60 | 408.60 | 408.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.70 | 0.00 | 408.70 | 408.70 | 408.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.80 | 0.00 | 408.80 | 408.80 | 408.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.90 | 0.00 | 408.90 | 408.90 | 408.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.00 | 0.00 | 409.00 | 409.00 | 409.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.10 | 0.00 | 409.10 | 409.10 | 409.10 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.20 | 0.00 | 409.20 | 409.20 | 409.20 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.30 | 0.00 | 409.30 | 409.30 | 409.30 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.40 | 0.00 | 409.40 | 409.40 | 409.40 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.50 | 0.00 | 409.50 | 409.50 | 409.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.60 | 0.00 | 409.60 | 409.60 | 409.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.70 | 0.00 | 409.70 | 409.70 | 409.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.80 | 0.00 | 409.80 | 409.80 | 409.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.90 | 0.00 | 409.90 | 409.90 | 409.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 410.00 | 0.00 | 410.00 | 410.00 | 410.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 1 (Orifice-Area)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| Hi=.10; Ht=.17; Qt=2.62 |
| Hi=.20; Ht=.17; Qt=2.62 |
| Hi=.30; Ht=.17; Qt=2.62 |
| H =.24 |
| H =.34 |
| H =.44 |
| H =.54 |
| H =.64 |
| H =.74 |
| H =.84 |
| H =.37 |
| H =.10 |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 1 (Orifice-Area)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 1 (Orifice-Area)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.20 | 0.00 | 0.00 | 0.00 | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.30 | 0.00 | 0.00 | 0.00 | 402.13 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.40 | 0.00 | 0.00 | 0.00 | 402.20 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.50 | 0.00 | 0.00 | 0.00 | 402.27 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.60 | 0.00 | 0.00 | 0.00 | 402.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.70 | 0.00 | 0.00 | 0.00 | 402.40 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.80 | 0.00 | 0.00 | 0.00 | 402.44 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.90 | 0.00 | 0.00 | 0.00 | 402.47 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.00 | 0.00 | 0.00 | 0.00 | 402.51 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.10 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.20 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.30 | 0.00 | 0.00 | 0.00 | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.40 | 0.00 | 0.00 | 0.00 | 402.58 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.50 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.60 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.70 | 0.00 | 0.00 | 0.00 | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.80 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.90 | 0.00 | 0.00 | 0.00 | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.00 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.10 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.20 | 0.00 | 0.00 | 0.00 | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.30 | 0.38 | 407.30 | Free Outfall | 402.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.40 | 1.06 | 407.40 | Free Outfall | 403.17 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.50 | 1.94 | 407.50 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.60 | 0.00 | 407.60 | Free Outfall | 403.25 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.70 | 0.00 | 407.70 | Free Outfall | 403.35 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.80 | 0.00 | 407.80 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.90 | 0.00 | 407.90 | Free Outfall | 403.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.00 | 0.00 | 408.00 | Free Outfall | 404.39 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.10 | 0.00 | 408.10 | Free Outfall | 405.32 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.20 | 0.00 | 408.20 | Free Outfall | 406.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.30 | 0.00 | 408.30 | 407.93 | 407.93 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.40 | 0.00 | 408.40 | 408.30 | 408.30 | 0.00 | 0.00 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) | Message |
|---|---|---|---|---|---|---|---|---|---|
| 408.50 | 0.00 | 408.50 | 408.50 | 408.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.60 | 0.00 | 408.60 | 408.60 | 408.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.70 | 0.00 | 408.70 | 408.70 | 408.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.80 | 0.00 | 408.80 | 408.80 | 408.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 408.90 | 0.00 | 408.90 | 408.90 | 408.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.00 | 0.00 | 409.00 | 409.00 | 409.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.10 | 0.00 | 409.10 | 409.10 | 409.10 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.20 | 0.00 | 409.20 | 409.20 | 409.20 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.30 | 0.00 | 409.30 | 409.30 | 409.30 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.40 | 0.00 | 409.40 | 409.40 | 409.40 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.50 | 0.00 | 409.50 | 409.50 | 409.50 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.60 | 0.00 | 409.60 | 409.60 | 409.60 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.70 | 0.00 | 409.70 | 409.70 | 409.70 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.80 | 0.00 | 409.80 | 409.80 | 409.80 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 409.90 | 0.00 | 409.90 | 409.90 | 409.90 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |
| 410.00 | 0.00 | 410.00 | 410.00 | 410.00 | 0.00 | 0.00 | (N/A) | 0.00 | WS below an invert; no flow. |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| H=.10; Htw=.00; Qfree=.38; |
| H=.20; Htw=.00; Qfree=1.06; |
| H=.30; Htw=.00; Qfree=1.94; |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| E >= E2= 407.530 |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

# Post-Development Conditions

Subsection: Individual Outlet Curves
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 2 (Orifice-Circular)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.03 | 405.10 | Free Outfall | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.20 | 0.10 | 405.20 | Free Outfall | 402.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.30 | 0.20 | 405.30 | Free Outfall | 402.13 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.40 | 0.37 | 405.40 | Free Outfall | 402.20 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.50 | 0.57 | 405.50 | Free Outfall | 402.27 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.60 | 0.79 | 405.60 | Free Outfall | 402.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.70 | 1.02 | 405.70 | Free Outfall | 402.40 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.80 | 1.15 | 405.80 | Free Outfall | 402.44 | 0.00 | 0.00 | (N/A) | 0.00 |
| 405.90 | 1.26 | 405.90 | Free Outfall | 402.47 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.00 | 1.37 | 406.00 | Free Outfall | 402.51 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.10 | 1.47 | 406.10 | Free Outfall | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.20 | 1.56 | 406.20 | Free Outfall | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.30 | 1.65 | 406.30 | Free Outfall | 402.54 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.40 | 1.74 | 406.40 | Free Outfall | 402.58 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.50 | 1.81 | 406.50 | Free Outfall | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.60 | 1.89 | 406.60 | Free Outfall | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.70 | 1.96 | 406.70 | Free Outfall | 402.61 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.80 | 2.03 | 406.80 | Free Outfall | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 406.90 | 2.10 | 406.90 | Free Outfall | 402.65 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.00 | 2.17 | 407.00 | Free Outfall | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.10 | 2.23 | 407.10 | Free Outfall | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.20 | 2.30 | 407.20 | Free Outfall | 402.68 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.30 | 2.36 | 407.30 | Free Outfall | 402.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.40 | 2.42 | 407.40 | Free Outfall | 403.17 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.50 | 2.47 | 407.50 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.60 | 2.53 | 407.60 | Free Outfall | 403.25 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.70 | 2.58 | 407.70 | Free Outfall | 403.35 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.80 | 2.64 | 407.80 | Free Outfall | 403.41 | 0.00 | 0.00 | (N/A) | 0.00 |
| 407.90 | 2.69 | 407.90 | Free Outfall | 403.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.00 | 2.74 | 408.00 | Free Outfall | 404.39 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.10 | 2.79 | 408.10 | 405.32 | 405.32 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.20 | 2.02 | 408.20 | 406.76 | 406.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.30 | 1.03 | 408.30 | 407.93 | 407.93 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.40 | 0.52 | 408.40 | 408.30 | 408.30 | 0.00 | 0.00 | (N/A) | 0.00 |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 2 (Orifice-Circular)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft³/s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft³/s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|---|---|---|---|---|---|---|---|---|
| 408.50 | 0.00 | 408.50 | 408.50 | 408.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.60 | 0.00 | 408.60 | 408.60 | 408.60 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.70 | 0.00 | 408.70 | 408.70 | 408.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.80 | 0.00 | 408.80 | 408.80 | 408.80 | 0.00 | 0.00 | (N/A) | 0.00 |
| 408.90 | 0.00 | 408.90 | 408.90 | 408.90 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.00 | 0.00 | 409.00 | 409.00 | 409.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.10 | 0.00 | 409.10 | 409.10 | 409.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.20 | 0.00 | 409.20 | 409.20 | 409.20 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.30 | 0.00 | 409.30 | 409.30 | 409.30 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.40 | 0.00 | 409.40 | 409.40 | 409.40 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.50 | 0.00 | 409.50 | 409.50 | 409.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.60 | 0.00 | 409.60 | 409.60 | 409.60 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.70 | 0.00 | 409.70 | 409.70 | 409.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.80 | 0.00 | 409.80 | 409.80 | 409.80 | 0.00 | 0.00 | (N/A) | 0.00 |
| 409.90 | 0.00 | 409.90 | 409.90 | 409.90 | 0.00 | 0.00 | (N/A) | 0.00 |
| 410.00 | 0.00 | 410.00 | 410.00 | 410.00 | 0.00 | 0.00 | (N/A) | 0.00 |

| Message |
|---|
| WS below an invert; no flow. |
| CRIT.DEPTH CONTROL Vh= .017ft Dcr= .083ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .032ft Dcr= .167ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .133ft Dcr= .167ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .150ft Dcr= .250ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .167ft Dcr= .333ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .183ft Dcr= .416ft CRIT.DEPTH Hev= .00ft |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 2 (Orifice-Circular)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| H =.37 |
| H =.47 |
| H =.57 |
| H =.67 |
| H =.77 |
| H =.87 |
| H =.97 |
| H =1.07 |
| H =1.17 |
| H =1.27 |
| H =1.37 |
| H =1.47 |
| H =1.57 |
| H =1.67 |
| H =1.77 |
| H =1.87 |
| H =1.97 |
| H =2.07 |
| H =2.17 |
| H =2.27 |
| H =2.37 |
| H =2.47 |
| H =2.57 |
| H =2.67 |
| H =2.77 |
| H =1.44 |
| H =.37 |
| H =.10 |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 2 (Orifice-Circular)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Orifice - 2 (Orifice-Circular)
---
Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
| --- |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO DOWNSTREAM CONTROLLING STRUCTURE |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 405.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | (N/A) | 0.00 |
| 405.20 | 0.08 | (N/A) | 0.00 |
| 405.30 | 0.18 | (N/A) | 0.00 |
| 405.40 | 0.37 | (N/A) | 0.00 |
| 405.50 | 0.57 | (N/A) | 0.00 |
| 405.60 | 0.88 | (N/A) | 0.00 |
| 405.70 | 1.00 | (N/A) | 0.00 |
| 405.80 | 1.11 | (N/A) | 0.00 |
| 405.90 | 1.28 | (N/A) | 0.00 |
| 406.00 | 1.45 | (N/A) | 0.00 |
| 406.10 | 1.55 | (N/A) | 0.00 |
| 406.20 | 1.55 | (N/A) | 0.00 |
| 406.30 | 1.65 | (N/A) | 0.00 |
| 406.40 | 1.73 | (N/A) | 0.00 |
| 406.50 | 1.85 | (N/A) | 0.00 |
| 406.60 | 1.85 | (N/A) | 0.00 |
| 406.70 | 1.96 | (N/A) | 0.00 |
| 406.80 | 2.03 | (N/A) | 0.00 |
| 406.90 | 2.03 | (N/A) | 0.00 |
| 407.00 | 2.17 | (N/A) | 0.00 |
| 407.10 | 2.17 | (N/A) | 0.00 |
| 407.20 | 2.30 | (N/A) | 0.00 |
| 407.30 | 3.53 | (N/A) | 0.00 |
| 407.40 | 5.10 | (N/A) | 0.00 |
| 407.50 | 6.77 | (N/A) | 0.00 |
| 407.60 | 5.61 | (N/A) | 0.00 |
| 407.70 | 6.37 | (N/A) | 0.00 |
| 407.80 | 6.77 | (N/A) | 0.00 |
| 407.90 | 8.77 | (N/A) | 0.00 |
| 408.00 | 12.12 | (N/A) | 0.00 |
| 408.10 | 15.45 | (N/A) | 0.00 |
| 408.20 | 19.51 | (N/A) | 0.00 |
| 408.30 | 22.26 | (N/A) | 0.00 |
| 408.40 | 23.08 | (N/A) | 0.00 |
| 408.50 | 23.50 | (N/A) | 0.00 |
| 408.60 | 23.70 | (N/A) | 0.00 |
| 408.70 | 23.91 | (N/A) | 0.00 |
| 408.80 | 24.12 | (N/A) | 0.00 |
| 408.90 | 24.32 | (N/A) | 0.00 |
| 409.00 | 24.52 | (N/A) | 0.00 |
| 409.10 | 24.72 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) | Contributing Structures |
|---|---|---|---|---|
| 409.20 | 24.92 | (N/A) | 0.00 | (no Q: Weir - 1,Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1) |
| 409.30 | 25.12 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.40 | 25.31 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.50 | 25.50 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.60 | 25.70 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.70 | 25.89 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.80 | 26.08 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.90 | 26.27 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 410.00 | 26.45 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

| Requested Pond Water Surface Elevations | |
|---|---|
| Minimum (Headwater) | 405.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 410.00 ft |

## Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|---|---|---|---|---|---|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 407.20 | 407.53 |
| Orifice-Area | Orifice - 1 | Forward | Culvert - 1 | 407.20 | 410.00 |
| Inlet Box | Riser - 1 | Forward | Culvert - 1 | 407.80 | 410.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 405.00 | 410.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 401.87 | 410.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

| Structure ID: Culvert - 1<br>Structure Type: Culvert-Circular | |
|---|---|
| Number of Barrels | 1 |
| Diameter | 18.0 in |
| Length | 38.78 ft |
| Length (Computed Barrel) | 38.78 ft |
| Slope (Computed) | 0.011 ft/ft |

| Outlet Control Data | |
|---|---|
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.018 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| Inlet Control Data | |
|---|---|
| Equation Form | Form 1 |
| K | 0.0045 |
| M | 2.0000 |
| C | 0.0317 |
| Y | 0.6900 |
| T1 ratio (HW/D) | 1.089 |
| T2 ratio (HW/D) | 1.192 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.
Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control,
interpolate between flows at T1 & T2...

| | | | |
|---|---|---|---|
| T1 Elevation | 403.50 ft | T1 Flow | 7.58 ft³/s |
| T2 Elevation | 403.66 ft | T2 Flow | 8.66 ft³/s |

# Post-Development Conditions

Subsection: Outlet Input Data
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Structure ID: Riser - 1<br>Structure Type: Inlet Box | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.82 ft |
| Orifice Area | 16.0 ft² |
| Orifice Coefficient | 0.600 |
| Weir Length | 16.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| Structure ID: Orifice - 1<br>Structure Type: Orifice-Area | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Orifice Area | 1.3 ft² |
| Top Elevation | 407.53 ft |
| Datum Elevation | 407.36 ft |
| Orifice Coefficient | 0.600 |

| Structure ID: Weir - 1<br>Structure Type: Rectangular Weir | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Weir Length | 4.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |

| Structure ID: Orifice - 2<br>Structure Type: Orifice-Circular | |
|---|---|
| Number of Openings | 1 |
| Elevation | 405.00 ft |
| Orifice Diameter | 8.0 in |
| Orifice Coefficient | 0.600 |

| Structure ID: TW<br>Structure Type: TW Setup, DS Channel | |
|---|---|
| Tailwater Type | Free Outfall |

| Convergence Tolerances |
|---|

| Convergence Tolerances | |
|---|---|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.100 $ft^3/s$ |
| Flow Tolerance (Maximum) | 10.000 $ft^3/s$ |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 405.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | (N/A) | 0.00 |
| 405.20 | 0.08 | (N/A) | 0.00 |
| 405.30 | 0.18 | (N/A) | 0.00 |
| 405.40 | 0.37 | (N/A) | 0.00 |
| 405.50 | 0.57 | (N/A) | 0.00 |
| 405.60 | 0.88 | (N/A) | 0.00 |
| 405.70 | 1.00 | (N/A) | 0.00 |
| 405.80 | 1.11 | (N/A) | 0.00 |
| 405.90 | 1.28 | (N/A) | 0.00 |
| 406.00 | 1.45 | (N/A) | 0.00 |
| 406.10 | 1.55 | (N/A) | 0.00 |
| 406.20 | 1.55 | (N/A) | 0.00 |
| 406.30 | 1.65 | (N/A) | 0.00 |
| 406.40 | 1.73 | (N/A) | 0.00 |
| 406.50 | 1.85 | (N/A) | 0.00 |
| 406.60 | 1.85 | (N/A) | 0.00 |
| 406.70 | 1.96 | (N/A) | 0.00 |
| 406.80 | 2.03 | (N/A) | 0.00 |
| 406.90 | 2.03 | (N/A) | 0.00 |
| 407.00 | 2.17 | (N/A) | 0.00 |
| 407.10 | 2.17 | (N/A) | 0.00 |
| 407.20 | 2.30 | (N/A) | 0.00 |
| 407.30 | 3.53 | (N/A) | 0.00 |
| 407.40 | 5.10 | (N/A) | 0.00 |
| 407.50 | 6.77 | (N/A) | 0.00 |
| 407.60 | 5.61 | (N/A) | 0.00 |
| 407.70 | 6.37 | (N/A) | 0.00 |
| 407.80 | 6.77 | (N/A) | 0.00 |
| 407.90 | 8.77 | (N/A) | 0.00 |
| 408.00 | 12.12 | (N/A) | 0.00 |
| 408.10 | 15.45 | (N/A) | 0.00 |
| 408.20 | 19.51 | (N/A) | 0.00 |
| 408.30 | 22.26 | (N/A) | 0.00 |
| 408.40 | 23.08 | (N/A) | 0.00 |
| 408.50 | 23.50 | (N/A) | 0.00 |
| 408.60 | 23.70 | (N/A) | 0.00 |
| 408.70 | 23.91 | (N/A) | 0.00 |
| 408.80 | 24.12 | (N/A) | 0.00 |
| 408.90 | 24.32 | (N/A) | 0.00 |
| 409.00 | 24.52 | (N/A) | 0.00 |
| 409.10 | 24.72 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 409.20 | 24.92 | (N/A) | 0.00 |
| 409.30 | 25.12 | (N/A) | 0.00 |
| 409.40 | 25.31 | (N/A) | 0.00 |
| 409.50 | 25.50 | (N/A) | 0.00 |
| 409.60 | 25.70 | (N/A) | 0.00 |
| 409.70 | 25.89 | (N/A) | 0.00 |
| 409.80 | 26.08 | (N/A) | 0.00 |
| 409.90 | 26.27 | (N/A) | 0.00 |
| 410.00 | 26.45 | (N/A) | 0.00 |

| Contributing Structures |
|---|
| (no Q: Weir - 1,Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

| Requested Pond Water Surface Elevations | |
|---|---|
| Minimum (Headwater) | 405.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 410.00 ft |

## Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|---|---|---|---|---|---|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 407.20 | 407.53 |
| Orifice-Area | Orifice - 1 | Forward | Culvert - 1 | 407.20 | 410.00 |
| Inlet Box | Riser - 1 | Forward | Culvert - 1 | 407.80 | 410.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 405.00 | 410.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 401.87 | 410.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

| Structure ID: Culvert - 1<br>Structure Type: Culvert-Circular | |
|---|---|
| Number of Barrels | 1 |
| Diameter | 18.0 in |
| Length | 38.78 ft |
| Length (Computed Barrel) | 38.78 ft |
| Slope (Computed) | 0.011 ft/ft |

| Outlet Control Data | |
|---|---|
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.018 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| Inlet Control Data | |
|---|---|
| Equation Form | Form 1 |
| K | 0.0045 |
| M | 2.0000 |
| C | 0.0317 |
| Y | 0.6900 |
| T1 ratio (HW/D) | 1.089 |
| T2 ratio (HW/D) | 1.192 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.
Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control,
interpolate between flows at T1 & T2...

| | | | |
|---|---|---|---|
| T1 Elevation | 403.50 ft | T1 Flow | 7.58 ft³/s |
| T2 Elevation | 403.66 ft | T2 Flow | 8.66 ft³/s |

# Post-Development Conditions

Subsection: Outlet Input Data
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Structure ID: Riser - 1<br>Structure Type: Inlet Box | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.82 ft |
| Orifice Area | 16.0 ft² |
| Orifice Coefficient | 0.600 |
| Weir Length | 16.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| Structure ID: Orifice - 1<br>Structure Type: Orifice-Area | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Orifice Area | 1.3 ft² |
| Top Elevation | 407.53 ft |
| Datum Elevation | 407.36 ft |
| Orifice Coefficient | 0.600 |

| Structure ID: Weir - 1<br>Structure Type: Rectangular Weir | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Weir Length | 4.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |

| Structure ID: Orifice - 2<br>Structure Type: Orifice-Circular | |
|---|---|
| Number of Openings | 1 |
| Elevation | 405.00 ft |
| Orifice Diameter | 8.0 in |
| Orifice Coefficient | 0.600 |

| Structure ID: TW<br>Structure Type: TW Setup, DS Channel | |
|---|---|
| Tailwater Type | Free Outfall |

| Convergence Tolerances |
|---|

| Convergence Tolerances | |
|---|---|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.100 $ft^3/s$ |
| Flow Tolerance (Maximum) | 10.000 $ft^3/s$ |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 405.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | (N/A) | 0.00 |
| 405.20 | 0.08 | (N/A) | 0.00 |
| 405.30 | 0.18 | (N/A) | 0.00 |
| 405.40 | 0.37 | (N/A) | 0.00 |
| 405.50 | 0.57 | (N/A) | 0.00 |
| 405.60 | 0.88 | (N/A) | 0.00 |
| 405.70 | 1.00 | (N/A) | 0.00 |
| 405.80 | 1.11 | (N/A) | 0.00 |
| 405.90 | 1.28 | (N/A) | 0.00 |
| 406.00 | 1.45 | (N/A) | 0.00 |
| 406.10 | 1.55 | (N/A) | 0.00 |
| 406.20 | 1.55 | (N/A) | 0.00 |
| 406.30 | 1.65 | (N/A) | 0.00 |
| 406.40 | 1.73 | (N/A) | 0.00 |
| 406.50 | 1.85 | (N/A) | 0.00 |
| 406.60 | 1.85 | (N/A) | 0.00 |
| 406.70 | 1.96 | (N/A) | 0.00 |
| 406.80 | 2.03 | (N/A) | 0.00 |
| 406.90 | 2.03 | (N/A) | 0.00 |
| 407.00 | 2.17 | (N/A) | 0.00 |
| 407.10 | 2.17 | (N/A) | 0.00 |
| 407.20 | 2.30 | (N/A) | 0.00 |
| 407.30 | 3.53 | (N/A) | 0.00 |
| 407.40 | 5.10 | (N/A) | 0.00 |
| 407.50 | 6.77 | (N/A) | 0.00 |
| 407.60 | 5.61 | (N/A) | 0.00 |
| 407.70 | 6.37 | (N/A) | 0.00 |
| 407.80 | 6.77 | (N/A) | 0.00 |
| 407.90 | 8.77 | (N/A) | 0.00 |
| 408.00 | 12.12 | (N/A) | 0.00 |
| 408.10 | 15.45 | (N/A) | 0.00 |
| 408.20 | 19.51 | (N/A) | 0.00 |
| 408.30 | 22.26 | (N/A) | 0.00 |
| 408.40 | 23.08 | (N/A) | 0.00 |
| 408.50 | 23.50 | (N/A) | 0.00 |
| 408.60 | 23.70 | (N/A) | 0.00 |
| 408.70 | 23.91 | (N/A) | 0.00 |
| 408.80 | 24.12 | (N/A) | 0.00 |
| 408.90 | 24.32 | (N/A) | 0.00 |
| 409.00 | 24.52 | (N/A) | 0.00 |
| 409.10 | 24.72 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) | Contributing Structures |
|---|---|---|---|---|
| 409.20 | 24.92 | (N/A) | 0.00 | (no Q: Weir - 1,Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1) |
| 409.30 | 25.12 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.40 | 25.31 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.50 | 25.50 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.60 | 25.70 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.70 | 25.89 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.80 | 26.08 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 409.90 | 26.27 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| 410.00 | 26.45 | (N/A) | 0.00 | Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
|---|
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

| Requested Pond Water Surface Elevations | |
|---|---|
| Minimum (Headwater) | 405.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 410.00 ft |

## Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|---|---|---|---|---|---|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 407.20 | 407.53 |
| Orifice-Area | Orifice - 1 | Forward | Culvert - 1 | 407.20 | 410.00 |
| Inlet Box | Riser - 1 | Forward | Culvert - 1 | 407.80 | 410.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 405.00 | 410.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 401.87 | 410.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

| Structure ID: Culvert - 1<br>Structure Type: Culvert-Circular | |
|---|---|
| Number of Barrels | 1 |
| Diameter | 18.0 in |
| Length | 38.78 ft |
| Length (Computed Barrel) | 38.78 ft |
| Slope (Computed) | 0.011 ft/ft |

| Outlet Control Data | |
|---|---|
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.018 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| Inlet Control Data | |
|---|---|
| Equation Form | Form 1 |
| K | 0.0045 |
| M | 2.0000 |
| C | 0.0317 |
| Y | 0.6900 |
| T1 ratio (HW/D) | 1.089 |
| T2 ratio (HW/D) | 1.192 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.
Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control,
interpolate between flows at T1 & T2...

| | | | |
|---|---|---|---|
| T1 Elevation | 403.50 ft | T1 Flow | 7.58 ft³/s |
| T2 Elevation | 403.66 ft | T2 Flow | 8.66 ft³/s |

# Post-Development Conditions

Subsection: Outlet Input Data
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Structure ID: Riser - 1<br>Structure Type: Inlet Box | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.82 ft |
| Orifice Area | 16.0 ft² |
| Orifice Coefficient | 0.600 |
| Weir Length | 16.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| Structure ID: Orifice - 1<br>Structure Type: Orifice-Area | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Orifice Area | 1.3 ft² |
| Top Elevation | 407.53 ft |
| Datum Elevation | 407.36 ft |
| Orifice Coefficient | 0.600 |

| Structure ID: Weir - 1<br>Structure Type: Rectangular Weir | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Weir Length | 4.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |

| Structure ID: Orifice - 2<br>Structure Type: Orifice-Circular | |
|---|---|
| Number of Openings | 1 |
| Elevation | 405.00 ft |
| Orifice Diameter | 8.0 in |
| Orifice Coefficient | 0.600 |

| Structure ID: TW<br>Structure Type: TW Setup, DS Channel | |
|---|---|
| Tailwater Type | Free Outfall |

| Convergence Tolerances |
|---|

| Convergence Tolerances | |
|---|---|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.100 $ft^3/s$ |
| Flow Tolerance (Maximum) | 10.000 $ft^3/s$ |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 405.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | (N/A) | 0.00 |
| 405.20 | 0.08 | (N/A) | 0.00 |
| 405.30 | 0.18 | (N/A) | 0.00 |
| 405.40 | 0.37 | (N/A) | 0.00 |
| 405.50 | 0.57 | (N/A) | 0.00 |
| 405.60 | 0.88 | (N/A) | 0.00 |
| 405.70 | 1.00 | (N/A) | 0.00 |
| 405.80 | 1.11 | (N/A) | 0.00 |
| 405.90 | 1.28 | (N/A) | 0.00 |
| 406.00 | 1.45 | (N/A) | 0.00 |
| 406.10 | 1.55 | (N/A) | 0.00 |
| 406.20 | 1.55 | (N/A) | 0.00 |
| 406.30 | 1.65 | (N/A) | 0.00 |
| 406.40 | 1.73 | (N/A) | 0.00 |
| 406.50 | 1.85 | (N/A) | 0.00 |
| 406.60 | 1.85 | (N/A) | 0.00 |
| 406.70 | 1.96 | (N/A) | 0.00 |
| 406.80 | 2.03 | (N/A) | 0.00 |
| 406.90 | 2.03 | (N/A) | 0.00 |
| 407.00 | 2.17 | (N/A) | 0.00 |
| 407.10 | 2.17 | (N/A) | 0.00 |
| 407.20 | 2.30 | (N/A) | 0.00 |
| 407.30 | 3.53 | (N/A) | 0.00 |
| 407.40 | 5.10 | (N/A) | 0.00 |
| 407.50 | 6.77 | (N/A) | 0.00 |
| 407.60 | 5.61 | (N/A) | 0.00 |
| 407.70 | 6.37 | (N/A) | 0.00 |
| 407.80 | 6.77 | (N/A) | 0.00 |
| 407.90 | 8.77 | (N/A) | 0.00 |
| 408.00 | 12.12 | (N/A) | 0.00 |
| 408.10 | 15.45 | (N/A) | 0.00 |
| 408.20 | 19.51 | (N/A) | 0.00 |
| 408.30 | 22.26 | (N/A) | 0.00 |
| 408.40 | 23.08 | (N/A) | 0.00 |
| 408.50 | 23.50 | (N/A) | 0.00 |
| 408.60 | 23.70 | (N/A) | 0.00 |
| 408.70 | 23.91 | (N/A) | 0.00 |
| 408.80 | 24.12 | (N/A) | 0.00 |
| 408.90 | 24.32 | (N/A) | 0.00 |
| 409.00 | 24.52 | (N/A) | 0.00 |
| 409.10 | 24.72 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 409.20 | 24.92 | (N/A) | 0.00 |
| 409.30 | 25.12 | (N/A) | 0.00 |
| 409.40 | 25.31 | (N/A) | 0.00 |
| 409.50 | 25.50 | (N/A) | 0.00 |
| 409.60 | 25.70 | (N/A) | 0.00 |
| 409.70 | 25.89 | (N/A) | 0.00 |
| 409.80 | 26.08 | (N/A) | 0.00 |
| 409.90 | 26.27 | (N/A) | 0.00 |
| 410.00 | 26.45 | (N/A) | 0.00 |

| Contributing Structures |
|---|
| (no Q: Weir - 1,Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

Composite Outflow Summary

| Contributing Structures |
| --- |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

| Requested Pond Water Surface Elevations | |
|---|---|
| Minimum (Headwater) | 405.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 410.00 ft |

## Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|---|---|---|---|---|---|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 407.20 | 407.53 |
| Orifice-Area | Orifice - 1 | Forward | Culvert - 1 | 407.20 | 410.00 |
| Inlet Box | Riser - 1 | Forward | Culvert - 1 | 407.82 | 410.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 405.00 | 410.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 401.87 | 410.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

| Structure ID: Culvert - 1<br>Structure Type: Culvert-Circular | |
|---|---|
| Number of Barrels | 1 |
| Diameter | 18.0 in |
| Length | 38.78 ft |
| Length (Computed Barrel) | 38.78 ft |
| Slope (Computed) | 0.011 ft/ft |

| Outlet Control Data | |
|---|---|
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.018 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| Inlet Control Data | |
|---|---|
| Equation Form | Form 1 |
| K | 0.0045 |
| M | 2.0000 |
| C | 0.0317 |
| Y | 0.6900 |
| T1 ratio (HW/D) | 1.089 |
| T2 ratio (HW/D) | 1.192 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.
Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control,
interpolate between flows at T1 & T2...

| | | | |
|---|---|---|---|
| T1 Elevation | 403.50 ft | T1 Flow | 7.58 ft³/s |
| T2 Elevation | 403.66 ft | T2 Flow | 8.66 ft³/s |

# Post-Development Conditions

Subsection: Outlet Input Data
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Structure ID: Riser - 1<br>Structure Type: Inlet Box | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.82 ft |
| Orifice Area | 16.0 ft² |
| Orifice Coefficient | 0.600 |
| Weir Length | 16.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| Structure ID: Orifice - 1<br>Structure Type: Orifice-Area | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Orifice Area | 1.3 ft² |
| Top Elevation | 407.53 ft |
| Datum Elevation | 407.36 ft |
| Orifice Coefficient | 0.600 |

| Structure ID: Weir - 1<br>Structure Type: Rectangular Weir | |
|---|---|
| Number of Openings | 1 |
| Elevation | 407.20 ft |
| Weir Length | 4.00 ft |
| Weir Coefficient | 3.00 (ft^0.5)/s |

| Structure ID: Orifice - 2<br>Structure Type: Orifice-Circular | |
|---|---|
| Number of Openings | 1 |
| Elevation | 405.00 ft |
| Orifice Diameter | 8.0 in |
| Orifice Coefficient | 0.600 |

| Structure ID: TW<br>Structure Type: TW Setup, DS Channel | |
|---|---|
| Tailwater Type | Free Outfall |

| Convergence Tolerances |
|---|

| Convergence Tolerances | |
|---|---|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.100 $ft^3/s$ |
| Flow Tolerance (Maximum) | 10.000 $ft^3/s$ |

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = ()
---
Upstream ID =
Downstream ID =

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|

Contributing Structures

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 405.00 | 0.00 | (N/A) | 0.00 |
| 405.10 | 0.08 | (N/A) | 0.00 |
| 405.20 | 0.08 | (N/A) | 0.00 |
| 405.30 | 0.18 | (N/A) | 0.00 |
| 405.40 | 0.37 | (N/A) | 0.00 |
| 405.50 | 0.57 | (N/A) | 0.00 |
| 405.60 | 0.88 | (N/A) | 0.00 |
| 405.70 | 1.00 | (N/A) | 0.00 |
| 405.80 | 1.11 | (N/A) | 0.00 |
| 405.90 | 1.28 | (N/A) | 0.00 |
| 406.00 | 1.45 | (N/A) | 0.00 |
| 406.10 | 1.55 | (N/A) | 0.00 |
| 406.20 | 1.55 | (N/A) | 0.00 |
| 406.30 | 1.65 | (N/A) | 0.00 |
| 406.40 | 1.73 | (N/A) | 0.00 |
| 406.50 | 1.85 | (N/A) | 0.00 |
| 406.60 | 1.85 | (N/A) | 0.00 |
| 406.70 | 1.96 | (N/A) | 0.00 |
| 406.80 | 2.03 | (N/A) | 0.00 |
| 406.90 | 2.03 | (N/A) | 0.00 |
| 407.00 | 2.17 | (N/A) | 0.00 |
| 407.10 | 2.17 | (N/A) | 0.00 |
| 407.20 | 2.30 | (N/A) | 0.00 |
| 407.30 | 3.53 | (N/A) | 0.00 |
| 407.40 | 5.10 | (N/A) | 0.00 |
| 407.50 | 6.77 | (N/A) | 0.00 |
| 407.60 | 5.61 | (N/A) | 0.00 |
| 407.70 | 6.37 | (N/A) | 0.00 |
| 407.80 | 6.77 | (N/A) | 0.00 |
| 407.82 | 6.96 | (N/A) | 0.00 |
| 407.90 | 8.34 | (N/A) | 0.00 |
| 408.00 | 11.49 | (N/A) | 0.00 |
| 408.10 | 14.34 | (N/A) | 0.00 |
| 408.20 | 19.15 | (N/A) | 0.00 |
| 408.30 | 21.28 | (N/A) | 0.00 |
| 408.40 | 22.85 | (N/A) | 0.00 |
| 408.50 | 23.50 | (N/A) | 0.00 |
| 408.60 | 23.70 | (N/A) | 0.00 |
| 408.70 | 23.91 | (N/A) | 0.00 |
| 408.80 | 24.12 | (N/A) | 0.00 |
| 408.90 | 24.32 | (N/A) | 0.00 |
| 409.00 | 24.52 | (N/A) | 0.00 |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow ($ft^3/s$) | Tailwater Elevation (ft) | Convergence Error (ft) |
|---|---|---|---|
| 409.10 | 24.72 | (N/A) | 0.00 |
| 409.20 | 24.92 | (N/A) | 0.00 |
| 409.30 | 25.12 | (N/A) | 0.00 |
| 409.40 | 25.31 | (N/A) | 0.00 |
| 409.50 | 25.50 | (N/A) | 0.00 |
| 409.60 | 25.70 | (N/A) | 0.00 |
| 409.70 | 25.89 | (N/A) | 0.00 |
| 409.80 | 26.08 | (N/A) | 0.00 |
| 409.90 | 26.27 | (N/A) | 0.00 |
| 410.00 | 26.45 | (N/A) | 0.00 |

| Contributing Structures |
|---|
| (no Q: Weir - 1,Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Orifice - 2,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Weir - 1,Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |

Composite Outflow Summary

| Contributing Structures |
| --- |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1,Riser - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Orifice - 1,Riser - 1,Orifice - 2,Culvert - 1 (no Q: Weir - 1) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

# Post-Development Conditions

Subsection: Composite Rating Curve
Label: Outfall Structure
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

Composite Outflow Summary

| Contributing Structures |
|---|
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |
| Riser - 1,Culvert - 1 (no Q: Weir - 1,Orifice - 1,Orifice - 2) |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond)
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.000 | 0.023 | 0.00 | 0.00 | 0.00 |
| 405.10 | 0.08 | 0.002 | 0.024 | 0.00 | 0.08 | 1.79 |
| 405.20 | 0.08 | 0.005 | 0.025 | 0.00 | 0.08 | 3.56 |
| 405.30 | 0.18 | 0.007 | 0.026 | 0.00 | 0.18 | 5.50 |
| 405.40 | 0.37 | 0.010 | 0.027 | 0.00 | 0.37 | 7.60 |
| 405.50 | 0.57 | 0.013 | 0.028 | 0.00 | 0.57 | 9.78 |
| 405.60 | 0.88 | 0.015 | 0.029 | 0.00 | 0.88 | 12.13 |
| 405.70 | 1.00 | 0.018 | 0.030 | 0.00 | 1.00 | 14.37 |
| 405.80 | 1.11 | 0.021 | 0.031 | 0.00 | 1.11 | 16.67 |
| 405.90 | 1.28 | 0.025 | 0.032 | 0.00 | 1.28 | 19.09 |
| 406.00 | 1.45 | 0.028 | 0.033 | 0.00 | 1.45 | 21.60 |
| 406.10 | 1.55 | 0.031 | 0.034 | 0.00 | 1.55 | 24.12 |
| 406.20 | 1.55 | 0.035 | 0.035 | 0.00 | 1.55 | 26.60 |
| 406.30 | 1.65 | 0.038 | 0.036 | 0.00 | 1.65 | 29.27 |
| 406.40 | 1.73 | 0.042 | 0.037 | 0.00 | 1.73 | 31.98 |
| 406.50 | 1.85 | 0.045 | 0.038 | 0.00 | 1.85 | 34.82 |
| 406.60 | 1.85 | 0.049 | 0.039 | 0.00 | 1.85 | 37.62 |
| 406.70 | 1.96 | 0.053 | 0.040 | 0.00 | 1.96 | 40.62 |
| 406.80 | 2.03 | 0.057 | 0.041 | 0.00 | 2.03 | 43.64 |
| 406.90 | 2.03 | 0.062 | 0.043 | 0.00 | 2.03 | 46.69 |
| 407.00 | 2.17 | 0.066 | 0.044 | 0.00 | 2.17 | 49.96 |
| 407.10 | 2.17 | 0.070 | 0.045 | 0.00 | 2.17 | 53.18 |
| 407.20 | 2.30 | 0.075 | 0.046 | 0.00 | 2.30 | 56.61 |
| 407.30 | 3.53 | 0.080 | 0.047 | 0.00 | 3.53 | 61.25 |
| 407.40 | 5.10 | 0.084 | 0.049 | 0.00 | 5.10 | 66.31 |
| 407.50 | 6.77 | 0.089 | 0.050 | 0.00 | 6.77 | 71.57 |
| 407.60 | 5.61 | 0.094 | 0.051 | 0.00 | 5.61 | 74.09 |
| 407.70 | 6.37 | 0.100 | 0.053 | 0.00 | 6.37 | 78.63 |
| 407.80 | 6.77 | 0.105 | 0.054 | 0.00 | 6.77 | 82.91 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 2 years
Label: Detention Pond Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 407.90 | 8.77 | 0.110 | 0.056 | 0.00 | 8.77 | 88.90 |
| 408.00 | 12.12 | 0.116 | 0.057 | 0.00 | 12.12 | 96.32 |
| 408.10 | 15.45 | 0.122 | 0.058 | 0.00 | 15.45 | 103.83 |
| 408.20 | 19.51 | 0.128 | 0.059 | 0.00 | 19.51 | 112.15 |
| 408.30 | 22.26 | 0.134 | 0.061 | 0.00 | 22.26 | 119.26 |
| 408.40 | 23.08 | 0.140 | 0.062 | 0.00 | 23.08 | 124.51 |
| 408.50 | 23.50 | 0.146 | 0.063 | 0.00 | 23.50 | 129.46 |
| 408.60 | 23.70 | 0.152 | 0.064 | 0.00 | 23.70 | 134.30 |
| 408.70 | 23.91 | 0.159 | 0.066 | 0.00 | 23.91 | 139.22 |
| 408.80 | 24.12 | 0.165 | 0.067 | 0.00 | 24.12 | 144.23 |
| 408.90 | 24.32 | 0.172 | 0.068 | 0.00 | 24.32 | 149.34 |
| 409.00 | 24.52 | 0.179 | 0.070 | 0.00 | 24.52 | 154.55 |
| 409.10 | 24.72 | 0.186 | 0.071 | 0.00 | 24.72 | 159.84 |
| 409.20 | 24.92 | 0.193 | 0.072 | 0.00 | 24.92 | 165.25 |
| 409.30 | 25.12 | 0.201 | 0.074 | 0.00 | 25.12 | 170.75 |
| 409.40 | 25.31 | 0.208 | 0.075 | 0.00 | 25.31 | 176.36 |
| 409.50 | 25.50 | 0.216 | 0.077 | 0.00 | 25.50 | 182.07 |
| 409.60 | 25.70 | 0.223 | 0.078 | 0.00 | 25.70 | 187.90 |
| 409.70 | 25.89 | 0.231 | 0.080 | 0.00 | 25.89 | 193.83 |
| 409.80 | 26.08 | 0.239 | 0.081 | 0.00 | 26.08 | 199.86 |
| 409.90 | 26.27 | 0.248 | 0.083 | 0.00 | 26.27 | 206.01 |
| 410.00 | 26.45 | 0.256 | 0.084 | 0.00 | 26.45 | 212.26 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond)
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.000 | 0.023 | 0.00 | 0.00 | 0.00 |
| 405.10 | 0.08 | 0.002 | 0.024 | 0.00 | 0.08 | 1.79 |
| 405.20 | 0.08 | 0.005 | 0.025 | 0.00 | 0.08 | 3.56 |
| 405.30 | 0.18 | 0.007 | 0.026 | 0.00 | 0.18 | 5.50 |
| 405.40 | 0.37 | 0.010 | 0.027 | 0.00 | 0.37 | 7.60 |
| 405.50 | 0.57 | 0.013 | 0.028 | 0.00 | 0.57 | 9.78 |
| 405.60 | 0.88 | 0.015 | 0.029 | 0.00 | 0.88 | 12.13 |
| 405.70 | 1.00 | 0.018 | 0.030 | 0.00 | 1.00 | 14.37 |
| 405.80 | 1.11 | 0.021 | 0.031 | 0.00 | 1.11 | 16.67 |
| 405.90 | 1.28 | 0.025 | 0.032 | 0.00 | 1.28 | 19.09 |
| 406.00 | 1.45 | 0.028 | 0.033 | 0.00 | 1.45 | 21.60 |
| 406.10 | 1.55 | 0.031 | 0.034 | 0.00 | 1.55 | 24.12 |
| 406.20 | 1.55 | 0.035 | 0.035 | 0.00 | 1.55 | 26.60 |
| 406.30 | 1.65 | 0.038 | 0.036 | 0.00 | 1.65 | 29.27 |
| 406.40 | 1.73 | 0.042 | 0.037 | 0.00 | 1.73 | 31.98 |
| 406.50 | 1.85 | 0.045 | 0.038 | 0.00 | 1.85 | 34.82 |
| 406.60 | 1.85 | 0.049 | 0.039 | 0.00 | 1.85 | 37.62 |
| 406.70 | 1.96 | 0.053 | 0.040 | 0.00 | 1.96 | 40.62 |
| 406.80 | 2.03 | 0.057 | 0.041 | 0.00 | 2.03 | 43.64 |
| 406.90 | 2.03 | 0.062 | 0.043 | 0.00 | 2.03 | 46.69 |
| 407.00 | 2.17 | 0.066 | 0.044 | 0.00 | 2.17 | 49.96 |
| 407.10 | 2.17 | 0.070 | 0.045 | 0.00 | 2.17 | 53.18 |
| 407.20 | 2.30 | 0.075 | 0.046 | 0.00 | 2.30 | 56.61 |
| 407.30 | 3.53 | 0.080 | 0.047 | 0.00 | 3.53 | 61.25 |
| 407.40 | 5.10 | 0.084 | 0.049 | 0.00 | 5.10 | 66.31 |
| 407.50 | 6.77 | 0.089 | 0.050 | 0.00 | 6.77 | 71.57 |
| 407.60 | 5.61 | 0.094 | 0.051 | 0.00 | 5.61 | 74.09 |
| 407.70 | 6.37 | 0.100 | 0.053 | 0.00 | 6.37 | 78.63 |
| 407.80 | 6.77 | 0.105 | 0.054 | 0.00 | 6.77 | 82.91 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 10 years
Label: Detention Pond Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 407.90 | 8.77 | 0.110 | 0.056 | 0.00 | 8.77 | 88.90 |
| 408.00 | 12.12 | 0.116 | 0.057 | 0.00 | 12.12 | 96.32 |
| 408.10 | 15.45 | 0.122 | 0.058 | 0.00 | 15.45 | 103.83 |
| 408.20 | 19.51 | 0.128 | 0.059 | 0.00 | 19.51 | 112.15 |
| 408.30 | 22.26 | 0.134 | 0.061 | 0.00 | 22.26 | 119.26 |
| 408.40 | 23.08 | 0.140 | 0.062 | 0.00 | 23.08 | 124.51 |
| 408.50 | 23.50 | 0.146 | 0.063 | 0.00 | 23.50 | 129.46 |
| 408.60 | 23.70 | 0.152 | 0.064 | 0.00 | 23.70 | 134.30 |
| 408.70 | 23.91 | 0.159 | 0.066 | 0.00 | 23.91 | 139.22 |
| 408.80 | 24.12 | 0.165 | 0.067 | 0.00 | 24.12 | 144.23 |
| 408.90 | 24.32 | 0.172 | 0.068 | 0.00 | 24.32 | 149.34 |
| 409.00 | 24.52 | 0.179 | 0.070 | 0.00 | 24.52 | 154.55 |
| 409.10 | 24.72 | 0.186 | 0.071 | 0.00 | 24.72 | 159.84 |
| 409.20 | 24.92 | 0.193 | 0.072 | 0.00 | 24.92 | 165.25 |
| 409.30 | 25.12 | 0.201 | 0.074 | 0.00 | 25.12 | 170.75 |
| 409.40 | 25.31 | 0.208 | 0.075 | 0.00 | 25.31 | 176.36 |
| 409.50 | 25.50 | 0.216 | 0.077 | 0.00 | 25.50 | 182.07 |
| 409.60 | 25.70 | 0.223 | 0.078 | 0.00 | 25.70 | 187.90 |
| 409.70 | 25.89 | 0.231 | 0.080 | 0.00 | 25.89 | 193.83 |
| 409.80 | 26.08 | 0.239 | 0.081 | 0.00 | 26.08 | 199.86 |
| 409.90 | 26.27 | 0.248 | 0.083 | 0.00 | 26.27 | 206.01 |
| 410.00 | 26.45 | 0.256 | 0.084 | 0.00 | 26.45 | 212.26 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond)
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.000 | 0.023 | 0.00 | 0.00 | 0.00 |
| 405.10 | 0.08 | 0.002 | 0.024 | 0.00 | 0.08 | 1.79 |
| 405.20 | 0.08 | 0.005 | 0.025 | 0.00 | 0.08 | 3.56 |
| 405.30 | 0.18 | 0.007 | 0.026 | 0.00 | 0.18 | 5.50 |
| 405.40 | 0.37 | 0.010 | 0.027 | 0.00 | 0.37 | 7.60 |
| 405.50 | 0.57 | 0.013 | 0.028 | 0.00 | 0.57 | 9.78 |
| 405.60 | 0.88 | 0.015 | 0.029 | 0.00 | 0.88 | 12.13 |
| 405.70 | 1.00 | 0.018 | 0.030 | 0.00 | 1.00 | 14.37 |
| 405.80 | 1.11 | 0.021 | 0.031 | 0.00 | 1.11 | 16.67 |
| 405.90 | 1.28 | 0.025 | 0.032 | 0.00 | 1.28 | 19.09 |
| 406.00 | 1.45 | 0.028 | 0.033 | 0.00 | 1.45 | 21.60 |
| 406.10 | 1.55 | 0.031 | 0.034 | 0.00 | 1.55 | 24.12 |
| 406.20 | 1.55 | 0.035 | 0.035 | 0.00 | 1.55 | 26.60 |
| 406.30 | 1.65 | 0.038 | 0.036 | 0.00 | 1.65 | 29.27 |
| 406.40 | 1.73 | 0.042 | 0.037 | 0.00 | 1.73 | 31.98 |
| 406.50 | 1.85 | 0.045 | 0.038 | 0.00 | 1.85 | 34.82 |
| 406.60 | 1.85 | 0.049 | 0.039 | 0.00 | 1.85 | 37.62 |
| 406.70 | 1.96 | 0.053 | 0.040 | 0.00 | 1.96 | 40.62 |
| 406.80 | 2.03 | 0.057 | 0.041 | 0.00 | 2.03 | 43.64 |
| 406.90 | 2.03 | 0.062 | 0.043 | 0.00 | 2.03 | 46.69 |
| 407.00 | 2.17 | 0.066 | 0.044 | 0.00 | 2.17 | 49.96 |
| 407.10 | 2.17 | 0.070 | 0.045 | 0.00 | 2.17 | 53.18 |
| 407.20 | 2.30 | 0.075 | 0.046 | 0.00 | 2.30 | 56.61 |
| 407.30 | 3.53 | 0.080 | 0.047 | 0.00 | 3.53 | 61.25 |
| 407.40 | 5.10 | 0.084 | 0.049 | 0.00 | 5.10 | 66.31 |
| 407.50 | 6.77 | 0.089 | 0.050 | 0.00 | 6.77 | 71.57 |
| 407.60 | 5.61 | 0.094 | 0.051 | 0.00 | 5.61 | 74.09 |
| 407.70 | 6.37 | 0.100 | 0.053 | 0.00 | 6.37 | 78.63 |
| 407.80 | 6.77 | 0.105 | 0.054 | 0.00 | 6.77 | 82.91 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 25 years
Label: Detention Pond Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| Elevation (ft) | Outflow ($ft^3/s$) | Storage (ac-ft) | Area (acres) | Infiltration ($ft^3/s$) | Flow (Total) ($ft^3/s$) | 2S/t + O ($ft^3/s$) |
|---|---|---|---|---|---|---|
| 407.90 | 8.77 | 0.110 | 0.056 | 0.00 | 8.77 | 88.90 |
| 408.00 | 12.12 | 0.116 | 0.057 | 0.00 | 12.12 | 96.32 |
| 408.10 | 15.45 | 0.122 | 0.058 | 0.00 | 15.45 | 103.83 |
| 408.20 | 19.51 | 0.128 | 0.059 | 0.00 | 19.51 | 112.15 |
| 408.30 | 22.26 | 0.134 | 0.061 | 0.00 | 22.26 | 119.26 |
| 408.40 | 23.08 | 0.140 | 0.062 | 0.00 | 23.08 | 124.51 |
| 408.50 | 23.50 | 0.146 | 0.063 | 0.00 | 23.50 | 129.46 |
| 408.60 | 23.70 | 0.152 | 0.064 | 0.00 | 23.70 | 134.30 |
| 408.70 | 23.91 | 0.159 | 0.066 | 0.00 | 23.91 | 139.22 |
| 408.80 | 24.12 | 0.165 | 0.067 | 0.00 | 24.12 | 144.23 |
| 408.90 | 24.32 | 0.172 | 0.068 | 0.00 | 24.32 | 149.34 |
| 409.00 | 24.52 | 0.179 | 0.070 | 0.00 | 24.52 | 154.55 |
| 409.10 | 24.72 | 0.186 | 0.071 | 0.00 | 24.72 | 159.84 |
| 409.20 | 24.92 | 0.193 | 0.072 | 0.00 | 24.92 | 165.25 |
| 409.30 | 25.12 | 0.201 | 0.074 | 0.00 | 25.12 | 170.75 |
| 409.40 | 25.31 | 0.208 | 0.075 | 0.00 | 25.31 | 176.36 |
| 409.50 | 25.50 | 0.216 | 0.077 | 0.00 | 25.50 | 182.07 |
| 409.60 | 25.70 | 0.223 | 0.078 | 0.00 | 25.70 | 187.90 |
| 409.70 | 25.89 | 0.231 | 0.080 | 0.00 | 25.89 | 193.83 |
| 409.80 | 26.08 | 0.239 | 0.081 | 0.00 | 26.08 | 199.86 |
| 409.90 | 26.27 | 0.248 | 0.083 | 0.00 | 26.27 | 206.01 |
| 410.00 | 26.45 | 0.256 | 0.084 | 0.00 | 26.45 | 212.26 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond)
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.000 | 0.023 | 0.00 | 0.00 | 0.00 |
| 405.10 | 0.08 | 0.002 | 0.024 | 0.00 | 0.08 | 1.79 |
| 405.20 | 0.08 | 0.005 | 0.025 | 0.00 | 0.08 | 3.56 |
| 405.30 | 0.18 | 0.007 | 0.026 | 0.00 | 0.18 | 5.50 |
| 405.40 | 0.37 | 0.010 | 0.027 | 0.00 | 0.37 | 7.60 |
| 405.50 | 0.57 | 0.013 | 0.028 | 0.00 | 0.57 | 9.78 |
| 405.60 | 0.88 | 0.015 | 0.029 | 0.00 | 0.88 | 12.13 |
| 405.70 | 1.00 | 0.018 | 0.030 | 0.00 | 1.00 | 14.37 |
| 405.80 | 1.11 | 0.021 | 0.031 | 0.00 | 1.11 | 16.67 |
| 405.90 | 1.28 | 0.025 | 0.032 | 0.00 | 1.28 | 19.09 |
| 406.00 | 1.45 | 0.028 | 0.033 | 0.00 | 1.45 | 21.60 |
| 406.10 | 1.55 | 0.031 | 0.034 | 0.00 | 1.55 | 24.12 |
| 406.20 | 1.55 | 0.035 | 0.035 | 0.00 | 1.55 | 26.60 |
| 406.30 | 1.65 | 0.038 | 0.036 | 0.00 | 1.65 | 29.27 |
| 406.40 | 1.73 | 0.042 | 0.037 | 0.00 | 1.73 | 31.98 |
| 406.50 | 1.85 | 0.045 | 0.038 | 0.00 | 1.85 | 34.82 |
| 406.60 | 1.85 | 0.049 | 0.039 | 0.00 | 1.85 | 37.62 |
| 406.70 | 1.96 | 0.053 | 0.040 | 0.00 | 1.96 | 40.62 |
| 406.80 | 2.03 | 0.057 | 0.041 | 0.00 | 2.03 | 43.64 |
| 406.90 | 2.03 | 0.062 | 0.043 | 0.00 | 2.03 | 46.69 |
| 407.00 | 2.17 | 0.066 | 0.044 | 0.00 | 2.17 | 49.96 |
| 407.10 | 2.17 | 0.070 | 0.045 | 0.00 | 2.17 | 53.18 |
| 407.20 | 2.30 | 0.075 | 0.046 | 0.00 | 2.30 | 56.61 |
| 407.30 | 3.53 | 0.080 | 0.047 | 0.00 | 3.53 | 61.25 |
| 407.40 | 5.10 | 0.084 | 0.049 | 0.00 | 5.10 | 66.31 |
| 407.50 | 6.77 | 0.089 | 0.050 | 0.00 | 6.77 | 71.57 |
| 407.60 | 5.61 | 0.094 | 0.051 | 0.00 | 5.61 | 74.09 |
| 407.70 | 6.37 | 0.100 | 0.053 | 0.00 | 6.37 | 78.63 |
| 407.80 | 6.77 | 0.105 | 0.054 | 0.00 | 6.77 | 82.91 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 50 years
Label: Detention Pond Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 407.90 | 8.77 | 0.110 | 0.056 | 0.00 | 8.77 | 88.90 |
| 408.00 | 12.12 | 0.116 | 0.057 | 0.00 | 12.12 | 96.32 |
| 408.10 | 15.45 | 0.122 | 0.058 | 0.00 | 15.45 | 103.83 |
| 408.20 | 19.51 | 0.128 | 0.059 | 0.00 | 19.51 | 112.15 |
| 408.30 | 22.26 | 0.134 | 0.061 | 0.00 | 22.26 | 119.26 |
| 408.40 | 23.08 | 0.140 | 0.062 | 0.00 | 23.08 | 124.51 |
| 408.50 | 23.50 | 0.146 | 0.063 | 0.00 | 23.50 | 129.46 |
| 408.60 | 23.70 | 0.152 | 0.064 | 0.00 | 23.70 | 134.30 |
| 408.70 | 23.91 | 0.159 | 0.066 | 0.00 | 23.91 | 139.22 |
| 408.80 | 24.12 | 0.165 | 0.067 | 0.00 | 24.12 | 144.23 |
| 408.90 | 24.32 | 0.172 | 0.068 | 0.00 | 24.32 | 149.34 |
| 409.00 | 24.52 | 0.179 | 0.070 | 0.00 | 24.52 | 154.55 |
| 409.10 | 24.72 | 0.186 | 0.071 | 0.00 | 24.72 | 159.84 |
| 409.20 | 24.92 | 0.193 | 0.072 | 0.00 | 24.92 | 165.25 |
| 409.30 | 25.12 | 0.201 | 0.074 | 0.00 | 25.12 | 170.75 |
| 409.40 | 25.31 | 0.208 | 0.075 | 0.00 | 25.31 | 176.36 |
| 409.50 | 25.50 | 0.216 | 0.077 | 0.00 | 25.50 | 182.07 |
| 409.60 | 25.70 | 0.223 | 0.078 | 0.00 | 25.70 | 187.90 |
| 409.70 | 25.89 | 0.231 | 0.080 | 0.00 | 25.89 | 193.83 |
| 409.80 | 26.08 | 0.239 | 0.081 | 0.00 | 26.08 | 199.86 |
| 409.90 | 26.27 | 0.248 | 0.083 | 0.00 | 26.27 | 206.01 |
| 410.00 | 26.45 | 0.256 | 0.084 | 0.00 | 26.45 | 212.26 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond)
Label: Detention Pond
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 405.00 | 0.00 | 0.000 | 0.023 | 0.00 | 0.00 | 0.00 |
| 405.10 | 0.08 | 0.002 | 0.024 | 0.00 | 0.08 | 1.79 |
| 405.20 | 0.08 | 0.005 | 0.025 | 0.00 | 0.08 | 3.56 |
| 405.30 | 0.18 | 0.007 | 0.026 | 0.00 | 0.18 | 5.50 |
| 405.40 | 0.37 | 0.010 | 0.027 | 0.00 | 0.37 | 7.60 |
| 405.50 | 0.57 | 0.013 | 0.028 | 0.00 | 0.57 | 9.78 |
| 405.60 | 0.88 | 0.015 | 0.029 | 0.00 | 0.88 | 12.13 |
| 405.70 | 1.00 | 0.018 | 0.030 | 0.00 | 1.00 | 14.37 |
| 405.80 | 1.11 | 0.021 | 0.031 | 0.00 | 1.11 | 16.67 |
| 405.90 | 1.28 | 0.025 | 0.032 | 0.00 | 1.28 | 19.09 |
| 406.00 | 1.45 | 0.028 | 0.033 | 0.00 | 1.45 | 21.60 |
| 406.10 | 1.55 | 0.031 | 0.034 | 0.00 | 1.55 | 24.12 |
| 406.20 | 1.55 | 0.035 | 0.035 | 0.00 | 1.55 | 26.60 |
| 406.30 | 1.65 | 0.038 | 0.036 | 0.00 | 1.65 | 29.27 |
| 406.40 | 1.73 | 0.042 | 0.037 | 0.00 | 1.73 | 31.98 |
| 406.50 | 1.85 | 0.045 | 0.038 | 0.00 | 1.85 | 34.82 |
| 406.60 | 1.85 | 0.049 | 0.039 | 0.00 | 1.85 | 37.62 |
| 406.70 | 1.96 | 0.053 | 0.040 | 0.00 | 1.96 | 40.62 |
| 406.80 | 2.03 | 0.057 | 0.041 | 0.00 | 2.03 | 43.64 |
| 406.90 | 2.03 | 0.062 | 0.043 | 0.00 | 2.03 | 46.69 |
| 407.00 | 2.17 | 0.066 | 0.044 | 0.00 | 2.17 | 49.96 |
| 407.10 | 2.17 | 0.070 | 0.045 | 0.00 | 2.17 | 53.18 |
| 407.20 | 2.30 | 0.075 | 0.046 | 0.00 | 2.30 | 56.61 |
| 407.30 | 3.53 | 0.080 | 0.047 | 0.00 | 3.53 | 61.25 |
| 407.40 | 5.10 | 0.084 | 0.049 | 0.00 | 5.10 | 66.31 |
| 407.50 | 6.77 | 0.089 | 0.050 | 0.00 | 6.77 | 71.57 |
| 407.60 | 5.61 | 0.094 | 0.051 | 0.00 | 5.61 | 74.09 |
| 407.70 | 6.37 | 0.100 | 0.053 | 0.00 | 6.37 | 78.63 |
| 407.80 | 6.77 | 0.105 | 0.054 | 0.00 | 6.77 | 82.91 |

# Post-Development Conditions

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 100 years
Label: Detention Pond Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

| Elevation (ft) | Outflow (ft³/s) | Storage (ac-ft) | Area (acres) | Infiltration (ft³/s) | Flow (Total) (ft³/s) | 2S/t + O (ft³/s) |
|---|---|---|---|---|---|---|
| 407.82 | 6.96 | 0.106 | 0.054 | 0.00 | 6.96 | 83.89 |
| 407.90 | 8.34 | 0.110 | 0.056 | 0.00 | 8.34 | 88.46 |
| 408.00 | 11.49 | 0.116 | 0.057 | 0.00 | 11.49 | 95.70 |
| 408.10 | 14.34 | 0.122 | 0.058 | 0.00 | 14.34 | 102.72 |
| 408.20 | 19.15 | 0.128 | 0.059 | 0.00 | 19.15 | 111.79 |
| 408.30 | 21.28 | 0.134 | 0.061 | 0.00 | 21.28 | 118.28 |
| 408.40 | 22.85 | 0.140 | 0.062 | 0.00 | 22.85 | 124.28 |
| 408.50 | 23.50 | 0.146 | 0.063 | 0.00 | 23.50 | 129.46 |
| 408.60 | 23.70 | 0.152 | 0.064 | 0.00 | 23.70 | 134.30 |
| 408.70 | 23.91 | 0.159 | 0.066 | 0.00 | 23.91 | 139.22 |
| 408.80 | 24.12 | 0.165 | 0.067 | 0.00 | 24.12 | 144.23 |
| 408.90 | 24.32 | 0.172 | 0.068 | 0.00 | 24.32 | 149.34 |
| 409.00 | 24.52 | 0.179 | 0.070 | 0.00 | 24.52 | 154.55 |
| 409.10 | 24.72 | 0.186 | 0.071 | 0.00 | 24.72 | 159.84 |
| 409.20 | 24.92 | 0.193 | 0.072 | 0.00 | 24.92 | 165.25 |
| 409.30 | 25.12 | 0.201 | 0.074 | 0.00 | 25.12 | 170.75 |
| 409.40 | 25.31 | 0.208 | 0.075 | 0.00 | 25.31 | 176.36 |
| 409.50 | 25.50 | 0.216 | 0.077 | 0.00 | 25.50 | 182.07 |
| 409.60 | 25.70 | 0.223 | 0.078 | 0.00 | 25.70 | 187.90 |
| 409.70 | 25.89 | 0.231 | 0.080 | 0.00 | 25.89 | 193.83 |
| 409.80 | 26.08 | 0.239 | 0.081 | 0.00 | 26.08 | 199.86 |
| 409.90 | 26.27 | 0.248 | 0.083 | 0.00 | 26.27 | 206.01 |
| 410.00 | 26.45 | 0.256 | 0.084 | 0.00 | 26.45 | 212.26 |

# Post-Development Conditions

Subsection: Detention Time
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Approximate Detention Times | |
|---|---|
| Time to Peak (Outflow + Infiltration, Peak to Peak Detention Time) | 12.267 hours |
| Time to Peak (Inflow, Peak to Peak Detention Time) | 12.100 hours |
| Detention Time (Peak to Peak) | 0.167 hours |
| Time to Centroid (Outflow) | 14.332 hours |
| Time to Centroid (Inflow) | 13.967 hours |
| Detention Time (Centroid to Centroid) | 0.365 hours |
| Weighted Average Plug Time | 0.368 hours |
| Maximum Plug Volume Plug Time | 0.260 hours |
| Maximum Inflow Plug Volume | 0.009 ac-ft |
| Time (Maximum Plug Volume, Start) | 12.100 hours |
| Time (Maximum Plug Volume, End) | 12.133 hours |

Subsection: Level Pool Pond Routing Summary
Return Event: 2 years
Label: Detention Pond (IN)
Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 3.18 ft³/s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 1.81 ft³/s | Time to Peak (Flow, Outlet) | 12.267 hours |

| | |
|---|---|
| Elevation (Water Surface, Peak) | 406.46 ft |
| Volume (Peak) | 0.044 ac-ft |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.261 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.261 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

# Post-Development Conditions

Subsection: Detention Time
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Approximate Detention Times | |
|---|---|
| Time to Peak (Outflow + Infiltration, Peak to Peak Detention Time) | 12.200 hours |
| Time to Peak (Inflow, Peak to Peak Detention Time) | 12.100 hours |
| Detention Time (Peak to Peak) | 0.100 hours |
| Time to Centroid (Outflow) | 14.075 hours |
| Time to Centroid (Inflow) | 13.710 hours |
| Detention Time (Centroid to Centroid) | 0.365 hours |
| Weighted Average Plug Time | 0.369 hours |
| Maximum Plug Volume Plug Time | 0.295 hours |
| Maximum Inflow Plug Volume | 0.015 ac-ft |
| Time (Maximum Plug Volume, Start) | 12.100 hours |
| Time (Maximum Plug Volume, End) | 12.133 hours |

# Post-Development Conditions

Subsection: Level Pool Pond Routing Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 5.43 ft³/s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 3.73 ft³/s | Time to Peak (Flow, Outlet) | 12.200 hours |

| | |
|---|---|
| Elevation (Water Surface, Peak) | 407.31 ft |
| Volume (Peak) | 0.080 ac-ft |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.446 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.446 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

# Post-Development Conditions

Subsection: Detention Time
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Approximate Detention Times | |
|---|---|
| Time to Peak (Outflow + Infiltration, Peak to Peak Detention Time) | 12.167 hours |
| Time to Peak (Inflow, Peak to Peak Detention Time) | 12.100 hours |
| Detention Time (Peak to Peak) | 0.067 hours |
| Time to Centroid (Outflow) | 13.947 hours |
| Time to Centroid (Inflow) | 13.611 hours |
| Detention Time (Centroid to Centroid) | 0.336 hours |
| Weighted Average Plug Time | 0.339 hours |
| Maximum Plug Volume Plug Time | 0.235 hours |
| Maximum Inflow Plug Volume | 0.018 ac-ft |
| Time (Maximum Plug Volume, Start) | 12.100 hours |
| Time (Maximum Plug Volume, End) | 12.133 hours |

# Post-Development Conditions

Subsection: Level Pool Pond Routing Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 6.67 ft³/s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 5.83 ft³/s | Time to Peak (Flow, Outlet) | 12.167 hours |

| | |
|---|---|
| Elevation (Water Surface, Peak) | 407.44 ft |
| Volume (Peak) | 0.086 ac-ft |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.550 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.550 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

# Post-Development Conditions

Subsection: Detention Time
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Approximate Detention Times | |
|---|---|
| Time to Peak (Outflow + Infiltration, Peak to Peak Detention Time) | 12.167 hours |
| Time to Peak (Inflow, Peak to Peak Detention Time) | 12.100 hours |
| Detention Time (Peak to Peak) | 0.067 hours |
| Time to Centroid (Outflow) | 13.821 hours |
| Time to Centroid (Inflow) | 13.511 hours |
| Detention Time (Centroid to Centroid) | 0.310 hours |
| Weighted Average Plug Time | 0.313 hours |
| Maximum Plug Volume Plug Time | 0.181 hours |
| Maximum Inflow Plug Volume | 0.022 ac-ft |
| Time (Maximum Plug Volume, Start) | 12.067 hours |
| Time (Maximum Plug Volume, End) | 12.100 hours |

# Post-Development Conditions

Subsection: Level Pool Pond Routing Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 8.19 ft³/s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 6.44 ft³/s | Time to Peak (Flow, Outlet) | 12.167 hours |

| | |
|---|---|
| Elevation (Water Surface, Peak) | 407.72 ft |
| Volume (Peak) | 0.101 ac-ft |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.680 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.680 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

# Post-Development Conditions

Subsection: Detention Time
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Approximate Detention Times | |
|---|---|
| Time to Peak (Outflow + Infiltration, Peak to Peak Detention Time) | 12.167 hours |
| Time to Peak (Inflow, Peak to Peak Detention Time) | 12.100 hours |
| Detention Time (Peak to Peak) | 0.067 hours |
| Time to Centroid (Outflow) | 13.782 hours |
| Time to Centroid (Inflow) | 13.479 hours |
| Detention Time (Centroid to Centroid) | 0.303 hours |
| Weighted Average Plug Time | 0.306 hours |
| Maximum Plug Volume Plug Time | 0.179 hours |
| Maximum Inflow Plug Volume | 0.024 ac-ft |
| Time (Maximum Plug Volume, Start) | 12.067 hours |
| Time (Maximum Plug Volume, End) | 12.100 hours |

# Post-Development Conditions

Subsection: Level Pool Pond Routing Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| Infiltration | |
|---|---|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|---|---|
| Elevation (Water Surface, Initial) | 405.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft³/s |
| Flow (Initial Infiltration) | 0.00 ft³/s |
| Flow (Initial, Total) | 0.00 ft³/s |
| Time Increment | 0.033 hours |

| Inflow/Outflow Hydrograph Summary | | | |
|---|---|---|---|
| Flow (Peak In) | 8.75 ft³/s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 6.92 ft³/s | Time to Peak (Flow, Outlet) | 12.167 hours |

| | |
|---|---|
| Elevation (Water Surface, Peak) | 407.82 ft |
| Volume (Peak) | 0.106 ac-ft |

| Mass Balance (ac-ft) | |
|---|---|
| Volume (Initial) | 0.000 ac-ft |
| Volume (Total Inflow) | 0.728 ac-ft |
| Volume (Total Infiltration) | 0.000 ac-ft |
| Volume (Total Outlet Outflow) | 0.728 ac-ft |
| Volume (Retained) | 0.000 ac-ft |
| Volume (Unrouted) | 0.000 ac-ft |
| Error (Mass Balance) | 0.0 % |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 2 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

| | |
|---|---|
| Peak Discharge | 1.81 ft³/s |
| Time to Peak | 12.267 hours |
| Hydrograph Volume | 0.261 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| 9.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.733 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 |
| 9.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.067 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.233 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 |
| 10.400 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 10.567 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 10.733 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 |
| 10.900 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 |
| 11.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 11.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 11.400 | 0.08 | 0.09 | 0.10 | 0.11 | 0.13 |
| 11.567 | 0.14 | 0.16 | 0.18 | 0.22 | 0.28 |
| 11.733 | 0.33 | 0.40 | 0.47 | 0.54 | 0.65 |
| 11.900 | 0.78 | 0.89 | 0.98 | 1.10 | 1.31 |
| 12.067 | 1.50 | 1.55 | 1.65 | 1.72 | 1.77 |
| 12.233 | 1.80 | 1.81 | 1.79 | 1.77 | 1.74 |
| 12.400 | 1.71 | 1.68 | 1.65 | 1.59 | 1.55 |
| 12.567 | 1.55 | 1.49 | 1.40 | 1.28 | 1.18 |
| 12.733 | 1.09 | 1.03 | 0.98 | 0.92 | 0.85 |
| 12.900 | 0.74 | 0.66 | 0.59 | 0.55 | 0.52 |
| 13.067 | 0.49 | 0.46 | 0.44 | 0.43 | 0.41 |
| 13.233 | 0.40 | 0.38 | 0.37 | 0.37 | 0.36 |
| 13.400 | 0.35 | 0.34 | 0.34 | 0.33 | 0.33 |
| 13.567 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 13.733 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 13.900 | 0.28 | 0.28 | 0.27 | 0.27 | 0.27 |
| 14.067 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 14.233 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 14.400 | 0.24 | 0.23 | 0.23 | 0.23 | 0.23 |
| 14.567 | 0.23 | 0.23 | 0.22 | 0.22 | 0.22 |
| 14.733 | 0.22 | 0.22 | 0.21 | 0.21 | 0.21 |
| 14.900 | 0.21 | 0.21 | 0.21 | 0.20 | 0.20 |
| 15.067 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 2 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (4.3 in)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 15.233 | 0.19 | 0.19 | 0.19 | 0.19 | 0.18 |
| 15.400 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 15.567 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 15.733 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |
| 15.900 | 0.16 | 0.16 | 0.16 | 0.15 | 0.15 |
| 16.067 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 16.233 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 16.400 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 16.567 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 16.733 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 16.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 17.067 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 17.233 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 17.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 17.567 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.733 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.900 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 18.067 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 18.233 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 18.400 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 18.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 21.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 21.900 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 22.067 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 2 years

Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (4.3 in)

Scenario: Bryant, AR - Synthetic Curve, 2 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 22.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.400 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.567 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.733 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.900 | 0.06 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.400 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.567 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.733 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.900 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 24.067 | 0.05 | 0.04 | 0.04 | 0.04 | 0.03 |
| 24.233 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 |
| 24.400 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 |
| 24.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.400 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 10 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

| | |
|---|---|
| Peak Discharge | 3.73 ft³/s |
| Time to Peak | 12.200 hours |
| Hydrograph Volume | 0.446 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.867 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 8.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.700 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 8.867 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 9.033 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 |
| 9.200 | 0.04 | 0.04 | 0.05 | 0.05 | 0.05 |
| 9.367 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 9.533 | 0.06 | 0.06 | 0.06 | 0.06 | 0.07 |
| 9.700 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 |
| 9.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.367 | 0.08 | 0.08 | 0.08 | 0.09 | 0.10 |
| 10.533 | 0.11 | 0.11 | 0.12 | 0.13 | 0.14 |
| 10.700 | 0.14 | 0.15 | 0.16 | 0.16 | 0.17 |
| 10.867 | 0.18 | 0.18 | 0.19 | 0.20 | 0.21 |
| 11.033 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 |
| 11.200 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 |
| 11.367 | 0.34 | 0.35 | 0.37 | 0.38 | 0.40 |
| 11.533 | 0.42 | 0.45 | 0.48 | 0.53 | 0.59 |
| 11.700 | 0.70 | 0.82 | 0.91 | 0.98 | 1.05 |
| 11.867 | 1.14 | 1.27 | 1.43 | 1.55 | 1.66 |
| 12.033 | 1.85 | 1.99 | 2.11 | 2.24 | 3.29 |
| 12.200 | 3.73 | 3.56 | 3.29 | 3.01 | 2.77 |
| 12.367 | 2.54 | 2.31 | 2.27 | 2.23 | 2.18 |
| 12.533 | 2.17 | 2.15 | 2.05 | 2.03 | 2.01 |
| 12.700 | 1.96 | 1.87 | 1.85 | 1.80 | 1.72 |
| 12.867 | 1.66 | 1.59 | 1.55 | 1.55 | 1.47 |
| 13.033 | 1.37 | 1.26 | 1.16 | 1.09 | 1.04 |
| 13.200 | 0.99 | 0.94 | 0.89 | 0.82 | 0.74 |
| 13.367 | 0.68 | 0.63 | 0.60 | 0.57 | 0.56 |
| 13.533 | 0.54 | 0.53 | 0.52 | 0.51 | 0.50 |
| 13.700 | 0.49 | 0.48 | 0.48 | 0.47 | 0.46 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 10 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.867 | 0.45 | 0.45 | 0.44 | 0.43 | 0.43 |
| 14.033 | 0.42 | 0.42 | 0.41 | 0.40 | 0.40 |
| 14.200 | 0.39 | 0.39 | 0.39 | 0.38 | 0.38 |
| 14.367 | 0.38 | 0.37 | 0.37 | 0.37 | 0.36 |
| 14.533 | 0.36 | 0.36 | 0.35 | 0.35 | 0.35 |
| 14.700 | 0.34 | 0.34 | 0.34 | 0.34 | 0.33 |
| 14.867 | 0.33 | 0.33 | 0.32 | 0.32 | 0.32 |
| 15.033 | 0.32 | 0.31 | 0.31 | 0.31 | 0.30 |
| 15.200 | 0.30 | 0.30 | 0.30 | 0.29 | 0.29 |
| 15.367 | 0.29 | 0.28 | 0.28 | 0.28 | 0.27 |
| 15.533 | 0.27 | 0.27 | 0.27 | 0.26 | 0.26 |
| 15.700 | 0.26 | 0.25 | 0.25 | 0.25 | 0.25 |
| 15.867 | 0.24 | 0.24 | 0.24 | 0.23 | 0.23 |
| 16.033 | 0.23 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.200 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 16.367 | 0.21 | 0.20 | 0.20 | 0.20 | 0.20 |
| 16.533 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 16.700 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 16.867 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 17.033 | 0.18 | 0.18 | 0.18 | 0.18 | 0.17 |
| 17.200 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 17.367 | 0.17 | 0.17 | 0.17 | 0.16 | 0.16 |
| 17.533 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 17.700 | 0.16 | 0.15 | 0.15 | 0.15 | 0.15 |
| 17.867 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 18.033 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.200 | 0.14 | 0.14 | 0.14 | 0.13 | 0.13 |
| 18.367 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.533 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.700 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.867 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.033 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.200 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.367 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.533 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 19.700 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.867 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.033 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.200 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.367 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.533 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.700 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 10 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.0 in)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.867 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.033 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.200 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.367 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.533 | 0.10 | 0.10 | 0.10 | 0.09 | 0.09 |
| 21.700 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.867 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.033 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.200 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.367 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.533 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.700 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 22.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.367 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.533 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.700 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.367 | 0.08 | 0.08 | 0.07 | 0.06 | 0.06 |
| 24.533 | 0.05 | 0.05 | 0.04 | 0.04 | 0.04 |
| 24.700 | 0.03 | 0.03 | 0.03 | 0.03 | 0.02 |
| 24.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 25.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.367 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.533 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.867 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 25 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

| | |
|---|---|
| Peak Discharge | 5.83 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.550 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.267 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 7.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.267 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.433 | 0.03 | 0.03 | 0.03 | 0.04 | 0.04 |
| 8.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.933 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 |
| 9.100 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 |
| 9.267 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.600 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.767 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.933 | 0.08 | 0.09 | 0.10 | 0.11 | 0.11 |
| 10.100 | 0.12 | 0.13 | 0.13 | 0.14 | 0.14 |
| 10.267 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 |
| 10.433 | 0.18 | 0.19 | 0.20 | 0.21 | 0.22 |
| 10.600 | 0.22 | 0.23 | 0.24 | 0.25 | 0.25 |
| 10.767 | 0.26 | 0.27 | 0.27 | 0.28 | 0.29 |
| 10.933 | 0.30 | 0.30 | 0.31 | 0.32 | 0.32 |
| 11.100 | 0.33 | 0.34 | 0.35 | 0.37 | 0.38 |
| 11.267 | 0.40 | 0.41 | 0.43 | 0.45 | 0.47 |
| 11.433 | 0.49 | 0.51 | 0.53 | 0.55 | 0.59 |
| 11.600 | 0.65 | 0.73 | 0.82 | 0.91 | 0.97 |
| 11.767 | 1.05 | 1.14 | 1.27 | 1.43 | 1.54 |
| 11.933 | 1.56 | 1.71 | 1.86 | 2.03 | 2.21 |
| 12.100 | 4.02 | 5.61 | 5.83 | 5.27 | 4.61 |
| 12.267 | 4.06 | 3.62 | 3.33 | 3.06 | 2.79 |
| 12.433 | 2.54 | 2.30 | 2.26 | 2.21 | 2.17 |
| 12.600 | 2.17 | 2.11 | 2.03 | 2.03 | 2.00 |
| 12.767 | 1.95 | 1.87 | 1.85 | 1.82 | 1.73 |
| 12.933 | 1.68 | 1.62 | 1.56 | 1.55 | 1.52 |
| 13.100 | 1.45 | 1.34 | 1.25 | 1.17 | 1.10 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 25 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.267 | 1.06 | 1.01 | 0.97 | 0.93 | 0.90 |
| 13.433 | 0.85 | 0.78 | 0.73 | 0.69 | 0.66 |
| 13.600 | 0.63 | 0.61 | 0.60 | 0.58 | 0.57 |
| 13.767 | 0.56 | 0.55 | 0.55 | 0.54 | 0.53 |
| 13.933 | 0.52 | 0.52 | 0.51 | 0.50 | 0.50 |
| 14.100 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 14.267 | 0.46 | 0.46 | 0.45 | 0.45 | 0.44 |
| 14.433 | 0.44 | 0.44 | 0.43 | 0.43 | 0.42 |
| 14.600 | 0.42 | 0.42 | 0.41 | 0.41 | 0.41 |
| 14.767 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 |
| 14.933 | 0.39 | 0.38 | 0.38 | 0.38 | 0.37 |
| 15.100 | 0.37 | 0.37 | 0.36 | 0.36 | 0.36 |
| 15.267 | 0.35 | 0.35 | 0.34 | 0.34 | 0.34 |
| 15.433 | 0.33 | 0.33 | 0.33 | 0.32 | 0.32 |
| 15.600 | 0.32 | 0.31 | 0.31 | 0.31 | 0.30 |
| 15.767 | 0.30 | 0.30 | 0.29 | 0.29 | 0.28 |
| 15.933 | 0.28 | 0.28 | 0.27 | 0.27 | 0.27 |
| 16.100 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 16.267 | 0.25 | 0.25 | 0.25 | 0.24 | 0.24 |
| 16.433 | 0.24 | 0.24 | 0.24 | 0.23 | 0.23 |
| 16.600 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| 16.767 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.933 | 0.22 | 0.21 | 0.21 | 0.21 | 0.21 |
| 17.100 | 0.21 | 0.21 | 0.20 | 0.20 | 0.20 |
| 17.267 | 0.20 | 0.20 | 0.20 | 0.20 | 0.19 |
| 17.433 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 17.600 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 17.767 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 17.933 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 18.100 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.267 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.433 | 0.16 | 0.16 | 0.15 | 0.15 | 0.15 |
| 18.600 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.767 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.933 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 19.100 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.433 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.600 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 19.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 19.933 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.100 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 25 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (6.9 in)
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.267 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.433 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 20.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.767 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.933 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.100 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.267 | 0.12 | 0.12 | 0.12 | 0.12 | 0.11 |
| 21.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.600 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.767 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.933 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.100 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.267 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 22.433 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.600 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.767 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.933 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.100 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.267 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.433 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.600 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.767 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.933 | 0.09 | 0.09 | 0.09 | 0.09 | 0.08 |
| 24.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.433 | 0.08 | 0.08 | 0.07 | 0.07 | 0.06 |
| 24.600 | 0.06 | 0.05 | 0.05 | 0.04 | 0.04 |
| 24.767 | 0.04 | 0.03 | 0.03 | 0.03 | 0.02 |
| 24.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 25.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.433 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| 25.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.933 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 50 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

| | |
|---|---|
| Peak Discharge | 6.44 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.680 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.433 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.767 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.600 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.933 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.100 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 8.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.433 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.600 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.767 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.933 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.09 |
| 9.433 | 0.09 | 0.10 | 0.11 | 0.12 | 0.12 |
| 9.600 | 0.13 | 0.14 | 0.14 | 0.15 | 0.15 |
| 9.767 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 |
| 9.933 | 0.18 | 0.19 | 0.20 | 0.21 | 0.21 |
| 10.100 | 0.22 | 0.22 | 0.23 | 0.24 | 0.24 |
| 10.267 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 |
| 10.433 | 0.28 | 0.29 | 0.30 | 0.31 | 0.31 |
| 10.600 | 0.32 | 0.33 | 0.33 | 0.34 | 0.35 |
| 10.767 | 0.36 | 0.37 | 0.37 | 0.38 | 0.39 |
| 10.933 | 0.40 | 0.41 | 0.42 | 0.42 | 0.43 |
| 11.100 | 0.45 | 0.46 | 0.47 | 0.49 | 0.51 |
| 11.267 | 0.52 | 0.54 | 0.57 | 0.60 | 0.63 |
| 11.433 | 0.66 | 0.69 | 0.72 | 0.75 | 0.80 |
| 11.600 | 0.87 | 0.91 | 0.97 | 1.04 | 1.13 |
| 11.767 | 1.27 | 1.43 | 1.54 | 1.56 | 1.68 |
| 11.933 | 1.85 | 1.96 | 2.13 | 2.96 | 5.84 |
| 12.100 | 6.06 | 6.11 | 6.44 | 6.37 | 5.95 |
| 12.267 | 5.97 | 6.11 | 4.62 | 3.88 | 3.41 |
| 12.433 | 3.09 | 2.78 | 2.45 | 2.28 | 2.24 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 50 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.600 | 2.18 | 2.17 | 2.17 | 2.08 | 2.03 |
| 12.767 | 2.03 | 2.00 | 1.96 | 1.89 | 1.85 |
| 12.933 | 1.85 | 1.78 | 1.71 | 1.67 | 1.61 |
| 13.100 | 1.55 | 1.55 | 1.53 | 1.47 | 1.39 |
| 13.267 | 1.30 | 1.22 | 1.16 | 1.11 | 1.07 |
| 13.433 | 1.03 | 1.00 | 0.97 | 0.94 | 0.91 |
| 13.600 | 0.89 | 0.84 | 0.79 | 0.75 | 0.73 |
| 13.767 | 0.70 | 0.68 | 0.66 | 0.65 | 0.64 |
| 13.933 | 0.62 | 0.61 | 0.60 | 0.59 | 0.58 |
| 14.100 | 0.57 | 0.57 | 0.56 | 0.56 | 0.55 |
| 14.267 | 0.55 | 0.54 | 0.54 | 0.53 | 0.53 |
| 14.433 | 0.53 | 0.52 | 0.52 | 0.51 | 0.51 |
| 14.600 | 0.50 | 0.50 | 0.50 | 0.49 | 0.49 |
| 14.767 | 0.48 | 0.48 | 0.47 | 0.47 | 0.47 |
| 14.933 | 0.46 | 0.46 | 0.45 | 0.45 | 0.45 |
| 15.100 | 0.44 | 0.44 | 0.43 | 0.43 | 0.42 |
| 15.267 | 0.42 | 0.42 | 0.41 | 0.41 | 0.40 |
| 15.433 | 0.40 | 0.39 | 0.39 | 0.39 | 0.38 |
| 15.600 | 0.38 | 0.37 | 0.37 | 0.37 | 0.36 |
| 15.767 | 0.36 | 0.35 | 0.35 | 0.34 | 0.34 |
| 15.933 | 0.34 | 0.33 | 0.33 | 0.32 | 0.32 |
| 16.100 | 0.31 | 0.31 | 0.31 | 0.30 | 0.30 |
| 16.267 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 16.433 | 0.29 | 0.28 | 0.28 | 0.28 | 0.28 |
| 16.600 | 0.28 | 0.27 | 0.27 | 0.27 | 0.27 |
| 16.767 | 0.27 | 0.26 | 0.26 | 0.26 | 0.26 |
| 16.933 | 0.26 | 0.26 | 0.25 | 0.25 | 0.25 |
| 17.100 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 17.267 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 17.433 | 0.23 | 0.23 | 0.23 | 0.22 | 0.22 |
| 17.600 | 0.22 | 0.22 | 0.22 | 0.21 | 0.21 |
| 17.767 | 0.21 | 0.21 | 0.21 | 0.20 | 0.20 |
| 17.933 | 0.20 | 0.20 | 0.20 | 0.20 | 0.19 |
| 18.100 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.267 | 0.19 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.433 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.600 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.767 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 18.933 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.100 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.267 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.433 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 50 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.600 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.767 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.933 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 20.100 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.267 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.433 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.600 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.767 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.933 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.100 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.433 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 21.600 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.933 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.100 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.267 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 22.433 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.767 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.933 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.100 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.267 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.600 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.767 | 0.11 | 0.11 | 0.11 | 0.11 | 0.10 |
| 23.933 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 24.100 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 24.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 24.600 | 0.07 | 0.06 | 0.05 | 0.05 | 0.05 |
| 24.767 | 0.04 | 0.04 | 0.03 | 0.03 | 0.03 |
| 24.933 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 25.100 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.433 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 |
| 25.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.933 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 26.100 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 100 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

| | |
|---|---|
| Peak Discharge | 6.92 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.728 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.567 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.733 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 7.900 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 8.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.400 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.233 | 0.09 | 0.10 | 0.10 | 0.11 | 0.12 |
| 9.400 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 |
| 9.567 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 |
| 9.733 | 0.18 | 0.19 | 0.20 | 0.20 | 0.21 |
| 9.900 | 0.22 | 0.22 | 0.23 | 0.23 | 0.24 |
| 10.067 | 0.24 | 0.25 | 0.25 | 0.26 | 0.27 |
| 10.233 | 0.27 | 0.28 | 0.29 | 0.29 | 0.30 |
| 10.400 | 0.31 | 0.31 | 0.32 | 0.33 | 0.34 |
| 10.567 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 |
| 10.733 | 0.39 | 0.39 | 0.40 | 0.41 | 0.42 |
| 10.900 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 |
| 11.067 | 0.48 | 0.49 | 0.50 | 0.52 | 0.53 |
| 11.233 | 0.55 | 0.57 | 0.60 | 0.63 | 0.66 |
| 11.400 | 0.69 | 0.72 | 0.75 | 0.79 | 0.82 |
| 11.567 | 0.88 | 0.91 | 0.95 | 1.02 | 1.09 |
| 11.733 | 1.21 | 1.37 | 1.51 | 1.55 | 1.65 |
| 11.900 | 1.78 | 1.86 | 2.03 | 2.19 | 4.56 |
| 12.067 | 6.57 | 5.94 | 6.63 | 6.92 | 6.75 |
| 12.233 | 6.51 | 6.06 | 5.97 | 6.07 | 4.54 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 100 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.400 | 3.76 | 3.32 | 2.97 | 2.61 | 2.30 |
| 12.567 | 2.26 | 2.21 | 2.17 | 2.17 | 2.14 |
| 12.733 | 2.06 | 2.03 | 2.03 | 2.00 | 1.95 |
| 12.900 | 1.89 | 1.85 | 1.85 | 1.78 | 1.72 |
| 13.067 | 1.67 | 1.62 | 1.56 | 1.55 | 1.54 |
| 13.233 | 1.48 | 1.41 | 1.33 | 1.25 | 1.19 |
| 13.400 | 1.13 | 1.09 | 1.06 | 1.03 | 1.00 |
| 13.567 | 0.97 | 0.94 | 0.92 | 0.89 | 0.86 |
| 13.733 | 0.81 | 0.78 | 0.75 | 0.72 | 0.70 |
| 13.900 | 0.68 | 0.67 | 0.65 | 0.64 | 0.63 |
| 14.067 | 0.62 | 0.61 | 0.60 | 0.59 | 0.59 |
| 14.233 | 0.58 | 0.57 | 0.57 | 0.57 | 0.56 |
| 14.400 | 0.56 | 0.55 | 0.55 | 0.55 | 0.54 |
| 14.567 | 0.54 | 0.53 | 0.53 | 0.52 | 0.52 |
| 14.733 | 0.52 | 0.51 | 0.51 | 0.50 | 0.50 |
| 14.900 | 0.49 | 0.49 | 0.49 | 0.48 | 0.48 |
| 15.067 | 0.47 | 0.47 | 0.46 | 0.46 | 0.45 |
| 15.233 | 0.45 | 0.45 | 0.44 | 0.44 | 0.43 |
| 15.400 | 0.43 | 0.42 | 0.42 | 0.41 | 0.41 |
| 15.567 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 |
| 15.733 | 0.38 | 0.38 | 0.37 | 0.37 | 0.36 |
| 15.900 | 0.36 | 0.36 | 0.35 | 0.35 | 0.34 |
| 16.067 | 0.34 | 0.33 | 0.33 | 0.33 | 0.32 |
| 16.233 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 16.400 | 0.31 | 0.30 | 0.30 | 0.30 | 0.30 |
| 16.567 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 |
| 16.733 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 |
| 16.900 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |
| 17.067 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 |
| 17.233 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| 17.400 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 |
| 17.567 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| 17.733 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 17.900 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 18.067 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 18.233 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 18.400 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.567 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.733 | 0.19 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.900 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 19.067 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 19.233 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |

# Post-Development Conditions

Subsection: Pond Routed Hydrograph (total out) Return Event: 100 years
Label: Detention Pond (OUT) Storm Event: TypeIII 24hr (8.4 in)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.400 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.567 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.733 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.900 | 0.17 | 0.17 | 0.17 | 0.17 | 0.16 |
| 20.067 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.233 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.400 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.567 | 0.16 | 0.16 | 0.16 | 0.15 | 0.15 |
| 20.733 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.900 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.067 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.233 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.400 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.567 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.733 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.900 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 22.067 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 22.233 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.400 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.567 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.733 | 0.13 | 0.13 | 0.13 | 0.13 | 0.12 |
| 22.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.067 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.233 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.400 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.567 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.900 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 24.067 | 0.10 | 0.10 | 0.09 | 0.08 | 0.08 |
| 24.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.567 | 0.08 | 0.07 | 0.06 | 0.06 | 0.05 |
| 24.733 | 0.05 | 0.04 | 0.04 | 0.04 | 0.03 |
| 24.900 | 0.03 | 0.03 | 0.02 | 0.02 | 0.02 |
| 25.067 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 |
| 25.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.567 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.733 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 26.067 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Pond Inflow Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

## Summary for Hydrograph Addition at 'Detention Pond'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Site |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.020 | 12.133 | 0.24 |
| Flow (From) | Site | 0.241 | 12.100 | 2.95 |
| Flow (In) | Detention Pond | 0.261 | 12.100 | 3.18 |

# Post-Development Conditions

Subsection: Pond Inflow Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

## Summary for Hydrograph Addition at 'Detention Pond'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Site |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) (ft³/s) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.037 | 12.100 | 0.45 |
| Flow (From) | Site | 0.409 | 12.100 | 4.98 |
| Flow (In) | Detention Pond | 0.446 | 12.100 | 5.43 |

## Summary for Hydrograph Addition at 'Detention Pond'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Site |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.047 | 12.100 | 0.58 |
| Flow (From) | Site | 0.502 | 12.100 | 6.09 |
| Flow (In) | Detention Pond | 0.550 | 12.100 | 6.67 |

# Post-Development Conditions

Subsection: Pond Inflow Summary
Return Event: 50 years
Label: Detention Pond (IN)
Storm Event: TypeIII 24hr (8.0 in)
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

## Summary for Hydrograph Addition at 'Detention Pond'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Site |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.060 | 12.100 | 0.73 |
| Flow (From) | Site | 0.620 | 12.100 | 7.46 |
| Flow (In) | Detention Pond | 0.680 | 12.100 | 8.19 |

# Post-Development Conditions

Subsection: Pond Inflow Summary
Label: Detention Pond (IN)
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

## Summary for Hydrograph Addition at 'Detention Pond'

| Upstream Link | Upstream Node |
|---|---|
| <Catchment to Outflow Node> | Offsite |
| <Catchment to Outflow Node> | Site |

## Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (hours) | Flow (Peak) ($ft^3/s$) |
|---|---|---|---|---|
| Flow (From) | Offsite | 0.065 | 12.100 | 0.79 |
| Flow (From) | Site | 0.663 | 12.100 | 7.96 |
| Flow (In) | Detention Pond | 0.728 | 12.100 | 8.75 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

| | |
|---|---|
| Peak Discharge | 1.81 ft³/s |
| Time to Peak | 12.267 hours |
| Hydrograph Volume | 0.261 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 9.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 |
| 9.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 9.733 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 |
| 9.900 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 10.067 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 10.233 | 0.03 | 0.03 | 0.04 | 0.04 | 0.04 |
| 10.400 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 10.567 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 10.733 | 0.06 | 0.06 | 0.06 | 0.07 | 0.07 |
| 10.900 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 |
| 11.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 11.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 11.400 | 0.08 | 0.09 | 0.10 | 0.11 | 0.13 |
| 11.567 | 0.14 | 0.16 | 0.18 | 0.22 | 0.28 |
| 11.733 | 0.33 | 0.40 | 0.47 | 0.54 | 0.65 |
| 11.900 | 0.78 | 0.89 | 0.98 | 1.10 | 1.31 |
| 12.067 | 1.50 | 1.55 | 1.65 | 1.72 | 1.77 |
| 12.233 | 1.80 | 1.81 | 1.79 | 1.77 | 1.74 |
| 12.400 | 1.71 | 1.68 | 1.65 | 1.59 | 1.55 |
| 12.567 | 1.55 | 1.49 | 1.40 | 1.28 | 1.18 |
| 12.733 | 1.09 | 1.03 | 0.98 | 0.92 | 0.85 |
| 12.900 | 0.74 | 0.66 | 0.59 | 0.55 | 0.52 |
| 13.067 | 0.49 | 0.46 | 0.44 | 0.43 | 0.41 |
| 13.233 | 0.40 | 0.38 | 0.37 | 0.37 | 0.36 |
| 13.400 | 0.35 | 0.34 | 0.34 | 0.33 | 0.33 |
| 13.567 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 13.733 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 13.900 | 0.28 | 0.28 | 0.27 | 0.27 | 0.27 |
| 14.067 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 14.233 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 14.400 | 0.24 | 0.23 | 0.23 | 0.23 | 0.23 |
| 14.567 | 0.23 | 0.23 | 0.22 | 0.22 | 0.22 |
| 14.733 | 0.22 | 0.22 | 0.21 | 0.21 | 0.21 |
| 14.900 | 0.21 | 0.21 | 0.21 | 0.20 | 0.20 |
| 15.067 | 0.20 | 0.20 | 0.20 | 0.19 | 0.19 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 15.233 | 0.19 | 0.19 | 0.19 | 0.19 | 0.18 |
| 15.400 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 15.567 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 15.733 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |
| 15.900 | 0.16 | 0.16 | 0.16 | 0.15 | 0.15 |
| 16.067 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 16.233 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 16.400 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 16.567 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 16.733 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 16.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 17.067 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 17.233 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 17.400 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 17.567 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.733 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 17.900 | 0.10 | 0.10 | 0.09 | 0.09 | 0.09 |
| 18.067 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 18.233 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 18.400 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 18.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 18.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 19.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 20.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 21.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 21.733 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 21.900 | 0.07 | 0.07 | 0.07 | 0.07 | 0.06 |
| 22.067 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 2 yrs

Return Event: 2 years
Storm Event: TypeIII 24hr (4.3 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 22.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.400 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.567 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.733 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 22.900 | 0.06 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.233 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.400 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.567 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.733 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 23.900 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 24.067 | 0.05 | 0.04 | 0.04 | 0.04 | 0.03 |
| 24.233 | 0.03 | 0.03 | 0.03 | 0.02 | 0.02 |
| 24.400 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 |
| 24.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 24.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.067 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.400 | 0.00 | 0.00 | 0.00 | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

| | |
|---|---|
| Peak Discharge | 3.73 ft³/s |
| Time to Peak | 12.200 hours |
| Hydrograph Volume | 0.446 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.867 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 8.367 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 8.533 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.700 | 0.02 | 0.02 | 0.02 | 0.03 | 0.03 |
| 8.867 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 9.033 | 0.03 | 0.04 | 0.04 | 0.04 | 0.04 |
| 9.200 | 0.04 | 0.04 | 0.05 | 0.05 | 0.05 |
| 9.367 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 |
| 9.533 | 0.06 | 0.06 | 0.06 | 0.06 | 0.07 |
| 9.700 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 |
| 9.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 10.367 | 0.08 | 0.08 | 0.08 | 0.09 | 0.10 |
| 10.533 | 0.11 | 0.11 | 0.12 | 0.13 | 0.14 |
| 10.700 | 0.14 | 0.15 | 0.16 | 0.16 | 0.17 |
| 10.867 | 0.18 | 0.18 | 0.19 | 0.20 | 0.21 |
| 11.033 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 |
| 11.200 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 |
| 11.367 | 0.34 | 0.35 | 0.37 | 0.38 | 0.40 |
| 11.533 | 0.42 | 0.45 | 0.48 | 0.53 | 0.59 |
| 11.700 | 0.70 | 0.82 | 0.91 | 0.98 | 1.05 |
| 11.867 | 1.14 | 1.27 | 1.43 | 1.55 | 1.66 |
| 12.033 | 1.85 | 1.99 | 2.11 | 2.24 | 3.29 |
| 12.200 | 3.73 | 3.56 | 3.29 | 3.01 | 2.77 |
| 12.367 | 2.54 | 2.31 | 2.27 | 2.23 | 2.18 |
| 12.533 | 2.17 | 2.15 | 2.05 | 2.03 | 2.01 |
| 12.700 | 1.96 | 1.87 | 1.85 | 1.80 | 1.72 |
| 12.867 | 1.66 | 1.59 | 1.55 | 1.55 | 1.47 |
| 13.033 | 1.37 | 1.26 | 1.16 | 1.09 | 1.04 |
| 13.200 | 0.99 | 0.94 | 0.89 | 0.82 | 0.74 |
| 13.367 | 0.68 | 0.63 | 0.60 | 0.57 | 0.56 |
| 13.533 | 0.54 | 0.53 | 0.52 | 0.51 | 0.50 |
| 13.700 | 0.49 | 0.48 | 0.48 | 0.47 | 0.46 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.867 | 0.45 | 0.45 | 0.44 | 0.43 | 0.43 |
| 14.033 | 0.42 | 0.42 | 0.41 | 0.40 | 0.40 |
| 14.200 | 0.39 | 0.39 | 0.39 | 0.38 | 0.38 |
| 14.367 | 0.38 | 0.37 | 0.37 | 0.37 | 0.36 |
| 14.533 | 0.36 | 0.36 | 0.35 | 0.35 | 0.35 |
| 14.700 | 0.34 | 0.34 | 0.34 | 0.34 | 0.33 |
| 14.867 | 0.33 | 0.33 | 0.32 | 0.32 | 0.32 |
| 15.033 | 0.32 | 0.31 | 0.31 | 0.31 | 0.30 |
| 15.200 | 0.30 | 0.30 | 0.30 | 0.29 | 0.29 |
| 15.367 | 0.29 | 0.28 | 0.28 | 0.28 | 0.27 |
| 15.533 | 0.27 | 0.27 | 0.27 | 0.26 | 0.26 |
| 15.700 | 0.26 | 0.25 | 0.25 | 0.25 | 0.25 |
| 15.867 | 0.24 | 0.24 | 0.24 | 0.23 | 0.23 |
| 16.033 | 0.23 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.200 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 16.367 | 0.21 | 0.20 | 0.20 | 0.20 | 0.20 |
| 16.533 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 16.700 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 16.867 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 17.033 | 0.18 | 0.18 | 0.18 | 0.18 | 0.17 |
| 17.200 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 17.367 | 0.17 | 0.17 | 0.17 | 0.16 | 0.16 |
| 17.533 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 17.700 | 0.16 | 0.15 | 0.15 | 0.15 | 0.15 |
| 17.867 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 18.033 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 18.200 | 0.14 | 0.14 | 0.14 | 0.13 | 0.13 |
| 18.367 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.533 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.700 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 18.867 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.033 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.200 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.367 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 19.533 | 0.12 | 0.12 | 0.12 | 0.11 | 0.11 |
| 19.700 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 19.867 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.033 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.200 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.367 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 20.533 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 20.700 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 10 yrs

Return Event: 10 years
Storm Event: TypeIII 24hr (6.0 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.867 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.033 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.200 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.367 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 21.533 | 0.10 | 0.10 | 0.10 | 0.09 | 0.09 |
| 21.700 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 21.867 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.033 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.200 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.367 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.533 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 22.700 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 22.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.367 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.533 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.700 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 23.867 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.033 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.200 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.367 | 0.08 | 0.08 | 0.07 | 0.06 | 0.06 |
| 24.533 | 0.05 | 0.05 | 0.04 | 0.04 | 0.04 |
| 24.700 | 0.03 | 0.03 | 0.03 | 0.03 | 0.02 |
| 24.867 | 0.02 | 0.02 | 0.02 | 0.02 | 0.01 |
| 25.033 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.200 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.367 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.533 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.867 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

| | |
|---|---|
| Peak Discharge | 5.83 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.550 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 7.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.267 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7.433 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.600 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.767 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 |
| 7.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.100 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 8.267 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 8.433 | 0.03 | 0.03 | 0.03 | 0.04 | 0.04 |
| 8.600 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.767 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.933 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 |
| 9.100 | 0.06 | 0.07 | 0.07 | 0.07 | 0.07 |
| 9.267 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.600 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.767 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.933 | 0.08 | 0.09 | 0.10 | 0.11 | 0.11 |
| 10.100 | 0.12 | 0.13 | 0.13 | 0.14 | 0.14 |
| 10.267 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 |
| 10.433 | 0.18 | 0.19 | 0.20 | 0.21 | 0.22 |
| 10.600 | 0.22 | 0.23 | 0.24 | 0.25 | 0.25 |
| 10.767 | 0.26 | 0.27 | 0.27 | 0.28 | 0.29 |
| 10.933 | 0.30 | 0.30 | 0.31 | 0.32 | 0.32 |
| 11.100 | 0.33 | 0.34 | 0.35 | 0.37 | 0.38 |
| 11.267 | 0.40 | 0.41 | 0.43 | 0.45 | 0.47 |
| 11.433 | 0.49 | 0.51 | 0.53 | 0.55 | 0.59 |
| 11.600 | 0.65 | 0.73 | 0.82 | 0.91 | 0.97 |
| 11.767 | 1.05 | 1.14 | 1.27 | 1.43 | 1.54 |
| 11.933 | 1.56 | 1.71 | 1.86 | 2.03 | 2.21 |
| 12.100 | 4.02 | 5.61 | 5.83 | 5.27 | 4.61 |
| 12.267 | 4.06 | 3.62 | 3.33 | 3.06 | 2.79 |
| 12.433 | 2.54 | 2.30 | 2.26 | 2.21 | 2.17 |
| 12.600 | 2.17 | 2.11 | 2.03 | 2.03 | 2.00 |
| 12.767 | 1.95 | 1.87 | 1.85 | 1.82 | 1.73 |
| 12.933 | 1.68 | 1.62 | 1.56 | 1.55 | 1.52 |
| 13.100 | 1.45 | 1.34 | 1.25 | 1.17 | 1.10 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 13.267 | 1.06 | 1.01 | 0.97 | 0.93 | 0.90 |
| 13.433 | 0.85 | 0.78 | 0.73 | 0.69 | 0.66 |
| 13.600 | 0.63 | 0.61 | 0.60 | 0.58 | 0.57 |
| 13.767 | 0.56 | 0.55 | 0.55 | 0.54 | 0.53 |
| 13.933 | 0.52 | 0.52 | 0.51 | 0.50 | 0.50 |
| 14.100 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 |
| 14.267 | 0.46 | 0.46 | 0.45 | 0.45 | 0.44 |
| 14.433 | 0.44 | 0.44 | 0.43 | 0.43 | 0.42 |
| 14.600 | 0.42 | 0.42 | 0.41 | 0.41 | 0.41 |
| 14.767 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 |
| 14.933 | 0.39 | 0.38 | 0.38 | 0.38 | 0.37 |
| 15.100 | 0.37 | 0.37 | 0.36 | 0.36 | 0.36 |
| 15.267 | 0.35 | 0.35 | 0.34 | 0.34 | 0.34 |
| 15.433 | 0.33 | 0.33 | 0.33 | 0.32 | 0.32 |
| 15.600 | 0.32 | 0.31 | 0.31 | 0.31 | 0.30 |
| 15.767 | 0.30 | 0.30 | 0.29 | 0.29 | 0.28 |
| 15.933 | 0.28 | 0.28 | 0.27 | 0.27 | 0.27 |
| 16.100 | 0.26 | 0.26 | 0.26 | 0.25 | 0.25 |
| 16.267 | 0.25 | 0.25 | 0.25 | 0.24 | 0.24 |
| 16.433 | 0.24 | 0.24 | 0.24 | 0.23 | 0.23 |
| 16.600 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| 16.767 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 16.933 | 0.22 | 0.21 | 0.21 | 0.21 | 0.21 |
| 17.100 | 0.21 | 0.21 | 0.20 | 0.20 | 0.20 |
| 17.267 | 0.20 | 0.20 | 0.20 | 0.20 | 0.19 |
| 17.433 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 17.600 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 17.767 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 17.933 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 18.100 | 0.17 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.267 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 18.433 | 0.16 | 0.16 | 0.15 | 0.15 | 0.15 |
| 18.600 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.767 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 18.933 | 0.15 | 0.15 | 0.15 | 0.15 | 0.14 |
| 19.100 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.433 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 19.600 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 19.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 19.933 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.100 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 25 yrs

Return Event: 25 years
Storm Event: TypeIII 24hr (6.9 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 20.267 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 20.433 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 20.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.767 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 20.933 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.100 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 21.267 | 0.12 | 0.12 | 0.12 | 0.12 | 0.11 |
| 21.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.600 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.767 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 21.933 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.100 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 22.267 | 0.11 | 0.11 | 0.10 | 0.10 | 0.10 |
| 22.433 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.600 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.767 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 22.933 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.100 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 23.267 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.433 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.600 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.767 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 |
| 23.933 | 0.09 | 0.09 | 0.09 | 0.09 | 0.08 |
| 24.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.433 | 0.08 | 0.08 | 0.07 | 0.07 | 0.06 |
| 24.600 | 0.06 | 0.05 | 0.05 | 0.04 | 0.04 |
| 24.767 | 0.04 | 0.03 | 0.03 | 0.03 | 0.02 |
| 24.933 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 25.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.433 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| 25.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.933 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

| | |
|---|---|
| Peak Discharge | 6.44 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.680 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.433 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.767 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.933 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.100 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.267 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.433 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.600 | 0.02 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.767 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.933 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 8.100 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 8.267 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.433 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.600 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.767 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.933 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.100 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.09 |
| 9.433 | 0.09 | 0.10 | 0.11 | 0.12 | 0.12 |
| 9.600 | 0.13 | 0.14 | 0.14 | 0.15 | 0.15 |
| 9.767 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 |
| 9.933 | 0.18 | 0.19 | 0.20 | 0.21 | 0.21 |
| 10.100 | 0.22 | 0.22 | 0.23 | 0.24 | 0.24 |
| 10.267 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 |
| 10.433 | 0.28 | 0.29 | 0.30 | 0.31 | 0.31 |
| 10.600 | 0.32 | 0.33 | 0.33 | 0.34 | 0.35 |
| 10.767 | 0.36 | 0.37 | 0.37 | 0.38 | 0.39 |
| 10.933 | 0.40 | 0.41 | 0.42 | 0.42 | 0.43 |
| 11.100 | 0.45 | 0.46 | 0.47 | 0.49 | 0.51 |
| 11.267 | 0.52 | 0.54 | 0.57 | 0.60 | 0.63 |
| 11.433 | 0.66 | 0.69 | 0.72 | 0.75 | 0.80 |
| 11.600 | 0.87 | 0.91 | 0.97 | 1.04 | 1.13 |
| 11.767 | 1.27 | 1.43 | 1.54 | 1.56 | 1.68 |
| 11.933 | 1.85 | 1.96 | 2.13 | 2.96 | 5.84 |
| 12.100 | 6.06 | 6.11 | 6.44 | 6.37 | 5.95 |
| 12.267 | 5.97 | 6.11 | 4.62 | 3.88 | 3.41 |
| 12.433 | 3.09 | 2.78 | 2.45 | 2.28 | 2.24 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.600 | 2.18 | 2.17 | 2.17 | 2.08 | 2.03 |
| 12.767 | 2.03 | 2.00 | 1.96 | 1.89 | 1.85 |
| 12.933 | 1.85 | 1.78 | 1.71 | 1.67 | 1.61 |
| 13.100 | 1.55 | 1.55 | 1.53 | 1.47 | 1.39 |
| 13.267 | 1.30 | 1.22 | 1.16 | 1.11 | 1.07 |
| 13.433 | 1.03 | 1.00 | 0.97 | 0.94 | 0.91 |
| 13.600 | 0.89 | 0.84 | 0.79 | 0.75 | 0.73 |
| 13.767 | 0.70 | 0.68 | 0.66 | 0.65 | 0.64 |
| 13.933 | 0.62 | 0.61 | 0.60 | 0.59 | 0.58 |
| 14.100 | 0.57 | 0.57 | 0.56 | 0.56 | 0.55 |
| 14.267 | 0.55 | 0.54 | 0.54 | 0.53 | 0.53 |
| 14.433 | 0.53 | 0.52 | 0.52 | 0.51 | 0.51 |
| 14.600 | 0.50 | 0.50 | 0.50 | 0.49 | 0.49 |
| 14.767 | 0.48 | 0.48 | 0.47 | 0.47 | 0.47 |
| 14.933 | 0.46 | 0.46 | 0.45 | 0.45 | 0.45 |
| 15.100 | 0.44 | 0.44 | 0.43 | 0.43 | 0.42 |
| 15.267 | 0.42 | 0.42 | 0.41 | 0.41 | 0.40 |
| 15.433 | 0.40 | 0.39 | 0.39 | 0.39 | 0.38 |
| 15.600 | 0.38 | 0.37 | 0.37 | 0.37 | 0.36 |
| 15.767 | 0.36 | 0.35 | 0.35 | 0.34 | 0.34 |
| 15.933 | 0.34 | 0.33 | 0.33 | 0.32 | 0.32 |
| 16.100 | 0.31 | 0.31 | 0.31 | 0.30 | 0.30 |
| 16.267 | 0.30 | 0.30 | 0.29 | 0.29 | 0.29 |
| 16.433 | 0.29 | 0.28 | 0.28 | 0.28 | 0.28 |
| 16.600 | 0.28 | 0.27 | 0.27 | 0.27 | 0.27 |
| 16.767 | 0.27 | 0.26 | 0.26 | 0.26 | 0.26 |
| 16.933 | 0.26 | 0.26 | 0.25 | 0.25 | 0.25 |
| 17.100 | 0.25 | 0.25 | 0.24 | 0.24 | 0.24 |
| 17.267 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |
| 17.433 | 0.23 | 0.23 | 0.23 | 0.22 | 0.22 |
| 17.600 | 0.22 | 0.22 | 0.22 | 0.21 | 0.21 |
| 17.767 | 0.21 | 0.21 | 0.21 | 0.20 | 0.20 |
| 17.933 | 0.20 | 0.20 | 0.20 | 0.20 | 0.19 |
| 18.100 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.267 | 0.19 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.433 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.600 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.767 | 0.18 | 0.18 | 0.18 | 0.17 | 0.17 |
| 18.933 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.100 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.267 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.433 | 0.17 | 0.17 | 0.16 | 0.16 | 0.16 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 50 yrs

Return Event: 50 years
Storm Event: TypeIII 24hr (8.0 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.600 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.767 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 19.933 | 0.16 | 0.16 | 0.16 | 0.16 | 0.15 |
| 20.100 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.267 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.433 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.600 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.767 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 20.933 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.100 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.267 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.433 | 0.14 | 0.14 | 0.14 | 0.14 | 0.13 |
| 21.600 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.767 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 21.933 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.100 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.267 | 0.13 | 0.13 | 0.12 | 0.12 | 0.12 |
| 22.433 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.600 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.767 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 22.933 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.100 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.267 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.433 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.600 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.767 | 0.11 | 0.11 | 0.11 | 0.11 | 0.10 |
| 23.933 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| 24.100 | 0.09 | 0.09 | 0.08 | 0.08 | 0.08 |
| 24.267 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.433 | 0.08 | 0.08 | 0.08 | 0.08 | 0.07 |
| 24.600 | 0.07 | 0.06 | 0.05 | 0.05 | 0.05 |
| 24.767 | 0.04 | 0.04 | 0.03 | 0.03 | 0.03 |
| 24.933 | 0.03 | 0.02 | 0.02 | 0.02 | 0.02 |
| 25.100 | 0.02 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.267 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.433 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 |
| 25.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.767 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.933 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 26.100 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

| | |
|---|---|
| Peak Discharge | 6.92 ft³/s |
| Time to Peak | 12.167 hours |
| Hydrograph Volume | 0.728 ac-ft |

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 6.233 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6.567 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.733 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 6.900 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 7.067 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.233 | 0.02 | 0.02 | 0.02 | 0.02 | 0.02 |
| 7.400 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.567 | 0.03 | 0.03 | 0.03 | 0.03 | 0.03 |
| 7.733 | 0.04 | 0.04 | 0.04 | 0.04 | 0.04 |
| 7.900 | 0.04 | 0.04 | 0.04 | 0.05 | 0.05 |
| 8.067 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| 8.233 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 8.400 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| 8.567 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.733 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 8.900 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.067 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 9.233 | 0.09 | 0.10 | 0.10 | 0.11 | 0.12 |
| 9.400 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 |
| 9.567 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 |
| 9.733 | 0.18 | 0.19 | 0.20 | 0.20 | 0.21 |
| 9.900 | 0.22 | 0.22 | 0.23 | 0.23 | 0.24 |
| 10.067 | 0.24 | 0.25 | 0.25 | 0.26 | 0.27 |
| 10.233 | 0.27 | 0.28 | 0.29 | 0.29 | 0.30 |
| 10.400 | 0.31 | 0.31 | 0.32 | 0.33 | 0.34 |
| 10.567 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 |
| 10.733 | 0.39 | 0.39 | 0.40 | 0.41 | 0.42 |
| 10.900 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 |
| 11.067 | 0.48 | 0.49 | 0.50 | 0.52 | 0.53 |
| 11.233 | 0.55 | 0.57 | 0.60 | 0.63 | 0.66 |
| 11.400 | 0.69 | 0.72 | 0.75 | 0.79 | 0.82 |
| 11.567 | 0.88 | 0.91 | 0.95 | 1.02 | 1.09 |
| 11.733 | 1.21 | 1.37 | 1.51 | 1.55 | 1.65 |
| 11.900 | 1.78 | 1.86 | 2.03 | 2.19 | 4.56 |
| 12.067 | 6.57 | 5.94 | 6.63 | 6.92 | 6.75 |
| 12.233 | 6.51 | 6.06 | 5.97 | 6.07 | 4.54 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 12.400 | 3.76 | 3.32 | 2.97 | 2.61 | 2.30 |
| 12.567 | 2.26 | 2.21 | 2.17 | 2.17 | 2.14 |
| 12.733 | 2.06 | 2.03 | 2.03 | 2.00 | 1.95 |
| 12.900 | 1.89 | 1.85 | 1.85 | 1.78 | 1.72 |
| 13.067 | 1.67 | 1.62 | 1.56 | 1.55 | 1.54 |
| 13.233 | 1.48 | 1.41 | 1.33 | 1.25 | 1.19 |
| 13.400 | 1.13 | 1.09 | 1.06 | 1.03 | 1.00 |
| 13.567 | 0.97 | 0.94 | 0.92 | 0.89 | 0.86 |
| 13.733 | 0.81 | 0.78 | 0.75 | 0.72 | 0.70 |
| 13.900 | 0.68 | 0.67 | 0.65 | 0.64 | 0.63 |
| 14.067 | 0.62 | 0.61 | 0.60 | 0.59 | 0.59 |
| 14.233 | 0.58 | 0.57 | 0.57 | 0.57 | 0.56 |
| 14.400 | 0.56 | 0.55 | 0.55 | 0.55 | 0.54 |
| 14.567 | 0.54 | 0.53 | 0.53 | 0.52 | 0.52 |
| 14.733 | 0.52 | 0.51 | 0.51 | 0.50 | 0.50 |
| 14.900 | 0.49 | 0.49 | 0.49 | 0.48 | 0.48 |
| 15.067 | 0.47 | 0.47 | 0.46 | 0.46 | 0.45 |
| 15.233 | 0.45 | 0.45 | 0.44 | 0.44 | 0.43 |
| 15.400 | 0.43 | 0.42 | 0.42 | 0.41 | 0.41 |
| 15.567 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 |
| 15.733 | 0.38 | 0.38 | 0.37 | 0.37 | 0.36 |
| 15.900 | 0.36 | 0.36 | 0.35 | 0.35 | 0.34 |
| 16.067 | 0.34 | 0.33 | 0.33 | 0.33 | 0.32 |
| 16.233 | 0.32 | 0.32 | 0.31 | 0.31 | 0.31 |
| 16.400 | 0.31 | 0.30 | 0.30 | 0.30 | 0.30 |
| 16.567 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 |
| 16.733 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 |
| 16.900 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |
| 17.067 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 |
| 17.233 | 0.25 | 0.25 | 0.25 | 0.25 | 0.25 |
| 17.400 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 |
| 17.567 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 |
| 17.733 | 0.22 | 0.22 | 0.22 | 0.22 | 0.22 |
| 17.900 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| 18.067 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| 18.233 | 0.20 | 0.20 | 0.19 | 0.19 | 0.19 |
| 18.400 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.567 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| 18.733 | 0.19 | 0.18 | 0.18 | 0.18 | 0.18 |
| 18.900 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 19.067 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| 19.233 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |

# Post-Development Conditions

Subsection: Diverted Hydrograph
Label: Outlet
Scenario: Bryant, AR - Synthetic Curve, 100 yrs

Return Event: 100 years
Storm Event: TypeIII 24hr (8.4 in)

**HYDROGRAPH ORDINATES (ft³/s)**
**Output Time Increment = 0.033 hours**
**Time on left represents time for first value in each row.**

| Time (hours) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) | Flow (ft³/s) |
|---|---|---|---|---|---|
| 19.400 | 0.18 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.567 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.733 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| 19.900 | 0.17 | 0.17 | 0.17 | 0.17 | 0.16 |
| 20.067 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.233 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.400 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| 20.567 | 0.16 | 0.16 | 0.16 | 0.15 | 0.15 |
| 20.733 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 20.900 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.067 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.233 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 21.400 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.567 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.733 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 21.900 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| 22.067 | 0.14 | 0.14 | 0.13 | 0.13 | 0.13 |
| 22.233 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.400 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.567 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 |
| 22.733 | 0.13 | 0.13 | 0.13 | 0.13 | 0.12 |
| 22.900 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.067 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.233 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.400 | 0.12 | 0.12 | 0.12 | 0.12 | 0.12 |
| 23.567 | 0.12 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.733 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 23.900 | 0.11 | 0.11 | 0.11 | 0.11 | 0.11 |
| 24.067 | 0.10 | 0.10 | 0.09 | 0.08 | 0.08 |
| 24.233 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.400 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| 24.567 | 0.08 | 0.07 | 0.06 | 0.06 | 0.05 |
| 24.733 | 0.05 | 0.04 | 0.04 | 0.04 | 0.03 |
| 24.900 | 0.03 | 0.03 | 0.02 | 0.02 | 0.02 |
| 25.067 | 0.02 | 0.02 | 0.02 | 0.01 | 0.01 |
| 25.233 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.400 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |
| 25.567 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.733 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 25.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 26.067 | 0.00 | 0.00 | (N/A) | (N/A) | (N/A) |

# Post-Development Conditions

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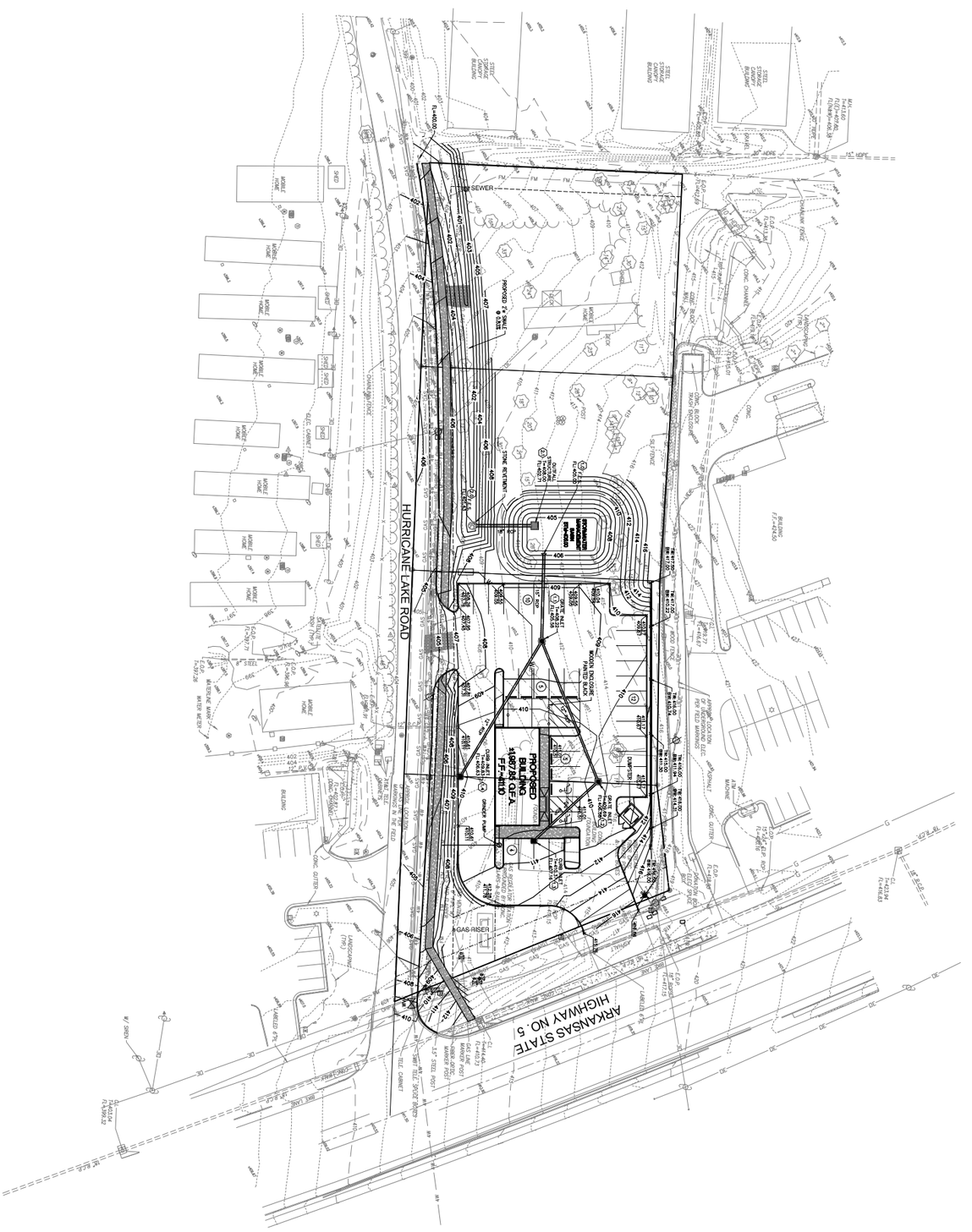
# APPENDIX G:
# SITE GRADING PLAN
# (PLAN SHEET C5.0)

DRAWING FILE: O:\DRAWITTOS\2025\7753\Drafr\elminary\7775-Base-Current_NEW.dwg LAYOUT: C5.0-Site Grading Plan PLOTTED: Jun 26, 2025 - 4:05pm PLOTTED BY: lucas.arthur




SITE GRADING PLAN

SHEET NO.
C5.0

SHEET TITLE:

WORK #

MAP BOOK #

S.U.C. MAP #

DATE OF SURVEY
DRAWN BY
C.R.M.
CHECKED BY
C.M.S.
JOB NO.
24-12-2023
SCALE
1" = 30'
PLAT BOOK #
2025-7775
PAGE NO. #

REVISIONS:

ISSUED FOR PERMIT
CITY COMMENTS
PERMIT NUMBER: 000946
5/7/25
1-2026

SITE IMPROVEMENT PLANS FOR:

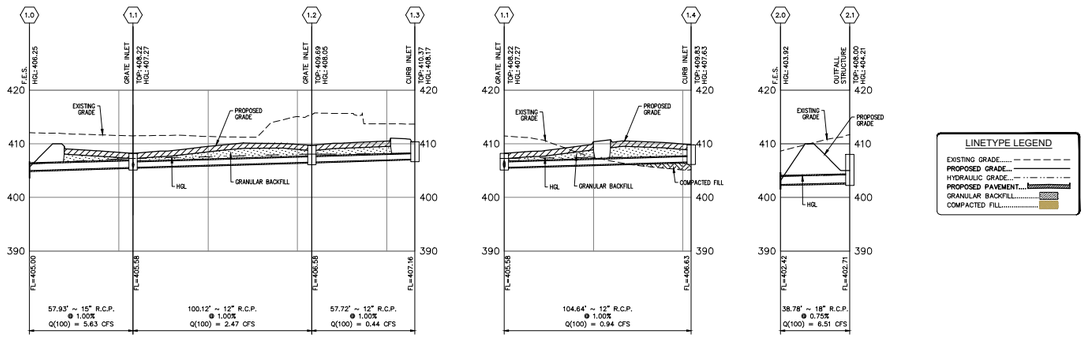
# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N,
BRYANT, ARKANSAS 72019

PREPARED BY:

STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO 63005 PH: (636) 530-9100 FAX: (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com

# APPENDIX H:
# SEWER PROFILES
# (PLAN SHEET C8.0)




## STORM SEWER PROFILES

HORIZONTAL SCALE: 1"=30'
VERTICAL SCALE: 1"=10'

LINETYPE LEGEND

EXISTING GRADE.....
PROPOSED GRADE.....
HYDRAULIC GRADE.....
PROPOSED PAVEMENT.....
GRANULAR BACKFILL.....
COMPACTED FILL.....

| Project name: | GDF - BRYANT | | | | | | | | Calculated By: | L.C.W. | | 100-year Pipe Hydraulics | | | | | | | |

# APPENDIX I:
# DRAINAGE AREA MAPS
# (PLAN SHEET C10.0 & C10.1)

## STORMWATER DIFFERENTIAL RUNOFF

| PRE-DEVELOPED | | | |
|---|---|---|---|
| | ACRES | C*I | TOTAL Q(100) |
| GRASS | 1.26 | 5.10 | 6.40 |
| PVMT/ROOF | 0.15 | 9.50 | 1.40 |
| | | TOTAL Q(100) = | 7.81 |

| POST-DEVELOPED | | | |
|---|---|---|---|
| | ACRES | C*I | TOTAL Q(100) |
| GRASS | 0.61 | 5.10 | 3.09 |
| PVMT/ROOF | 0.80 | 9.50 | 7.58 |
| | | TOTAL Q(100) = | 10.67 |
| | | | |
| | DIFFERENTIAL = POST - PRE = | + | 2.86 |

**TABLE 1**
**Allowable Peak Discharge**
**Pre-Developed Conditions**

| *Design Storm (Year)* | *Pre-Development Runoff (c.f.s.)** | *Volume (ac-ft)* |
|---|---|---|
| 2 | 2.53 | 0.210 |
| 10 | 4.61 | 0.377 |
| 25 | 5.77 | 0.472 |
| 50 | 7.22 | 0.593 |
| 100 | 7.75 | 0.637 |

* = Includes offsite drainage onto subject property





PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
Chesterfield, MO 63005-1243
530-3800 FAX (636) 530-8030
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

05/21/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY
NUMBER: 000096

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO.: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
EXISTING DRAINAGE AREA MAP

SHEET NO.:
C10.0

**GOOD DAY FARM - BRYANT** 2024-7775

**STORMWATER RUNOFF CALCULATIONS**

Q=CIA
Q=PEAK FLOW, C=RUNOFF COEFF.,
I=RAINFALL INTENSITY, A=DRAINAGE AREA

100 YEAR 5-MIN
I=10 IN/HR
C (IMPERVIOUS)=0.95*
C (PERVIOUS) = 0.51*
*=FROM TABLE 400-1

**POST-DEVELOPMENT RUNOFF**

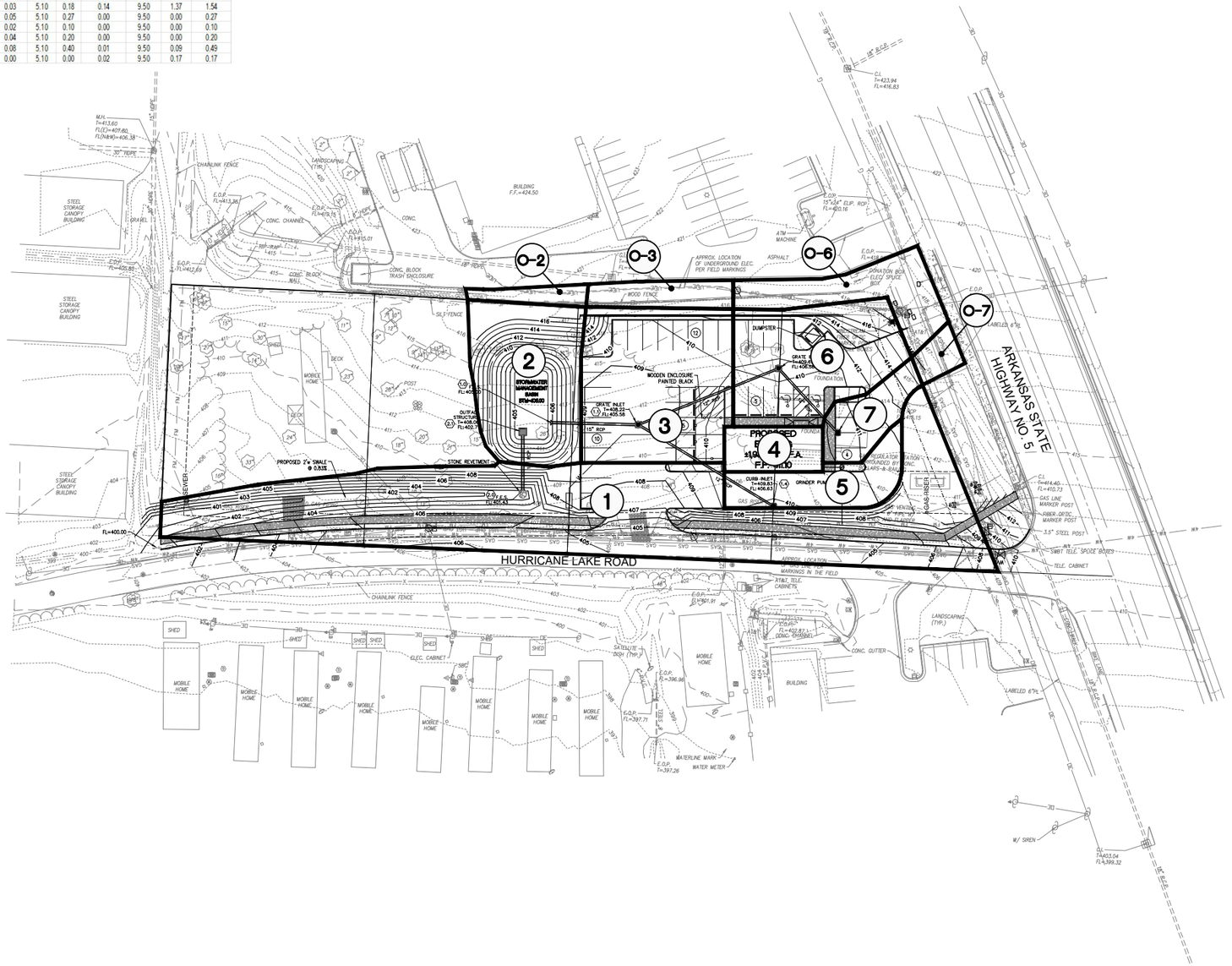
| SUBAREA | AREA ( SQ FT ) PERVIOUS | IMPERVIOUS | TOTAL AREA SQ FT | AC | PERVIOUS ACREAGE | C*I (PERV.) | Q (PERV.) | IMPERVIOUS ACREAGE | C*I (IMPRV.) | Q (IMPRV.) | Q (TOTAL) |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 15,088 | 12,945 | 28,033 | 0.64 | 0.35 | 5.10 | 1.77 | 0.30 | 9.50 | 2.82 | 4.59 |
| 2 | 7,501 | 0 | 7,501 | 0.17 | 0.17 | 5.10 | 0.88 | 0.00 | 9.50 | 0.00 | 0.88 |
| 3 | 0 | 10,160 | 10,160 | 0.23 | 0.00 | 5.10 | 0.00 | 0.23 | 9.50 | 2.22 | 2.22 |
| 4 | 0 | 1,960 | 1,960 | 0.04 | 0.00 | 5.10 | 0.00 | 0.04 | 9.50 | 0.43 | 0.43 |
| 5 | 0 | 3,415 | 3,415 | 0.08 | 0.00 | 5.10 | 0.00 | 0.08 | 9.50 | 0.74 | 0.74 |
| 6 | 1,500 | 6,268 | 7,768 | 0.18 | 0.03 | 5.10 | 0.18 | 0.14 | 9.50 | 1.37 | 1.54 |
| 7 | 2,292 | 0 | 2,292 | 0.05 | 0.05 | 5.10 | 0.27 | 0.00 | 9.50 | 0.00 | 0.27 |
| O-2 | 854 | 0 | 854 | 0.02 | 0.02 | 5.10 | 0.10 | 0.00 | 9.50 | 0.00 | 0.10 |
| O-3 | 1,689 | 0 | 1,689 | 0.04 | 0.04 | 5.10 | 0.20 | 0.00 | 9.50 | 0.00 | 0.20 |
| O-6 | 3,424 | 400 | 3,824 | 0.09 | 0.08 | 5.10 | 0.40 | 0.01 | 9.50 | 0.09 | 0.49 |
| O-7 | 0 | 779 | 779 | 0.02 | 0.00 | 5.10 | 0.00 | 0.02 | 9.50 | 0.17 | 0.17 |

**TABLE 2**
**Peak Discharge - Post-Developed Conditions**

| Design Storm (Year) | Allowable Discharge (cfs) | Post-Developed Discharge (cfs) |
|---|---|---|
| 2 | 2.53 | 1.81 |
| 10 | 4.61 | 3.73 |
| 25 | 5.77 | 5.83 |
| 50 | 7.22 | 6.44 |
| 100 | 7.75 | 6.92 |

**Stormwater Detention Summary**

| Design Storm (Year) | Basin Discharge (cfs) | Basin WSEL (feet) | Basin Freeboard (feet) |
|---|---|---|---|
| 2 | 1.81 | 406.46 | 3.54 |
| 10 | 3.73 | 407.31 | 2.69 |
| 25 | 5.83 | 407.44 | 2.56 |
| 50 | 6.44 | 407.72 | 2.28 |
| 100 | 6.92 | 407.82 | 2.18 |





PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
Chesterfield, MO 63005-1243
530-3800 FAX (636) 530-8030
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

05/21/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY
NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P. # | BASE MAP # |
| S.L.C. H&T # | H&T S.U.P. # |
| M.D.N.R. # | |

SHEET TITLE:
PROPOSED DRAINAGE AREA MAP

SHEET NO.:
C10.1

# APPENDIX J:
# OUTFALL STRUCTURE
# DETAIL

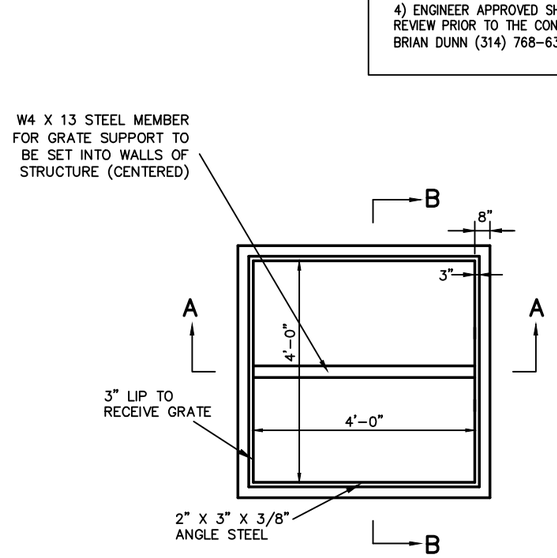
OUTFALL STRUCTURE NOTES:

1) CONTROL STRUCTURE TO BE REINFORCED CONCRETE: WALL THICKNESS IS 8" w/ TWO (2) ROWS OF #4 STEEL.

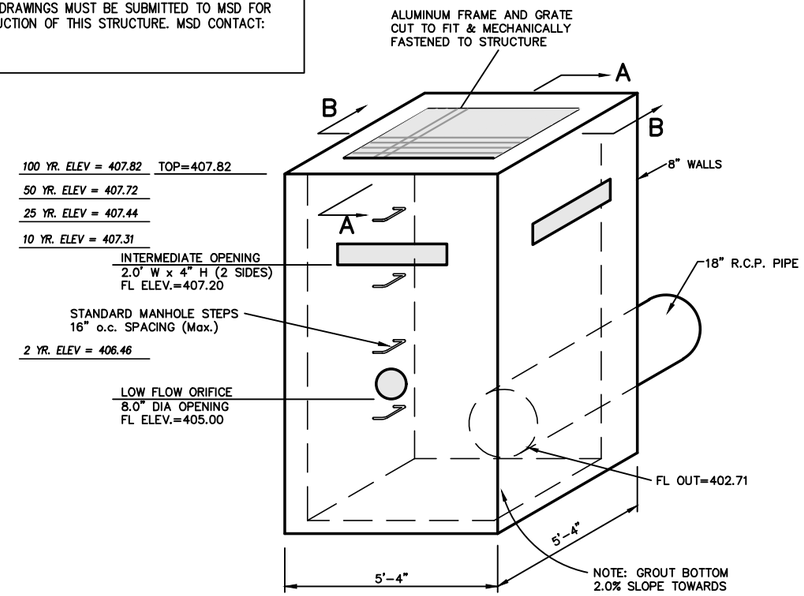
2) OUTFALL STRUCTURE SHALL BE PRE-CAST OR CAST-IN-PLACE.

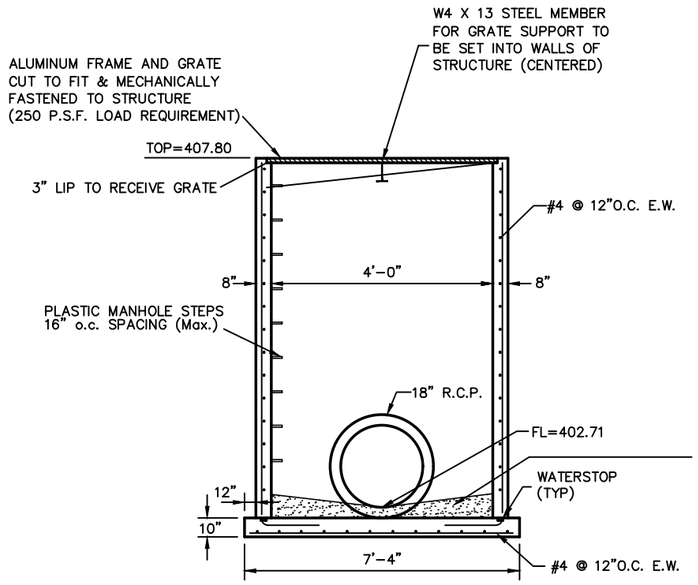
3) CONTRACTOR SHALL PROVIDE A HIGH LEVEL OF CARE WHEN PLACING & COMPACTING "CLAY" SOILS AROUND OUTFALL STRUCTURE & PIPING. THE GEOTECHNICAL ENGINEER SHALL BE PRESENT TO CONFIRM THE "LEVEL OF PLACEMENT"

4) ENGINEER APPROVED SHOP DRAWINGS MUST BE SUBMITTED TO MSD FOR REVIEW PRIOR TO THE CONSTRUCTION OF THIS STRUCTURE. MSD CONTACT: BRIAN DUNN (314) 768-6387.

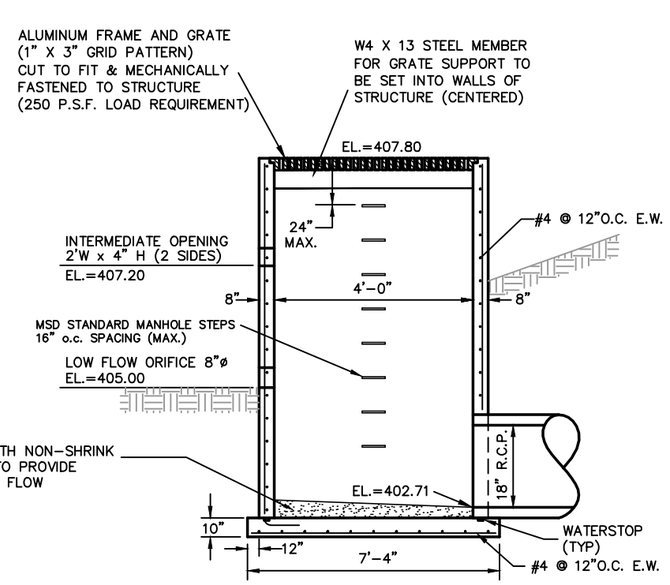



PLAN VIEW




SECTION B-B




SECTION A-A

## OUTFALL STRUCTURE #2.1

(N.T.S.)

# SITE IMPROVEMENT PLANS

A TRACT OF LAND BEING PART OF THE SE 1/4 OF SECTION 20,
TOWNSHIP 1 SOUTH, RANGE 14 WEST
CITY OF BRYANT, SALINE COUNTY, ARKANSAS

## LEGEND

- BENCH MARK
- FOUND IRON ROD
- FOUND IRON PIPE
- RIGHT OF WAY MARKER
- UTILITY POLE
- SUPPORT POLE
- UTILITY POLE WITH LIGHT
- LIGHT STANDARD
- ELECTRIC METER
- ELECTRIC MANHOLE
- ELECTRIC PEDESTAL
- ELECTRIC SPLICE BOX
- ELECTRIC BREAKER
- GAS DRIP
- GAS METER
- GAS VALVE
- TELEPHONE MANHOLE
- TELEPHONE PEDESTAL
- TELEPHONE SPLICE BOX
- CABLE TV PEDESTAL
- FIRE HYDRANT
- FIRE DEPARTMENT CONNECTION
- WATER MANHOLE
- WATER METER
- WATER VALVE
- POST INDICATOR VALVE
- CLEAN OUT
- STORM MANHOLE
- GRATED MANHOLE
- STORMWATER INLET
- GRATED STORMWATER INLET
- SANITARY MANHOLE
- TREE
- BUSH
- TRAFFIC SIGNAL
- PARKING METER
- STREET SIGN
- SPRINKLER
- MAIL BOX

## LINE TYPE LEGEND

- EX CONT MJR
- EX CONT MNR
- TREE LINE
- FEMA ELEV
- FEMA LIMIT
- PAVEMENT
- WALL
- GUARD RAIL
- CHAINLINK/WIRE FENCE
- WOOD/VINYL FENCE
- GAS
- UNDER GROUND ELEC
- OVERHEAD ELEC
- TELEPHONE LINE
- FIBER OPTIC LINE
- WATERLINE
- FLOODWAY
- SLOPE/LEVEE

## ABBREVIATIONS

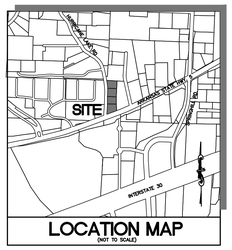
| | | |
|---|---|---|
| C.O. | – | CLEANOUT |
| DB. | – | DEED BOOK |
| E | – | ELECTRIC |
| FL | – | FLOWLINE |
| FT | – | FEET |
| FND. | – | FOUND |
| G | – | GAS |
| M.H. | – | MANHOLE |
| N/F | – | NOW OR FORMERLY |
| PB. | – | PLAT BOOK |
| PG. | – | PAGE |
| P.V.C. | – | POLYVINYL CHLORIDE PIPE |
| R.B. | – | RADIAL BEARING |
| R.C.P. | – | REINFORCED CONCRETE PIPE |
| SQ. | – | SQUARE |
| T | – | TELEPHONE CABLE |
| V.C.P. | – | VETRIFIED CLAY PIPE |
| W | – | WATER |
| (80'W) | – | RIGHT-OF-WAY WIDTH |

## GENERAL NOTES

1. BOUNDARY AND TOPOGRAPHIC SURVEY BY STOCK & ASSOCIATES CONSULTING ENGINEERS, INC.
2. ALL UTILITIES SHOWN HAVE BEEN LOCATED BY THE ENGINEER FROM AVAILABLE RECORDS. THEIR LOCATION SHOULD BE CONSIDERED APPROXIMATE. THE CONTRACTOR HAS THE RESPONSIBILITY TO NOTIFY ALL UTILITY COMPANIES, PRIOR TO CONSTRUCTION, TO HAVE EXISTING UTILITIES FIELD LOCATED.
3. ALL IMPROVEMENTS SHALL CONFORM TO THE CITY OF BRYANT STANDARDS AND SPECIFICATIONS.

## CONTACTS

SUMMIT UTILITIES – SHANE GIBBONS, (501) 581–9428




## PERTINENT DATA

| | |
|---|---|
| TRACT AREA: | 1.99 ± AC. |
| CURRENT OWNER: | NEATHERY SHARON CLYDENA |
| SITE ADDRESS: | 3205 HWY 5 N, BRYANT, AR 72019<br>2320 HURRICANE LAKE RD, BRYANT, AR 72019 |
| PARCEL ID: | 840–12042–000, 840–12038–000 |
| FEMA FLOOD MAP: | 05125C0360E (REVISED JUNE 05, 2020) |
| EXISTING ZONING: | "C–2" – HIGHWAY COMMERCIAL |
| PROPOSED USE: | COMMUNITY BUSINESS – MARIJUANA DISPENSARY |

## PARKING CALCS.

MINIMUM PARKING FOR C–2 DISTRICT:
1.0 SPACES PER 300 SF
(1,960 SF/300 SF) * 1.0 SPACE = 6.53 OR A MINIMUM OF 7 SPACES

PARKING SPACES PROVIDED = 36 SPACES (2 ADA)

## SHEET INDEX


| | |
|---|---|
| C1.0 | TITLE SHEET |
| C2.0 | SPECIFICATIONS |
| C3.0 | EXISTING CONDITIONS & DEMOLITION PLAN |
| C4.0 | STORMWATER POLLUTION PREVENTION PLAN |
| C4.1 | STORMWATER POLLUTION PREVENTION DETAILS |
| C5.0 | SITE GRADING PLAN |
| C6.0 | SITE UTILITY PLAN |
| C7.0 | SITE GEOMETRIC PLAN |
| C8.0 | SEWER PROFILE |
| C9.0 | CONSTRUCTION DETAILS |
| C9.1 | CONSTRUCTION DETAILS |
| C10.0 | PRE-DEVELOPED DRAINAGE AREA MAP |
| C10.1 | POST-DEVELOPED DRAINAGE AREA MAP |


**PREPARED FOR:**
GOOD DAY FARM
C/O REGAN ETHERIDGE
SENIOR PROJECT MANAGER–
STORE DEVELOPMENT, DESIGN & CONSTRUCTION
425 W. CAPITOL AVE.,
LITTLE ROCK, AR 72201

**USGS BENCHMARK**

*BENCHMARK# R 338 ELEV.=405.60 (NAVD88)*
*DESCRIBED BY ARKANSAS DEPARTMENT OF TRANSPORTATION 2013 THE STATION IS LOCATED ABOUT 5.9 MI (9.5 KM) EAST–SOUTHEAST OF CONGO, 3.0 MI (4.8 KM) WEST OF ALEXANDER AND 1.8 MI (2.9 KM) NORTH OF BRYANT.*
*TO REACH FROM THE INTERSECTION OF BASELINE ROAD AND NORTH FRONTAGE ROAD PARALLELING I–30, GO WEST ON NORTH FRONTAGE ROAD FOR 7.48 MITO THE STATION ON THE RIGHT, IN THE CENTER OF A HEADWALL.*
*IT IS 85 FT (25.9 M) WEST OF A COMBINATION POLE AND 20 FT (6.1 M) NORTH OF THE CENTERLINE OF NORTH FRONTAGE ROAD.*

**DISCLAIMER**

STOCK AND ASSOCIATES CONSULTING ENGINEERS, INC. AND THE UNDERSIGNED ENGINEER HAVE NO RESPONSIBILITY FOR SERVICES PROVIDED BY OTHERS TO IMPLEMENT THE IMPROVEMENTS SHOWN ON THIS PLAN AND ALL OTHER DRAWINGS WHERE THE UNDERSIGNED ENGINEER'S SEAL APPEARS. THE CONSTRUCTION MEANS AND METHODS ARE THE SOLE RESPONSIBILITY OF THE OWNER AND CONTRACTOR. STOCK AND ASSOCIATES CONSULTING ENGINEERS, INC. HAS NO RESPONSIBILITY TO VERIFY FINAL IMPROVEMENTS AS SHOWN ON THIS PLAN UNLESS SPECIFICALLY ENGAGED AND AUTHORIZED TO DO SO BY THE OWNER OR CONTRACTOR.


PREPARED BY:
STOCK & ASSOCIATES
Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH. (636) 530-9100 FAX (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:
GOOD DAY FARM - BRYANT
3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS
GEORGE M. STOCK
E-25116
REGISTERED PROFESSIONAL ENGINEER
06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05–14–2025 | JOB NO: 2025–7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
PRELIMINARY SITE PLAN

SHEET NO.:
1.0


Drawing File: S:\Drawings\2025\7775\Submittals\Preliminary\7775 Base.dwg LAYOUT: C1.0 File Saved: 6/25/2025 - Jun 25, 2025 - 3:05pm PLOTTED BY: Frank Alford

# GENERAL NOTES

1. SAFETY NOTICE TO CONTRACTOR: IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR SHALL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS.
2. THE CONTRACTOR SHALL ALSO BE SOLELY RESPONSIBLE FOR THE SAFETY FOR THE GENERAL PUBLIC AND PASSERBY WITH RESPECT TO WORK ZONE AREAS, MEANS AND METHODS AND PEDESTRIAN SAFETY.
3. ALL EXCAVATIONS, WHETHER THEY ARE FOR RETAINING WALLS, UTILITY TRENCHES OR FOOTING EXCAVATIONS, SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE LATEST OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) "CONSTRUCTION STANDARDS FOR EXCAVATIONS".
4. PROPERTY LINES, EASEMENTS AND TOPOGRAPHIC SURVEY BY STOCK & ASSOCIATES CONSULTING ENGINEERS.
5. ALL UTILITIES, STRUCTURES AND UNDERGROUND FACILITIES HAVE BEEN PLOTTED FROM BEST AVAILABLE RECORDS. THEREFORE, THE RELATIONSHIP BETWEEN PROPOSED WORK AND EXISTING FACILITIES, STRUCTURES AND UTILITIES MUST BE CONSIDERED APPROXIMATE; AND IT IS THE CONTRACTORS RESPONSIBILITY TO DETERMINE THEIR LOCATION AND THE EXISTENCE OF ANY NOT SHOWN. THE CONTRACTOR HAS THE RESPONSIBILITY TO NOTIFY ALL UTILITY COMPANIES, PRIOR TO CONSTRUCTION, TO HAVE EXISTING UTILITIES FIELD LOCATED, UNCOVERED AND DEPTHS VERIFIED TO AVOID CONFLICTS.
6. IT IS NOT WARRANTED THAT THESE PLANS CONTAIN COMPLETE INFORMATION REGARDING EASEMENTS, RESERVATIONS, RESTRICTIONS, RIGHT-OF-WAY, BUILDING LINES AND OTHER ENCUMBRANCES. FOR COMPLETE INFORMATION, A TITLE OPINION OR COMMITMENT FOR TITLE INSURANCE SHOULD BE OBTAINED.
7. THIS PLAN IS SUBJECT TO ALL LOCAL, STATE AND FEDERAL REGULATIONS. THERE HAS BEEN NO WETLAND DELINEATION, GEOTECHNICAL OR ENVIRONMENTAL DATA PROVIDED TO THIS ENGINEER PRIOR TO DESIGNING THIS PLAN.
8. THE CONTRACTOR SHALL NOTIFY THE ENGINEER IMMEDIATELY OF ANY CONFLICTS WITH PROPOSED IMPROVEMENTS.
9. IT IS THE CONTRACTORS RESPONSIBILITY TO ENSURE HE HAS THE LATEST SET OF IMPROVEMENT PLANS. CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR COORDINATING ALL PERMIT PLAN SETS AND ANY SUBSEQUENT PLAN ISSUANCES.
10. IMPROVEMENTS SHALL BE STAKED IN THE FIELD BY THE CONTRACTOR AND REVIEWED BY THE ARCHITECT AND OWNER PRIOR TO INSTALLATION. CONTRACTOR SHALL REVIEW OTHER SITE-RELATED SHEETS BY OTHER DESIGNERS (LANDSCAPING, ARCHITECT, ETC.) IN ADDITION TO CIVIL SHEETS FOR COORDINATION PURPOSES. ANY CONFLICTS SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER IMMEDIATELY AND PRIOR TO ANY START OF CONSTRUCTION.
11. THE CONTRACTOR SHALL MAINTAIN A COMPLETE SET OF RECORD DRAWINGS AT THE JOB SITE AND MARK THEREON ANY CHANGES AS THE WORK PROCEEDS. THE CONTRACTOR SHALL SUBMIT COMPUTER GENERATED, LEGIBLE RECORD DRAWINGS TO THE ENGINEER PRIOR TO FINAL INSPECTION AND ACCEPTANCE.
12. ALL WORK WITHIN PUBLIC RIGHT-OF-WAY SHALL BE TO CITY OF BRYANT OR ARKANSAS HIGHWAYS AND TRANSPORTATION STANDARDS, WHERE APPLICABLE.
13. ALL MATERIALS AND METHODS OF CONSTRUCTION TO MEET THE CURRENT STANDARDS AND SPECIFICATIONS OF CITY OF BRYANT OR ARKANSAS HIGHWAYS AND TRANSPORTATION, WHERE APPLICABLE.
14. THE CONTRACTOR SHALL COORDINATE AND/OR OBTAIN ALL NECESSARY LOCAL, STATE, AND FEDERAL PERMITS RELATED TO CONSTRUCTION OF THE IMPROVEMENTS.
15. PRIOR TO BEGINNING ANY WORK, THE CONTRACTOR SHALL CONTACT THE OFFICE OF THE OWNER FOR SPECIFIC INSTRUCTIONS RELEVANT TO THE SEQUENCING OF WORK.
16. ALL WORK MUST BE PERFORMED WITHIN EXISTING OR ACQUIRED EASEMENTS. AGENCY APPROVAL OF THESE PLANS DOES NOT AUTHORIZE OR CONDONE WORK OUTSIDE OF THE EASEMENTS.
17. THE DEVELOPER OR OWNER IS ADVISED THAT UTILITY COMPANIES MAY REQUIRE COMPENSATION FOR RELOCATION OF THEIR FACILITIES WITHIN THE PUBLIC RIGHT-OF-WAY. THE DEVELOPER OR OWNER SHALL ALSO BE MADE AWARE OF EXTENSIVE DELAYS IN UTILITY COMPANY RELOCATIONS AND ADJUSTMENTS WHICH MAY OCCUR.
THE DELAYS DUE TO UTILITY RELOCATION AND ADJUSTMENTS WILL NOT CONSTITUTE A CAUSE TO ALLOW OCCUPANCY PRIOR TO COMPLETION OF ROAD IMPROVEMENTS.
18. THE CONTRACTOR SHALL VERIFY PROPOSED AND COORDINATE PROPOSED SERVICES AND LOCATIONS OR RELOCATIONS WITH ALL UTILITIES. CONTRACTOR SHALL BE RESPONSIBLE TO OBTAIN ALL UTILITY PERMITS, UNLESS SPECIFICALLY MENTIONED OTHERWISE.
19. ALL PROPOSED UTILITIES TO BE LOCATED UNDERGROUND, UNLESS STATED OTHERWISE.
20. ALL HYDRANTS, POWER POLES OR OTHER OBSTRUCTIONS SHALL HAVE A MINIMUM TWO FOOT SETBACK FROM FACE OF CURB OR EDGE OF SHOULDER OF THE ULTIMATE PAVEMENT SECTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONFIRMING THIS REQUIREMENT, PRIOR TO CONSTRUCTION. ANY LOCATION WHICH DOES NOT MEET THIS REQUIREMENT SHALL BE BROUGHT TO THE ENGINEER'S ATTENTION IMMEDIATELY. THE CONTRACTOR SHALL ASSUME ALL LIABILITY IF CONFLICTS ARE NOT BROUGHT TO THE ENGINEERS ATTENTION FOR A DETERMINATION HOW TO PROCEED PRIOR TO CONSTRUCTION.
21. ALL TRAFFIC CONTROL DEVICES SHALL COMPLY WITH THE CURRENT EDITION OF THE MANUAL FOR UNIFORM TRAFFIC CONTROL DEVICES (MUTCD) AND ArDOT, WHERE APPLICABLE.
22. ACCESS TO PRIVATE PROPERTIES SHALL BE MAINTAINED AT ALL TIMES. EXISTING COMMERCIAL ENTRANCES MAY HAVE ACCESS RESTRICTED TO 1/2 OF THE ENTRANCE AT A TIME, UNLESS OTHERWISE APPROVED IN THIS PLAN SET.
23. NO SIDEWALK SHALL BE REMOVED WITHOUT CONFIRMING ADEQUATE PEDESTRIAN FACILITIES WILL EXIST DURING CONSTRUCTION. PROJECT NEEDS TO PROVIDE CONTINUOUS PEDESTRIAN ACCESS DURING CONSTRUCTION, UNLESS APPROVED ELSEWHERE. FOR SIDEWALK REMOVAL/REPLACEMENT VERIFY THERE IS ADEQUATE PEDESTRIAN ACCESS AROUND SITE, OR PROVIDE TEMPORARY PEDESTRIAN ACCESS.
24. IF A PEDESTRIAN DETOUR PLAN IS NOT INCLUDED IN THIS PLAN SET, THE CONTRACTOR SHALL BE RESPONSIBLE FOR CREATING A DETOUR PLAN AND SUBMITTING SAID PLAN TO THE ENGINEER AND AGENCIES FOR REVIEW AND APPROVAL.
25. ALL SIDEWALKS, CURB RAMPS, RAMPS, ACCESSIBLE PARKING SPACES SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE CURRENT APPROVED "AMERICANS WITH DISABILITIES ACT ACCESSIBILITY GUIDELINES" (ADAAG) ALONG WITH THE GRADES, CONSTRUCTION MATERIALS, SPECIFICATIONS, AND SIGNAGE. IF ANY CONFLICT OCCURS BETWEEN THE ABOVE INFORMATION AND THE PLANS, THE ADAAG GUIDELINES SHALL TAKE PRECEDENCE, AND THE CONTRACTOR, PRIOR TO ANY CONSTRUCTION, SHALL NOTIFY THE ENGINEER. THE CONTRACTOR SHALL VERIFY THESE IMPROVEMENTS WITH THE ENGINEER PRIOR TO INSTALLATION.
26. THE CONTRACTOR SHALL BE MADE AWARE THAT CERTAIN EXCEPTIONS TO ADA REQUIREMENTS MAY BE APPLICABLE. UNLESS SPECIFICALLY NOTED WITHIN THIS PLAN SET, THE CONTRACTOR SHALL ASSUME THAT NO EXCEPTION WILL APPLY.
27. ALL SIDEWALKS (THICKNESS AND WIDTH) AND CURB RAMPS TO BE CONSTRUCTED IN ACCORDANCE WITH ADA, CITY OF BRYANT OR ARKANSAS HIGHWAYS AND TRANSPORTATION STANDARDS.
28. ANY DISTURBED OFF-SITE PROPERTY (I.E. BUSHES, TREES, FENCES, MAILBOXES, ETC.), WHICH MAY NOT BE LABELED, SHALL BE REPLACED IN-KIND AT THE DEVELOPER'S EXPENSE.
29. SIGNAGE SHALL BE IN ACCORDANCE WITH CITY OF BRYANT SIGN ORDINANCE(S).

# STORM SEWER NOTES

1.) ALL CONCRETE PIPE SHALL BE REINFORCED, AND CONFORM TO A.S.T.M. DESIGNATION C76-80 CLASS UNLESS NOTED.

2.) ALL SEWER CONSTRUCTION AND MATERIALS TO BE IN ACCORDANCE WITH THE CITY OF BRYANT STREET, STORM DRAIN AND SANITARY SEWER SPECIFICATIONS AND STANDARDS.

3.) ALL TRENCHES UNDER AREAS TO BE PAVED AND UNDER EXISTING PAVING SHALL BE GRANULARLY FILLED WITH 3/4" CLEAN BACKFILL ONLY. BACKFILL SHALL BE PLACED IN ACCORDANCE WITH CITY OF BRYANT STANDARDS.

4.) ALL TRENCH BACKFILLS UNDER PAVEMENT WITHIN THE PUBLIC RIGHT-OF-WAY SHALL BE GRANULAR BACKFILLED. TRENCH BACKFILLS UNDER PAVED AREAS, OUTSIDE OF PUBLIC RIGHT-OF-WAY SHALL BE GRANULAR BACKFILL IN LIEU OF THE EARTH BACKFILL COMPACTED TO 95 PERCENT OF THE STANDARD AASHTO T-99 COMPACTION TEST A.S.T.M. D-698.

5.) JETTING IS NOT AN ACCEPTABLE METHOD OF ACHIEVING BACKFILL COMPACTION. ALL BACKFILL MATERIAL SHALL BE MECHANICALLY COMPACTED TO AT LEAST 95 PERCENT OF THE MATERIAL'S STANDARD PROCTOR MAXIMUM DRY DENSITY.

6.) FOR SEWER PIPE (STORM AND SANITARY) WITH A DESIGN GRADE LESS THAN ONE PERCENT (1%), VERIFICATION OF THE PIPE GRADE WILL BE REQUIRED FOR EACH INSTALLED REACH OF SEWER, PRIOR TO ANY SURFACE RESTORATION OR INSTALLATION OF ANY SURFACE IMPROVEMENTS. THE CONTRACTOR'S FIELD SUPERVISOR WILL BE REQUIRED TO PROVIDE DAILY DOCUMENTATION VERIFYING THAT THE AS-BUILT PIPE GRADE MEETS THE DESIGN GRADE THROUGH THE SUBMITTAL OF SIGNED CUT SHEETS TO THE CITY OF BRYANT INSPECTOR UPON REQUEST.

FIELD SURVEYED VERIFICATION MUST BE MADE UNDER THE DIRECTION OF A LICENSED LAND SURVEYOR OR REGISTERED ENGINEER. THE CONTRACTOR WILL BE REQUIRED TO REMOVE AND REPLACE ANY SEWER REACH HAVING AN AS-BUILT GRADE WHICH IS FLATTER THAN THE DESIGN GRADE BY MORE THAN 0.1%.
SEWERS WITH GRADES GREATER THAN THE DESIGN SLOPE MAY BE LEFT IN PLACE, PROVIDED NO OTHER SEWER GRADE IS REDUCED BY THIS VARIANCE IN THE AS-BUILT GRADE.

THE CITY ALSO RESERVES THE RIGHT TO REQUIRE THE CONTRACTOR TO REMOVE AND REPLACE ANY SEWER (AT ANY TIME PRIOR TO CONSTRUCTION APPROVAL) FOR WHICH THE AS-BUILT GRADE DOES NOT COMPLY WITH THE GRADE TOLERANCE STATED IN THE ABOVE PARAGRAPH.

THE SEWER CONTRACTOR SHALL BE RESPONSIBLE FOR ANY COSTS ASSOCIATED WITH THE FIELD VERIFICATION OF THE SEWER GRADE, OR REMOVAL AND REPLACEMENT OF THE SEWER PIPE OR ASSOCIATED APPURTENANCES.

7.) ADJUSTMENT OF MANHOLE TO GRADE:
IF A MANHOLE IS TO BE RAISED: MANHOLES MAY BE RAISED USING COURSES OF BRICK OR APPROVED GRADE RING(S), PROVIDED THE TOTAL ADJUSTMENT OF THE MANHOLE DOES NOT EXCEED 12-INCHES (INCLUDING THE EXISTING RINGS OR COURSES OF BRICK). FOR MANHOLES WHICH WILL EXCEED THE MAXIMUM OF
12-INCHES, THE TRANSITION SECTION OF THE STRUCTURE SHALL BE REMOVED AND THE BOTTOM SECTION RAISED USING THE SAME MATERIAL AS THE EXISTING STRUCTURE.

IF A MANHOLE IS TO BE LOWERED:
MANHOLES MAY BE LOWERED BY REMOVING THE TRANSITION SECTION, AND LOWERING THE EXISTING BOTTOM SECTION BY SAWCUTTING THE EXISTING CAST-IN-PLACE CONCRETE, REMOVING THE REQUIRED COURSES OF BRICK, OR REMOVING THE PRECAST RISER SECTION AS APPROPRIATE.

# DEMOLITION NOTES

1. CONTRACTOR SHALL VISIT THE PROJECT SITE TO DETERMINE EXTENT OF DEMOLITION.
2. USE OF EXPLOSIVES OR BURNING IS NOT PERMITTED.
3. PAVEMENT AREAS, CURBS, BUILDINGS, TREES, ETC. SHALL BE REMOVED IN COMPLIANCE WITH ALL GOVERNING AGENCIES.
4. CONTRACTOR SHALL OBTAIN HAUL ROUTE APPROVAL FROM CITY OF BRYANT OR ARKANSAS DEPARTMENT OF TRANSPORTATION PRIOR TO COMMENCEMENT OF HAULING OPERATIONS, IF REQUIRED.
5. THE CONTRACTOR SHALL NOTIFY THE APPROPRIATE UTILITY COMPANY PRIOR TO BEGINNING ANY WORK THAT WILL AFFECT AN EXISTING UTILITY.
6. CONTRACTOR TO COORDINATE RELOCATIONS, ABANDONMENT OR REMOVAL OF EXISTING UTILITIES WITH UTILITY COMPANIES TO AVOID INTERRUPTION OF SERVICE TO BUILDINGS OUTSIDE OF SPECIFIED PHASE OF WORK.
7. CONTRACTOR SHALL COORDINATE ALL UTILITY SERVICE INSTALLATIONS, REMOVALS, RELOCATIONS AND ABANDONMENT WITH PROPOSED IMPROVEMENTS. CONTRACTOR SHALL AVOID CONDITION WHERE NEW PAVEMENT, CURBING, SIDEWALK, ETC. WILL BE DISTURBED BY UTILITY INSTALLATION.
8. ALL EROSION CONTROL AND SILTATION CONTROL MEASURES SHALL BE IN PLACE PRIOR TO DEMOLITION.
9. PROTECT EXISTING TREES AND VEGETATION INDICATED TO REMAIN SHALL BE PROTECTED AGAINST UNNECESSARY CUTTING OR SKINNING OF ROOTS, BRANCHES OR BARK, SMOTHERING OF TREES BY STOCKPILE MATERIAL, OR PARKING VEHICLES WITHIN DRIP LINE. PROTECT TREES AND VEGETATION TO REMAIN WITH TEMPORARY CONSTRUCTION FENCING, PRIOR TO SITE CLEARING OPERATIONS.
10. EXISTING PROPERTY CORNERS AND/OR SURVEY MONUMENTS DISTURBED BY CONSTRUCTION TO BE REMOVED AND REPLACED BY LICENSED SURVEYOR IN MISSOURI.
11. REMOVAL AND/OR ABANDONMENT OF EXISTING SEWERS SHALL BE IN ACCORDANCE WITH THE STANDARD CONSTRUCTION SPECIFICATIONS FOR SEWER AND DRAINAGE FACILITIES OF ArDOT OR THE CITY OF BRYANT SEWER DISTRICT, WHERE APPLICABLE.
12. EXISTING SEWERS INDICATED TO BE REMOVED AND/OR ABANDONED SHALL BE SECURELY BLOCKED AT ANY POINTS OF INTAKE OR DISCHARGE (OF THE SYSTEM TO REMAIN) WITH THE BULKHEAD OR PREFORMED PLUG. IF THE SEWER IS ABANDONED, IT SHALL BE COMPLETELY FILLED WITH GROUT.
13. ANY SEWER INLETS INDICATED TO REMAIN IN PLACE BUT ARE CHOKED SHALL BE CLEANED OUT AND POSITIVE FLOW SHALL BE VERIFIED. IF INLETS ARE UNABLE TO BE REPAIRED, THE ENGINEER SHALL BE NOTIFIED IMMEDIATELY.
14. EXISTING WATER METERS, HYDRANTS AND VALVES INDICATED TO REMAIN SHALL HAVE CONNECTING PIPES FIELD LOCATED AND ANY CONFLICTS WITH THE PROPOSED IMPROVEMENTS SHALL BE REPORTED TO THE ENGINEER.
15. CONSTRUCTION DEBRIS, INCLUDING BUT NOT LIMITED TO, CONDUIT, DUCTS, FITTINGS, VALVES, PIPES AND OTHER DEBRIS TO BE REMOVED, SHALL BE DISPOSED OF OFF-SITE, AND IN ACCORDANCE WITH ALL LOCAL, STATE AND FEDERAL REGULATIONS.
16. CONTRACTOR TO PROVIDE ALL NECESSARY FENCING, BARRICADES, SIGNAGE, ETC. FOR PEDESTRIAN SAFETY DURING SITE DEMOLITION/CONSTRUCTION ACTIVITIES.
17. A PEDESTRIAN DETOUR PLAN SHALL BE IMPLEMENTED IF PUBLIC SIDEWALKS ARE TO BE CLOSED DURING CONSTRUCTION.
18. DEMOLITION LIMITS OF EXISTING SIDEWALK, CURB LINE, CURB RAMPS AND ROADWAY HAS BEEN APPROXIMATED AND SHOWN ON THE DEMOLITION SHEET(S).
19. REMOVAL OF PAVEMENT, CURB & GUTTER, SIDEWALKS, ETC. SHALL BE TO THE NEAREST EXISTING JOINT OR FULL DEPTH SAWCUT AT LIMITS OF REMOVAL.
20. SAWCUTTING, CURB AND PAVEMENT REMOVALS TO BE COORDINATED WITH INSTALLATION OF PROPOSED UTILITY MAINS AND SERVICES WITH INSTALLATION OF PROPOSED UTILITY MAINS AND SERVICES. CONTRACTOR TO CONTACT UTILITY COMPANIES TO COORDINATE PAVEMENT REMOVAL AND/OR REPLACEMENT BY UTILITY COMPANY WITH ON-SITE DEMOLITION BY CONTRACTOR.
21. EXISTING PAVEMENT SHOWN TO BE REMOVED SHALL REQUIRE BACKFILL AND PROPER COMPACTION WITH GRADES TO BE RE-ESTABLISHED TO AVOID CONDITIONS WHERE PONDING WATER OCCURS.
23. DEBRIS AND FOUNDATION MATERIAL FROM ANY EXISTING ON-SITE BUILDING OR STRUCTURE WHICH IS SCHEDULED TO BE RAZED FOR THIS DEVELOPMENT MUST BE PROPERLY DISPOSED OF OFF-SITE.
24. CONTRACTOR TO COORDINATE REMOVAL AND/OR DISCONNECTION OF EXISTING SERVICE LINES TO ANY BUILDING PRIOR TO BUILDING DEMOLITION.

# SANITARY SEWER NOTES

1.) ALL SEWER CONSTRUCTION AND MATERIALS TO BE IN ACCORDANCE WITH THE CITY OF ST. CLAIR SPECIFICATIONS AND STANDARDS.

2.) 6" AND 8" LATERALS CONSTRUCTED OF P.V.C.S.D. R.-35 THICKWALL PIPE, A.S.T.M. D-3034.

3.) 6" AND 8" LATERAL JOINTS TO CONFORM TO A.S.T.M. STANDARD S.D.R.-35 THICKWALL COMPRESSION JOINT FOR P.V.C..

4.) ALL MANHOLE FRAMES AND COVERS SHALL BE M.S.D. STANDARD FRAME AND COVER.

5.) ALL LATERAL SEWER CONSTRUCTION METHODS TO CONFORM TO LATEST STANDARDS AND SPECIFICATIONS OF THE CITY OF ST. CLAIR PLUMBING CODE.

6.) ALL TRENCHES UNDER AREAS TO BE PAVED SHALL BE GRANULARLY FILLED WITH 3/4" CLEAN ROCK BEDDING. BACKFILL SHALL BE PLACED IN ACCORDANCE WITH THE CITY OF ST. CLAIR SPECIFICATIONS AND STANDARDS.

7) CONTRACTOR TO START LAYING PIPE AT DOWNSTREAM MANHOLE AND WORK UPSTREAM.

8.) CLEANOUTS SHALL BE LOCATED AT ALL HORIZONTAL AND VERTICAL CHANGES IN DIRECTION OF FLOW OF HOUSE LATERALS AND ANY SANITARY LATERAL OF 100 FEET OR LONGER.

9.) HAUNCH CATEGORY I BEDDING PER CITY STANDARDS REQUIRED FOR PIPES IN ROCK.

10.) VERTICAL CLEARANCE BETWEEN SEWER AND WATER MAINS SHALL BE A MINIMUM OF 2' - 0".

11.) ALL TRENCH BACKFILLS UNDER PAVEMENT WITHIN THE PUBLIC RIGHT-OF-WAY SHALL BE GRANULAR BACKFILLED. TRENCH BACKFILLS UNDER PAVED AREAS, OUTSIDE OF PUBLIC RIGHT-OF-WAY SHALL BE GRANULAR BACKFILL IN LIEU OF THE EARTH BACKFILL COMPACTED TO 95 PERCENT OF THE STANDARD AASHTO T-99 COMPACTION TEST A.S.T.M. D-698.

12.) JETTING IS NOT AN ACCEPTABLE METHOD OF ACHIEVING BACKFILL COMPACTION. ALL BACKFILL MATERIAL SHALL BE MECHANICALLY COMPACTED TO AT LEAST 95 PERCENT OF THE MATERIAL'S STANDARD PROCTOR MAXIMUM DRY DENSITY.

13.) FOR SEWER PIPE (STORM AND SANITARY) WITH A DESIGN GRADE LESS THAN ONE PERCENT (1%), VERIFICATION OF THE PIPE GRADE WILL BE REQUIRED FOR EACH INSTALLED REACH OF SEWER, PRIOR TO ANY SURFACE RESTORATION OR INSTALLATION OF ANY SURFACE IMPROVEMENTS. THE CONTRACTOR'S FIELD SUPERVISOR WILL BE REQUIRED TO PROVIDE DAILY DOCUMENTATION VERIFYING THAT THE AS-BUILT PIPE GRADE MEETS THE DESIGN GRADE THROUGH THE SUBMITTAL OF SIGNED CUT SHEETS TO THE CITY OF ST. CLAIR INSPECTOR UPON REQUEST.

FIELD SURVEYED VERIFICATION MUST BE MADE UNDER THE DIRECTION OF A LICENSED LAND SURVEYOR OR REGISTERED ENGINEER. THE CONTRACTOR WILL BE REQUIRED TO REMOVE AND REPLACE ANY SEWER REACH HAVING AN AS-BUILT GRADE WHICH IS FLATTER THAN THE DESIGN GRADE BY MORE THAN 0.1%. SEWERS WITH GRADES GREATER THAN THE DESIGN SLOPE MAY BE LEFT IN PLACE, PROVIDED NO OTHER SEWER GRADE IS REDUCED BY THIS VARIANCE IN THE AS-BUILT GRADE.

THE CITY ALSO RESERVES THE RIGHT TO REQUIRE THE CONTRACTOR TO REMOVE AND REPLACE ANY SEWER (AT ANY TIME PRIOR TO CONSTRUCTION APPROVAL) FOR WHICH THE AS-BUILT GRADE DOES NOT COMPLY WITH THE GRADE TOLERANCE STATED IN THE ABOVE PARAGRAPH.

THE SEWER CONTRACTOR SHALL BE RESPONSIBLE FOR ANY COSTS ASSOCIATED WITH THE FIELD VERIFICATION OF THE SEWER GRADE, OR REMOVAL AND REPLACEMENT OF THE SEWER PIPE OR ASSOCIATED APPURTENANCES.

14.) ADJUSTMENT OF MANHOLE TO GRADE:
IF A MANHOLE IS TO BE RAISED: MANHOLES MAY BE RAISED USING COURSES OF BRICK OR APPROVED GRADE RING(S), PROVIDED THE TOTAL ADJUSTMENT OF THE MANHOLE DOES NOT EXCEED 12-INCHES (INCLUDING THE EXISTING RINGS OR COURSES OF BRICK). FOR MANHOLES WHICH WILL EXCEED THE MAXIMUM OF 12-INCHES, THE TRANSITION SECTION OF THE STRUCTURE SHALL BE REMOVED AND THE BOTTOM SECTION RAISED USING THE SAME MATERIAL AS THE EXISTING STRUCTURE.

IF A MANHOLE IN TO BE LOWERED: MANHOLES MAY BE LOWERED BY REMOVING THE TRANSITION SECTION, AND LOWERING THE EXISTING BOTTOM SECTION BY SAWCUTTING THE EXISTING CAST-IN-PLACE CONCRETE, REMOVING THE REQUIRED COURSES OF BRICK, OR REMOVING THE PRECAST RISER SECTION AS APPROPRIATE.

15.) FOUNDATION DRAINS, IF INSTALLED, SHALL NOT CONNECT TO THE SANITARY SEWER.

16.) EXTERNAL GREASE TRAP REQUIRED. GREASE TRAP TO BE LOCATED IN AN ACCESSIBLE LOCATION FOR CITY INSPECTION. GREASE TRAP TO PROVIDE MEANS FOR VISUAL INSPECTION FROM ABOVE FOR BOTH THE INFLUENT AND EFFLUENT SIDES.

17.) ALL SEWER CONSTRUCTION AND MATERIALS TO BE IN ACCORDANCE WITH THE CITY OF ST. CLAIR SPECIFICATIONS AND STANDARDS.

18.) ALL SEWER CONSTRUCTION AND MATERIALS TO BE IN ACCORDANCE WITH THE CLEAN WATER ACT.

# GRADING NOTES

1. ALL EROSION AND SILTATION CONTROL SHALL BE INSTALLED PRIOR TO STARTING CONSTRUCTION OR GRADING.
2. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTORS TO CONSULT PROJECT GEOTECHNICAL ENGINEER(S), FOR REVIEW OF THIS PLAN PRIOR TO GRADING OPERATIONS AND FOR GRADING RECOMMENDATIONS AND FIELD TESTING.
3. PROPOSED GRADES AND CONTOURS SHOWN ARE TO FINISHED ELEVATION. CONTRACTOR TO ACCOUNT FOR ALL TOP FINISHES INCLUDING BUT NOT LIMITED TO PAVEMENT, SUB-BASES, SOD, TOPSOIL, RIP-RAP AND FIELD TOP MIXES.
4. ALL GRADING WILL UTILIZE STANDARD GRADING EQUIPMENT TO ACHIEVE THE PROPOSED GRADES SHOWN ON THIS PLAN.
5. TOP OF SEWER STRUCTURE ELEVATIONS SHALL BE VERIFIED BY THE CONTRACTOR IN THE FIELD PRIOR TO FINAL INSTALLATION OF STRUCTURE TOP.
6. THE ENGINEER ASSUMES NO RESPONSIBILITY FOR COSTS INCURRED DUE TO UNSUITABLE MATERIAL THAT MUST BE REMOVED FROM SITE.
7. NO EXCAVATION SHALL BE MADE SO CLOSE TO THE PROPERTY LINE AS TO ENDANGER ANY ADJOINING PROPERTY OF ANY PUBLIC OR PRIVATE STREET WITHOUT SUPPORTING AND PROTECTING SUCH PUBLIC OR PRIVATE STREET, PROPERTY OR UTILITY FROM SETTLING, CRACKING OR OTHER DAMAGE.
8. ALL EXCAVATIONS, GRADING OR FILLING SHALL HAVE A FINISHED GRADE NOT TO EXCEED A 3:1 SLOPE (33%), UNLESS SPECIFICALLY APPROVED OTHERWISE.
9. EARTHWORK QUANTITIES ARE THE RESPONSIBILITY OF CONTRACTORS. THE CONTRACTOR IS RESPONSIBLE FOR HAUL-ON OR HAUL-OFF MATERIAL FROM SITE, AS MAY BE REQUIRED.
10. ALL FILLS AND BACKFILLS SHALL BE MADE OF SELECTED EARTH MATERIALS FREE FROM BROKEN MASONRY, ROCK, FROZEN EARTH, RUBBISH, ORGANIC MATERIAL AND DEBRIS, AND AS APPROVED BY THE PROJECT GEOTECHNICAL ENGINEER.
11. ALL FILLS PLACED UNDER PROPOSED STORM AND SANITARY SEWER LINES AND/OR PAVED AREAS, INCLUDING TRENCH BACKFILLS AND WITHIN AND OFF THE ROAD RIGHT-OF-WAY, SHALL BE COMPACTED TO 90% OF MAXIMUM DENSITY AS DETERMINED BY THE "MODIFIED AASHTO T-180 COMPACTION TEST" (ASTM D-1557) FOR THE ENTIRE DEPTH OF THE FILL. COMPACTED GRANULAR BACKFILL IS REQUIRED IN ALL TRENCH EXCAVATION WITHIN THE STREET RIGHT-OF-WAY AND UNDER ALL PAVED AREAS. ALL TESTS SHALL BE PERFORMED UNDER THE DIRECTION OF AND VERIFIED BY A SOILS ENGINEER CONCURRENT WITH GRADING AND BACKFILLING OPERATIONS.
12. SOFT SOILS IN THE BOTTOM AND BANKS OF ANY EXISTING OR FORMER POND SITES OR TRIBUTARIES OR ANY SEDIMENT BASINS OR TRAPS SHOULD BE REMOVED, SPREAD OUT AND PERMITTED TO DRY SUFFICIENTLY TO BE USED AS FILL. NONE OF THIS MATERIAL SHOULD BE PLACED IN PROPOSED PUBLIC RIGHT-OF-WAY LOCATIONS OR IN ANY STORM SEWER LOCATIONS.
13. THE CONTRACTOR SHALL VERIFY THAT ALL AREAS WILL DRAIN POSITIVELY AND WITHOUT PONDING PRIOR TO INSTALLATION OF IMPROVEMENTS.
14. STORMWATER TO BE DISCHARGED AT ADEQUATE NATURAL DISCHARGE POINT. SINKHOLES ARE NOT AN ADEQUATE NATURAL DISCHARGE POINTS.
15. ANY WELLS, CISTERNS AND/OR SPRINGS, WHICH MAY EXIST ON THE PROPERTY, SHOULD BE LOCATED AND SEALED IN A MANNER ACCEPTABLE TO CITY OF BRYANT AND THE ARKANSAS DEPARTMENT OF AGRICULTURE .
16. DESIGN OF SHORING FOR UTILITY TRENCHES AND/OR SEWER CONSTRUCTION IS THE RESPONSIBILITY OF THE CONTRACTOR, UNLESS OTHERWISE NOTED IN THIS SET OF PLANS.
17. TRUCKS SHALL NOT EXCEED POSTED WEIGHT LIMITS FOR ANY ROAD TRAVELED OR BRIDGES DURING HAUL OPERATIONS.
18. CONTRACTOR SHALL OBTAIN HAUL ROUTE APPROVAL FROM CITY OF BRYANT OR ARKANSAS DEPARTMENT OF TRANSPORTATION PRIOR TO COMMENCEMENT OF HAULING OPERATIONS, IF REQUIRED.
19. PROTECT EXISTING TREES AND VEGETATION INDICATED TO REMAIN SHALL BE PROTECTED AGAINST UNNECESSARY CUTTING OR SKINNING OF ROOTS, BRANCHES OR BARK, SMOTHERING OF TREES BY STOCKPILE MATERIAL, OR PARKING VEHICLES WITHIN DRIP LINE. PROTECT TREES AND VEGETATION TO REMAIN WITH TEMPORARY CONSTRUCTION FENCING, PRIOR TO SITE CLEARING OPERATIONS.
20. ALL OPEN SPACE DETENTION AREAS SHALL BE REVEGETATED WITH BERMUDA SOD.


PREPARED BY:
STOCK & ASSOCIATES
Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS
GEORGE M. STOCK
REGISTERED PROFESSIONAL ENGINEER
No. 9125
06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO.: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
SPECIFICATIONS

SHEET NO.:
2.0


Drawing No.: S:\DRAWINGS\2025\7775\Construction\Plans\7775 Site.dwg, LAYOUT: C2 Sheet, 5/27/2025 10:41:25 AM, User: ALEXIS, Xref: None

## DEMO LEGEND

TBR = TO BE REMOVED

TBA = TO BE ABANDONED

TBR&R = TO BE REMOVED & REPLACED

DND = DO NOT DISTURB

UIP = USE IN PLACE

ATG = ADJUST TO GRADE

– – – – LIMITS OF DISTURBANCE

GRAPHIC SCALE

30 0 15 30 60 120

( IN FEET )

1 inch = 30 ft.

PREPARED BY:


STOCK & ASSOCIATES Consulting Engineers, Inc.

257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS GEORGE M. STOCK 25116 REGISTERED PROFESSIONAL ENGINEER GEORGE STOCK

06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

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| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:

EXISTING CONDITIONS AND DEMOLITION PLAN

SHEET NO.:

C3.0


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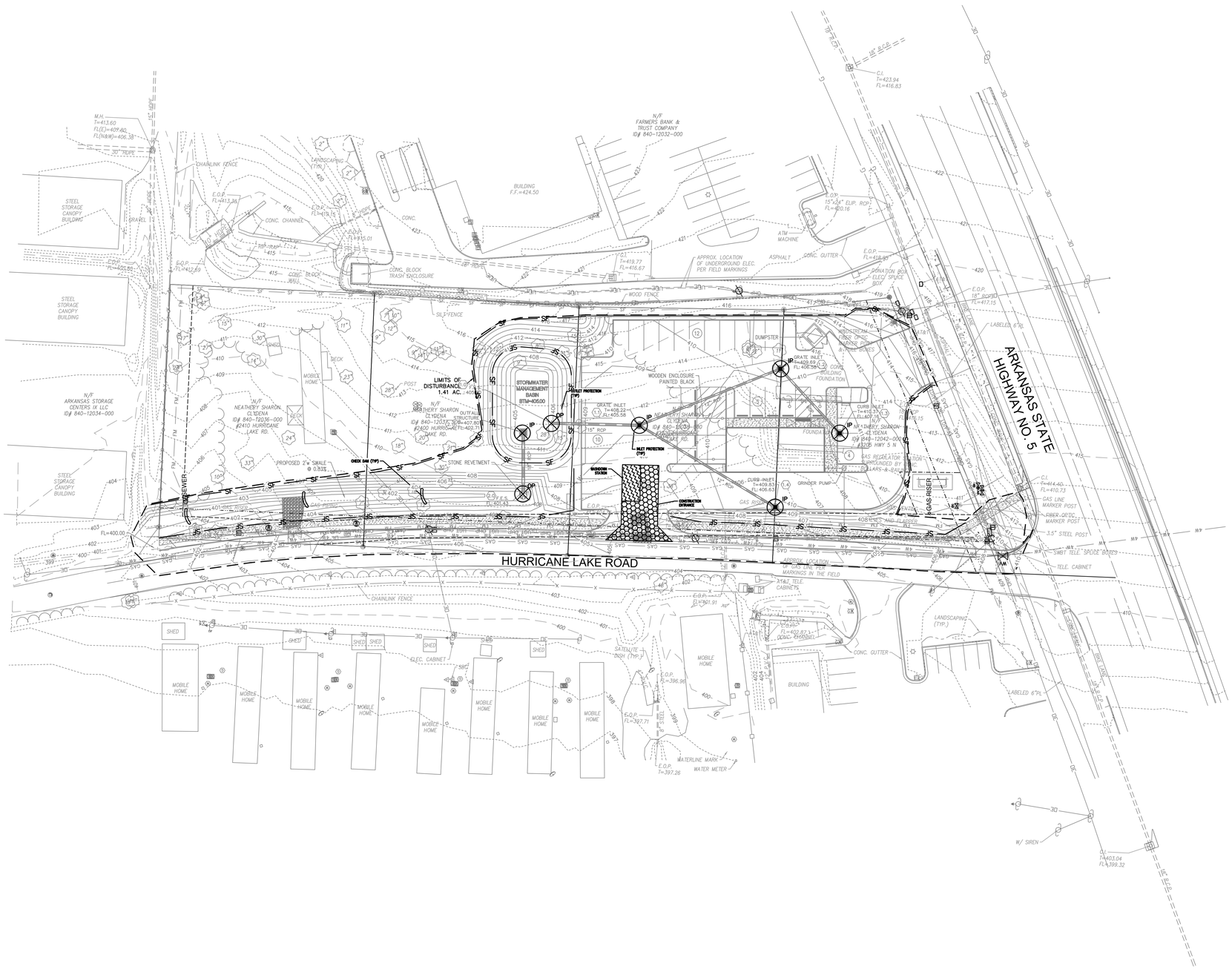
## SWPPP LEGEND

- IP — INLET PROTECTION
- OP — OUTLET PROTECTION
- CONSTRUCTION ENTRANCE
- WASHDOWN STATION
- SF — SILTATION FENCE
- DISTURBED LIMITS
- CHECK DAM

**TOTAL AREA DISTURBED: 1.41 Ac.±**

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e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS GEORGE M. STOCK REGISTERED PROFESSIONAL ENGINEER No. 25116

06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

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|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. # |
| M.D.N.R. #: | |

SHEET TITLE:
STORMWATER POLLUTION PREVENTION PLAN

SHEET NO.:
C4.0

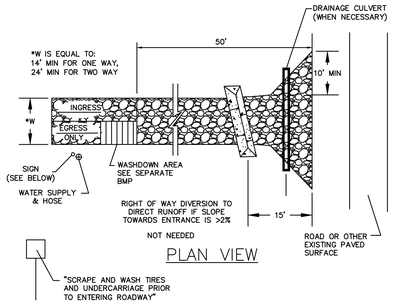

DRAWING FILE: S:\DRAWINGS\2025\7775\Civil\Permitting\7775Base.dwg LAYOUT: C4.0 SWPPP PLOTTED: Jun 25, 2025 - 9:56am PLOTTED BY: Lisa Weber

## STORM WATER POLLUTION PREVENTION PLAN NOTES

1. IT IS THE RESPONSIBILITY OF ALL CONTRACTORS TO CONTACT UTILITY COMPANIES AT LEAST 48 HOURS PRIOR TO ANY EXCAVATION ON OR RELATING TO THIS PROJECT. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO MAKE OR ARRANGE FOR THE RELOCATION OF ANY UTILITIES AFFECTED BY THE PROJECT CONSTRUCTION.
2. CONTRACTOR SHALL TAKE ALL MEASURES NECESSARY TO PROTECT THE ADJOINING PROPERTIES FROM THE DELETERIOUS EFFECTS OF EROSION UNTIL PROJECT COMPLETION AND ACCEPTANCE.
3. SOIL SHALL BE COMPACTED IN ACCORDANCE WITH THE CITY OF BRYANT AND SALINE COUNTY STANDARD SPECIFICATIONS FOR STREET CONSTRUCTION.
4. 6" OF TOPSOIL SHALL BE STRIPPED UNDER ALL FILL AREAS.
5. FIBER ROLLS AND WATTLES SHALL BE USED AS INLET PROTECTION FOR INLETS WITHIN PARKING LOTS AND ALONG ROADWAYS.
6. EROSION AND SILTATION CONTROL SHALL BE INSTALLED AND BE MAINTAINED THROUGHOUT THE PROJECT UNTIL/ACCEPTANCE OF THE WORK BY THE VA AND ADEQUATE VEGETATIVE GROWTH INSURES NO FURTHER EROSION OF THE SOIL.
7. AT LEAST ONCE EVERY WEEK AND AFTER EVERY RAINFALL EVENT OF 0.25 INCHES OR MORE, EROSION AND SILTATION CONTROL DEVICES SHALL BE INSPECTED BY THE CONTRACTOR FOR DAMAGE AND AMOUNT OF SEDIMENTATION ACCUMULATED AND CORRECTIVE ACTIONS TAKEN.
8. TEMPORARY SILTATION CONTROL MEASURES (STRUCTURAL) SHALL BE MAINTAINED UNTIL VEGETATIVE COVER IS ESTABLISHED AT A SUFFICIENT DENSITY TO PROVIDE EROSION CONTROL ON THE SITE.
9. WHERE NATURAL VEGETATION IS REMOVED DURING GRADING, VEGETATION SHALL BE REESTABLISHED IN SUCH A DENSITY AS TO PREVENT EROSION.
10. WHEN GRADING OPERATIONS ARE COMPLETED OR SUSPENDED FOR MORE THAN 5 DAYS IN ANY AREA, THE DISTURBED AREA SHALL BE SEEDED OR OTHERWISE STABILIZED TO SIGNIFICANTLY REDUCE THE ERODING OF THE SOIL. PROTECTIVE MEASURES MAY INCLUDE A COMBINATION OF SEEDING, SODDING, MULCHING OR OTHER SUITABLE MEANS TO PROTECT THE GROUND SURFACE FROM EROSION.
11. IF CUT AND FILL OPERATIONS OCCUR DURING A SEASON NOT FAVORABLE FOR IMMEDIATE ESTABLISHMENT OF PERMANENT GROUND COVER, A FAST GERMINATING ANNUAL SUCH AS RYE GRASSES SHALL BE UTILIZED TO RETARD EROSION, IF EROSION CONTROL DEVICES HAVE NOT BEEN ESTABLISHED.
12. ALL FINISHED GRADES (AREAS NOT TO BE DISTURBED BY FUTURE IMPROVEMENT) IN EXCESS OF 20% SLOPES (5:1) SHALL BE MULCHED AND TACKED AT THE RATE OF 100 POUNDS PER 1,000 SQUARE FEET WHEN SEEDED.
13. STORM WATER PIPES, OUTLETS AND CHANNELS SHALL BE PROTECTED BY SILT BARRIERS AND KEPT FREE OF WASTE AND SILT AT ALL TIMES PRIOR TO FINAL SURFACE STABILIZATION AND/OR PAVING.
14. SEDIMENT BUILD-UP REMOVED DURING ROUTINE BMP MAINTENANCE SHALL REMAIN ON-SITE. SEDIMENT SHALL BE RELOCATED TO WITHIN THE STOCKPILE AREA OR TO A LEVEL AREA (1% MAX.) ABSENT OF CONCENTRATED FLOWS. LEVEL OUT SEDIMENT AND ALLOW TO DRY.
15. THE SILTATION CONTROL NOTES, IMPLEMENTATION SCHEDULE, AND SILTATION CONTROL DETAILS, ALONG WITH THE SILTATION CONTROL PLANS INCLUDED ON SHEET C4.1 CONSTITUTE THE STORMWATER POLLUTION PREVENTION PLAN AND IS INFORMATIONAL IN NATURE. THE CONTRACTOR IS REQUIRED TO CREATE A PROJECT SPECIFIC EROSION CONTROL PLAN AND UPDATE IT THROUGHOUT CONSTRUCTION.

## SILTATION IMPLEMENTATION SCHEDULE

1. INSTALL PERIMETER SILTATION CONTROL AND CONSTRUCTION ENTRANCE.
2. DEMO EXISTING PARKING LOT AND BEGIN PLACING AGGREGATE BASE IN PAVEMENT AREAS ONCE AREA HAS REACHED FINAL GRADE TO PREVENT EROSION.
3. PLACE SILT FENCE AROUND EACH STORM SEWER INLET AS IT IS CONSTRUCTED.
4. IMMEDIATELY SOD GRADED AREAS UPON REACHING FINAL GRADE THAT ARE TO BE PERMANENTLY TURFED.




## CONSTRUCTION ENTRANCE/WASHDOWN/PARKING AREA - PROFILE

N.T.S.
(SEE SHEET C4.0 FOR LOCATION)

## CONSTRUCTION ENTRANCE:

INSTALLATION/CONSTRUCTION PROCEDURES:

1. GRADE AND COMPACT AREA OF CONSTRUCTION ENTRANCE
2. INSTALL CULVERT UNDER ENTRANCE IF NEEDED TO MAINTAIN POSITIVE DRAINAGE
3. PLACE FABRIC AND COVER WITH AGGREGATE, FORMING DIVERSION ACROSS ENTRANCE IF NEEDED TO DIRECT RUNOFF AWAY FROM ROADWAY
4. SEE WASHDOWN STATION BMP FOR ADDITIONAL STEPS

OPERATIONS & MAINTENANCE PROCEDURES:

1. IMMEDIATELY REMOVE ANY MUD OR DEBRIS TRACKED ONTO PAVED SURFACES
2. REMOVE SEDIMENT AND CLODS OF DIRT FROM CONSTRUCTION ENTRANCE CONTINUOUSLY
3. REPLACE ROCK IF NECESSARY TO MAINTAIN CLEAN SURFACE
4. REPAIR SETTLED AREAS

SITE CONDITIONS FOR REMOVAL:

REMOVE WHEN VEHICLES AND EQUIPMENT WILL NO LONGER ACCESS UNPAVED AREAS

WASHDOWN:
INSTALLATION/CONSTRUCTION PROCEDURES:

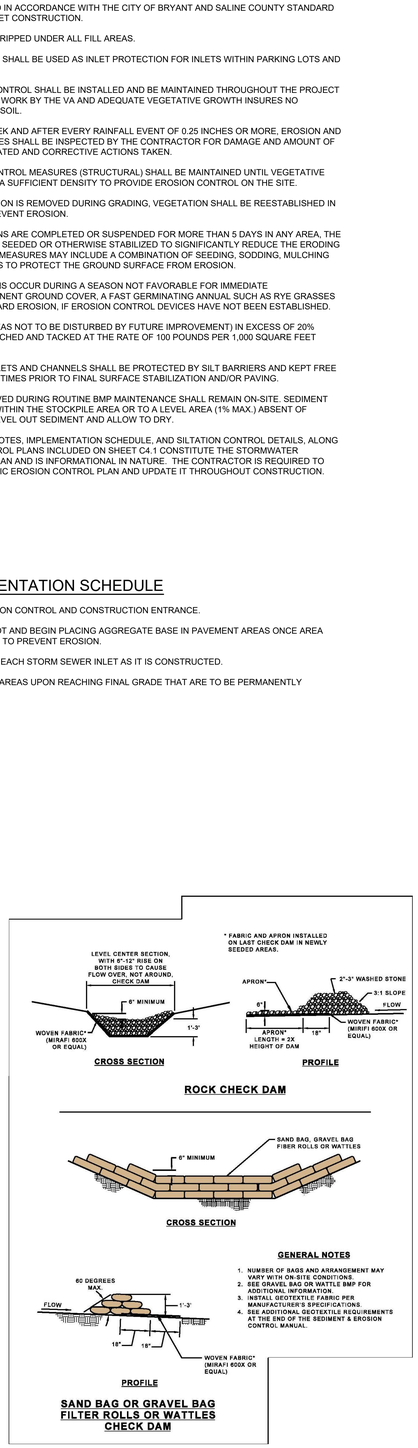
1. GRADE AND COMPACT AREA FOR DRAINAGE UNDER WASHDOWN PAD
2. INSTALL STEEL-RIBBED PLATE ON FRAME OR OTHER SUPPORT TO ALLOW A 2" DRAIN SPACE
3. GRADE AND VEGETATE DOWNSTREAM BMP (V-DITCH SHOWN ON DETAIL)
4. INSTALL WATER SUPPLY AND HOSE
5. POST SIGN IN ADVANCE OF STATION INDICATING THAT ALL EXITING VEHICLES AND EQUIPMENT MUST USE STATION PRIOR TO EXITING SITE

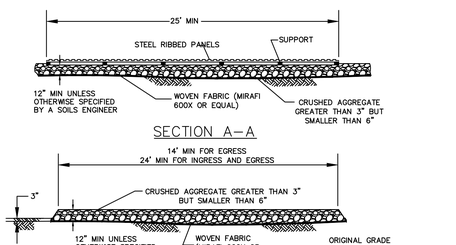
OPERATIONS & MAINTENANCE PROCEDURES:

1. REMOVE SEDIMENT DAILY
2. REPAIR SETTLED AREAS
3. REPLACE ROCK IF NECESSARY TO MAINTAIN CLEAN SURFACE

SITE CONDITIONS FOR REMOVAL:

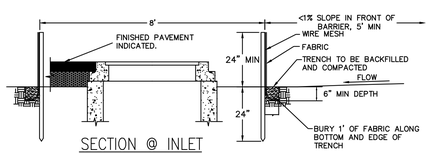
REMOVE WHEN VEHICLES AND EQUIPMENT WILL NO LONGER ACCESS UNPAVED AREAS.




## WASHDOWN

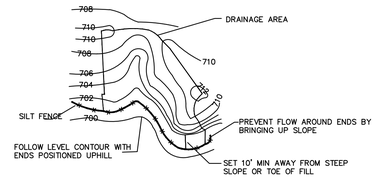
N.T.S.
(SEE SHEET C4.0 FOR LOCATION)



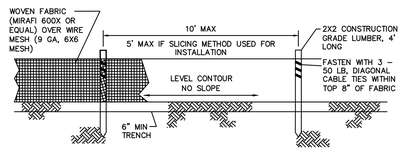

NOTE:
FIBER ROLLS OR WATTLES MAY BE USED AT INLETS IN LIEU OF SILT FENCE AS CONTRACTORS OPTION.

## INLET PROTECTION

N.T.S.
(SEE SHEET C4.0 FOR LOCATIONS)

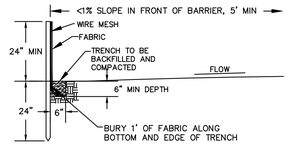



PLAN VIEW




ELEVATION

JOINING SECTIONS OF SILT FENCE




SECTION

NOTE: IF FABRIC IS INSTALLED BY EQUIPMENT DESIGNED TO SLICE INTO THE GROUND, THE TRENCH IS NOT NEEDED

## SILT FENCE

N.T.S.
(SEE SHEET C4.0 FOR LOCATION)

SILT FENCE:
INSTALLATION/CONSTRUCTION PROCEDURES:

1. DRIVE POST FOR FENCE LINE.
2. DIG TRENCH TO REQUIRED DIMENSIONS IN FRONT OF POSTS FOR FABRIC BURIAL.
3. ATTACH WIRE MESH TO POSTS.
4. ATTACH FABRIC TO POSTS, ALLOWING REQUIRED LENGTH BELOW GROUND LEVEL TO RUN FABRIC ALONG BOTTOM OF TRENCH.
5. BACKFILL AND COMPACT SOIL IN TRENCH TO PROTECT AND ANCHOR FABRIC.

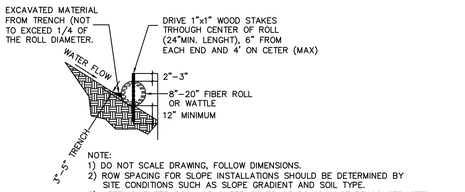
ALTERNATE CONSTRUCTION - INSTALL FENCE BY SLICING IT INTO GROUND WITH SPECIALIZED EQUIPMENT.
INSTALL POSTS AT REDUCED SPACING INDICATED ON DETAIL.

O&M PROCEDURES:

1. INSPECT ONCE A WEEK AND AFTER EVERY STORM.
2. REMOVE SEDIMENT BUILDUP DEEPER THAN 1/2 THE FENCE HEIGHT OR 12" DEPTH, WHICHEVER IS LESS.
3. REPLACE TORN OR CLOGGED FABRIC. REPAIR LOOSE FABRIC.
4. REPAIR UNSTABLE OR BROKEN POSTS.
5. STABILIZE ANY AREAS SUSCEPTIBLE TO UNDERMINING.
6. EXTEND FENCE OR ADD ADDITIONAL ROW(S) FENCE IF NECESSARY TO PROVIDE ADEQUATE PROTECTION.
7. SILT THAT HAS MIGRATED PAST SILT FENCE INTO UNWANTED AREAS OF THE FACILITY OR OFFSITE THROUGH TORN OR LOOSE FABRIC SHALL BE REMOVED AND THE AFFECTED AREAS SHALL BE RESTORED IMMEDIATELY AT THE COST OF THE CONTRACTOR.

SITE CONDITIONS FOR REMOVAL:

AFTER PERMANENT VEGETATION OF SLOPE IS ESTABLISHED. REMOVE FENCE, REGRADE TRENCH AREA AND VEGETATE.




NOTE:
1) DO NOT SCALE DRAWING, FOLLOW DIMENSIONS.
2) ROW SPACING FOR SLOPE INSTALLATIONS SHOULD BE DETERMINED BY SITE CONDITIONS SUCH AS SLOPE GRADIENT AND SOIL TYPE.
3) NETTING, FILTER SOCK OR OUTER COVER OF ROLLS MUST BE CONSTRUCTED OF PHOTODEGRADABLE OR BIODEGRADABLE MATERIAL.
4) FIBER ROLLS AND WATTLES SHALL CONTAIN STRAW, FLAX, COCONUT FIBER (COIR), RICE STRAW OR ASPEN EXCELSIOR, IN A TIGHT TUBULAR ROLL, SPECIFICALLY DESIGNED FOR REMOVAL OF SOLIDS FROM STORM WATER RUNOFF. FILL MATERIAL MUST BE BIODEGRADABLE AND CONTAIN NO CHEMICAL ADDITIVES.
6) FIBER ROLLS OR WATTLES MAY BE WEIGHTED FOR USE AROUND STREET INLETS (INTERNAL ROLL WEIGHT OR PLACING A WEIGHT, SUCH AS A CONCRETE BLOCK, ON THE DOWNSTREAM SIDE OF THE ROLL.
7) FOLLOW THE ROLL MANUFACTURERS INSTRUCTIONS AND RECOMMENDATIONS FOR THE SIZING, INSTALLATION AND MAINTENANCE OF ALL FIBER ROLLS OR WATTLES.

## FIBER ROLLS AND WATTLES

(SEE SHEET C4.0 FOR LOCATION)


PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9101
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS REGISTERED PROFESSIONAL ENGINEER GEORGE M. STOCK No. 9116 06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

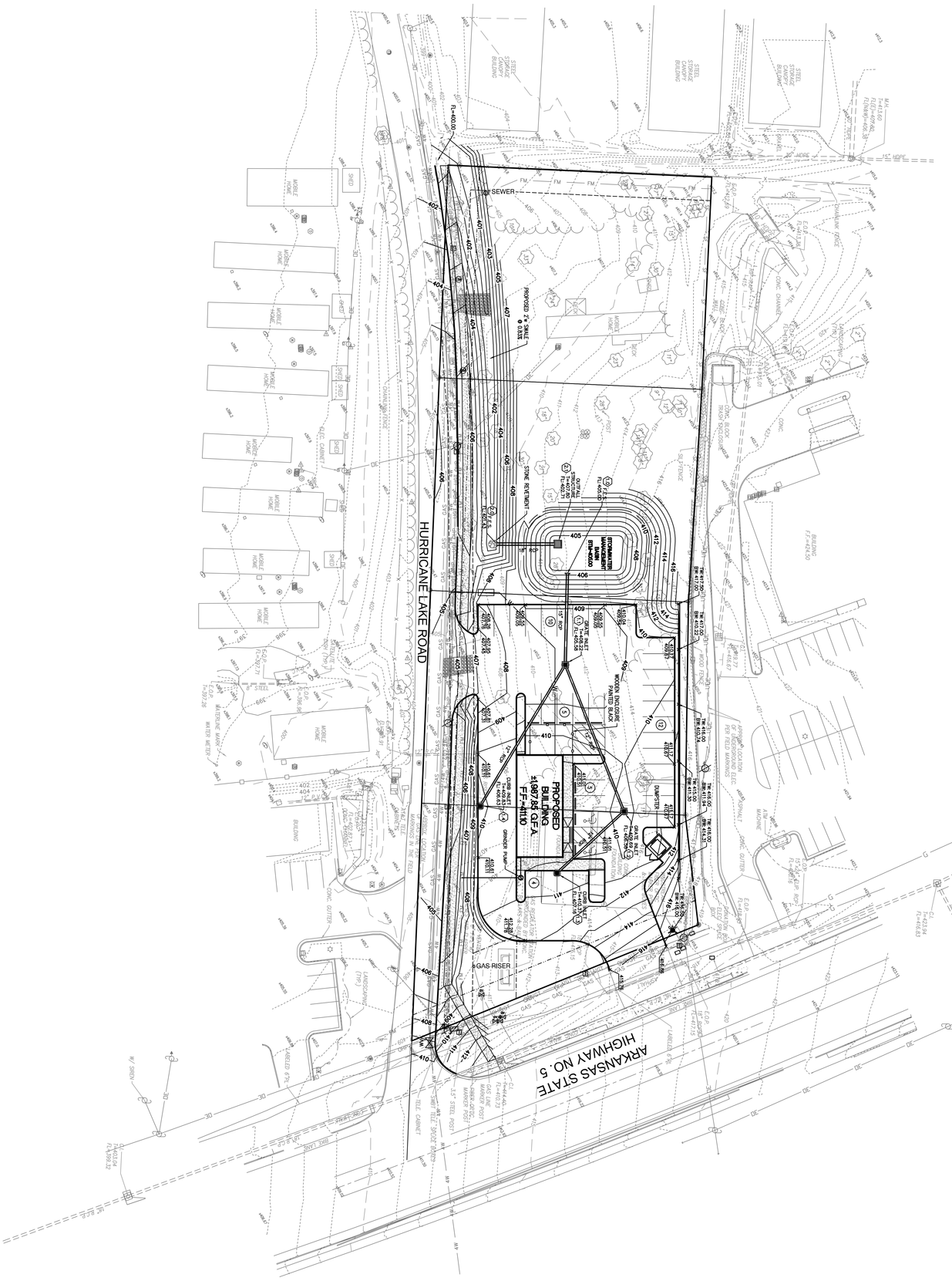
| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
STORMWATER POLLUTION PROTECTION PLAN DETAILS

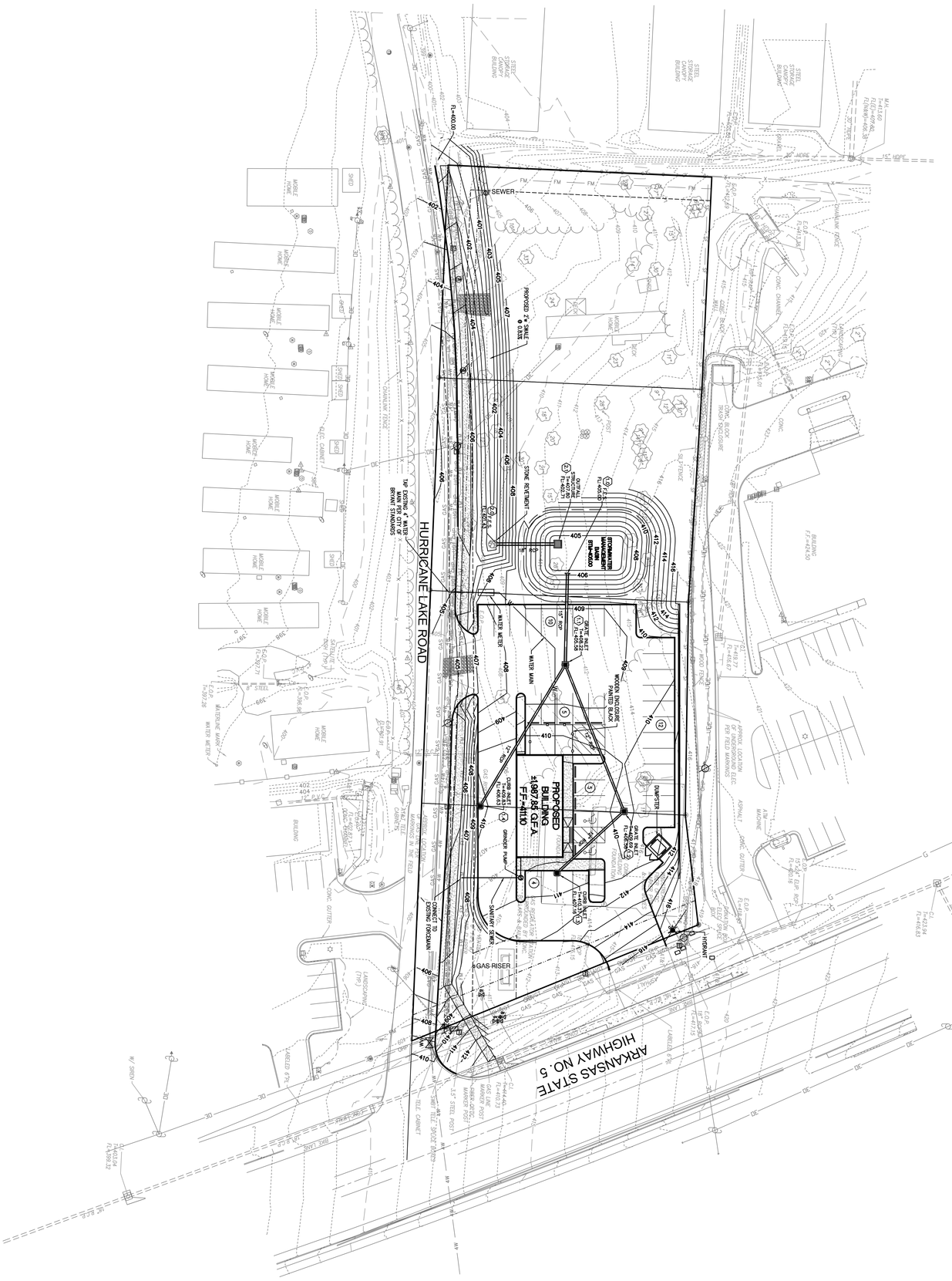
SHEET NO.:
4.1


Updated: 6/2/25 G:\STOCK\PROJECTS\Civil\Planset\PTP\Title Sheet.dwg LAYOUT: C4.1 SWPPP Details PLOTTED: Jun 25, 2025 - 3:56pm PLOTTED BY: Lucas Weber

DRAWING FILE: O:\DRAWITT\2025\2577\SCH\Preliminary\7775-Base.dwg LAYOUT: C5.0-Site Grading Plan PLOTTED: Jun 25, 2025 - 5:06pm PLOTTED BY: lucas.wilcut


HURRICANE LAKE ROAD
ARKANSAS STATE HIGHWAY NO. 5
PROPOSED BUILDING
±1,987.86 GFA
FF=411.10
PROPOSED 4" SWALE @ 0.83%
PROPOSED STRUCTURE
FF=411.10
FL=400.00
PROPOSED STRUCTURE
FL=400.00
STONE RIVETMENT
GAS RISER
SEWER
WOODEN ENCLOSURE PAINTED BLACK
GRINDER PUMP
DUMPSTER
CONC. BLOCK RETAINING WALL
CHAINLINK FENCE
BARBED WIRE FENCE
OVERHEAD ELEC. LINES
STEEL STORAGE CANOPY BUILDING
MOBILE HOME
SHED
CONC. CHANNEL
CONC. GUTTER
ASPHALT DRIVE
GRAVEL DRIVE
GRASS
TREE LINE
WATER LINE
GAS LINE
FIRE LINE
SANITARY SEWER LINE
STORM SEWER LINE
OVERHEAD UTILITY LINE
FENCE LINE
PROPERTY LINE
RIGHT-OF-WAY LINE
CENTERLINE
BUILDING SETBACK LINE
EASEMENT LINE
CURB INLET
GRATE INLET
DROP INLET
FLARE END SECTION
CLEANOUT
MANHOLE
FIRE HYDRANT
WATER METER
GAS VALVE
GAS MARKER POST
TELEPHONE PEDESTAL
TELEPHONE MANHOLE
ELECTRIC CABINET
ELECTRIC MANHOLE
ELECTRIC METER
ELECTRIC TRANSFORMER
UTILITY POLE
LIGHT POLE
GUY WIRE
SIGN
MAILBOX
FLAG POLE
TREE
BUSH
BENCH MARK
SET 1/2" REBAR
FOUND 1/2" REBAR
FOUND 1" PIPE
SET 1/2" REBAR W/ CAP
SET 1/2" REBAR W/ CAP "STOCK & ASSOC."
SET 1/2" REBAR W/ CAP "STOCK & ASSOC. CE 0013"
SET 1/2" REBAR W/ CAP "STOCK & ASSOC. LS 0013"
SET 1/2" REBAR W/ CAP "STOCK & ASSOC. CE 0013 

DRAWING FILE: O:\DRAWITT\2025\2577\SCH\Preliminary\7775-Base.dwg LAYOUT: C6.0-Utility Plan PLOTTED: Jun 25, 2025 - 5:12pm PLOTTED BY: lucas.wilcut

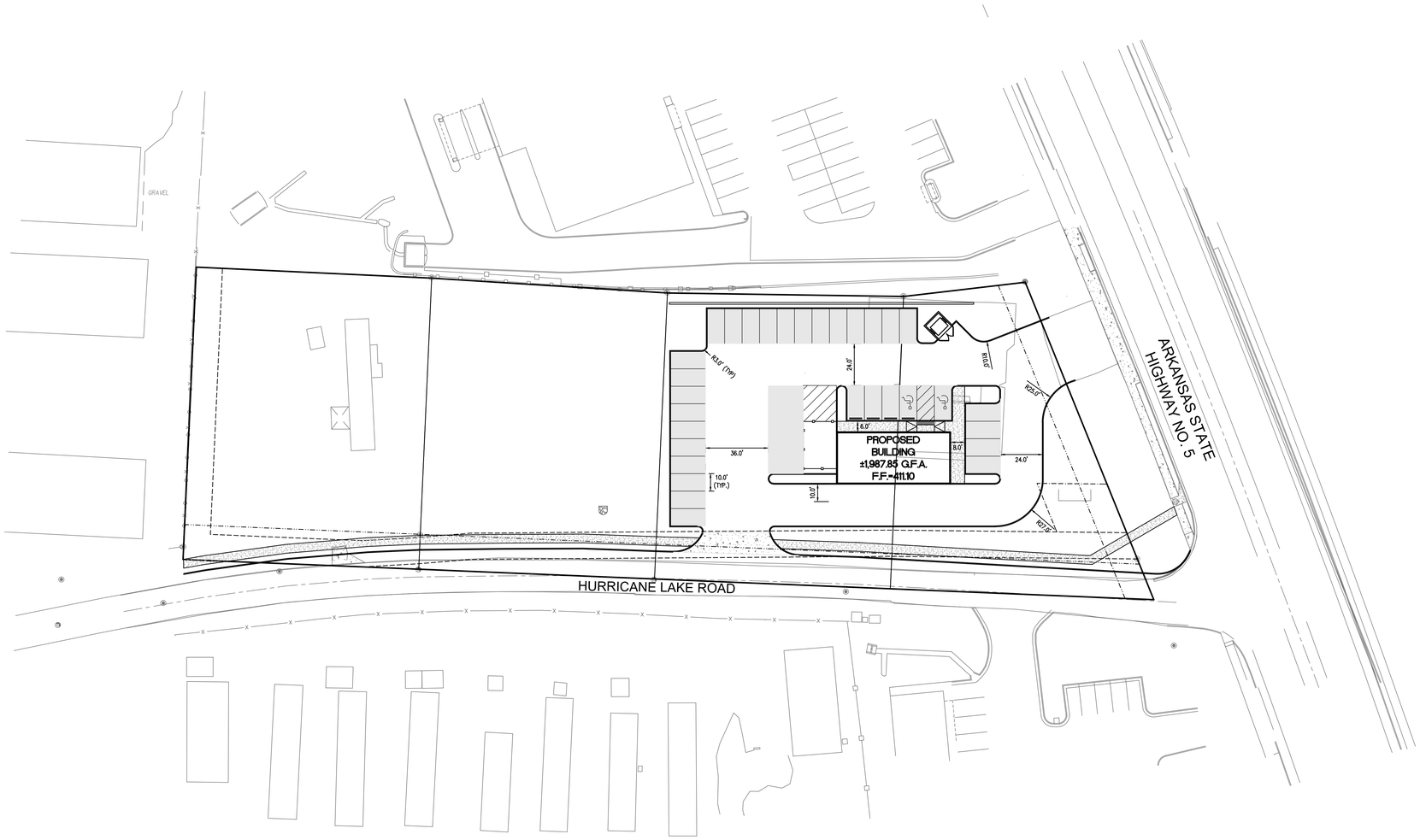

HURRICANE LAKE ROAD
ARKANSAS STATE HIGHWAY NO. 5
PROPOSED BUILDING ±1,987.85 GFA FF=411.0
PROPOSED 4" SWALE @ 0.33%
SEWER
WATER MAIN
WATER METER
GAS RISER
SANITARY SEWER
CONNECT TO EXISTING FORCEMAIN
GRINDER PUMP
DUMPSTER
WOODEN ENCLOSURE PAINTED BLACK
STONE RIVETMENT
EXISTING STRUCTURE TO BE REMOVED FL=400.71
EXISTING BARN TO BE REMOVED FL=400.00
FF=400.00
TAP EXISTING 8" MAIN PER CITY OF BRYANT STANDARDS
STEEL STORAGE CANOPY BUILDING
STEEL STORAGE CANOPY BUILDING
STEEL STORAGE CANOPY BUILDING
M.H. FL=411.69
M.H. FL=411.69
M.H. FL=411.69

## SHEET NOTES

1. ALL PROPOSED WORK WITHIN ENSIGN DRIVE RIGHT OF WAY SHALL BE IN ACCORDANCE WITH KANSAS CITY STANDARDS & SPECIFICATIONS, UNLESS OTHERWISE NOTED.
2. ALL DIMENSIONS SHOWN HEREON ARE FROM FACE OF CURB, UNLESS OTHERWISE NOTED.
3. CONTRACTOR SHALL CONSTRUCT A FULL DEPTH SAW CUT AND PROVIDE A SMOOTH TRANSITION WHERE EXISTING PAVEMENT MEETS NEW PAVEMENT. SAW CUT SHALL BE TO NEAREST JOINT. SAWCUT MUST BE MADE PRIOR TO EXCAVATION. BASE ROCK MUST BE MECHANICALLY COMPACTED. PAVEMENT MUST BE REPLACED IN LIKE AND KIND.
4. IT IS THE CONTRACTORS RESPONSIBILITY TO HIRE A THIRD PARTY TESTING AGENCY FOR THE PLACEMENT AND SUBGRADE TESTING OF THE PROPOSED PAVEMENT.
5. REFER TO SHEET C10.0 FOR PAVEMENT SECTIONS, JOINT AND SIDEWALK DETAILS.

## PAVEMENT LEGEND

- LIGHT DUTY ASPHALT – PARKING AREAS
- HEAVY DUTY ASPHALT – DRIVE AISLES
- HEAVY DUTY CONCRETE – ENTRANCE
- CONCRETE SIDEWALK PAVING




GRAPHIC SCALE

30 0 15 30 60 120

( IN FEET )
1 inch = 30 ft.


PREPARED BY:
STOCK & ASSOCIATES
Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS
GEORGE M. STOCK
REGISTERED PROFESSIONAL ENGINEER
E-25116
06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

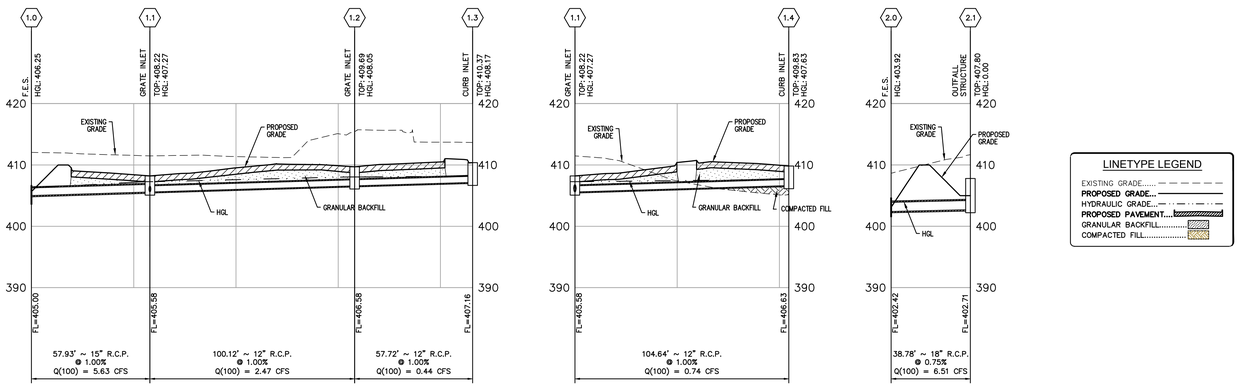
REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
GEOMETRIC PLAN

SHEET NO.:
C7.0


Autodesk Docs://GOOD DAY FARM - BRYANT/GOOD DAY FARM - BRYANT Site.rvt 5/27/2025 7:21:43 AM Plot By: LARRY STEVENS










LINETYPE LEGEND

EXISTING GRADE.....
PROPOSED GRADE...
HYDRAULIC GRADE...
PROPOSED PAVEMENT....
GRANULAR BACKFILL.....
COMPACTED FILL.....

## STORM SEWER PROFILES

HORIZONTAL SCALE: 1"=30'
VERTICAL SCALE: 1"=10'

| Project name: | *GDF - BRYANT* | Calculated By: | *L.C.W.* | 100-year Pipe Hydraulics |
|---|---|---|---|---|
| Project number: | *2024-7775* | Checked By: | *G.M.S.* | *Bend Coefficients :* |
| Project Location: | *BRYANT, AR* | Date: | *5/21/2025* | $5^{\circ}$ = 0.06 $20^{\circ}$ = 0.24 $35^{\circ}$ = 0.4 $50^{\circ}$ = 0.50 $65^{\circ}$ = 0.57 $80^{\circ}$ = 0.65 |
| | | | | $10^{\circ}$ = 0.11 $25^{\circ}$ = 0.30 $40^{\circ}$ = 0.43 $55^{\circ}$ = 0.52 $70^{\circ}$ = 0.60 $85^{\circ}$ = 0.67 |
| | | | | $15^{\circ}$ = 0.18 $30^{\circ}$ = 0.35 $45^{\circ}$ = 0.47 $60^{\circ}$ = 0.55 $75^{\circ}$ = 0.62 $90^{\circ}$ = 0.70 |

Revisions:

| | LINE | | FLOW LINE ELEVATIONS | | | | | | | | | | | | | HEAD LOSS | | | | Hydraulic Elevations | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Structure Number | Upper structure | Lower structure | Upper structure | Lower structure | Length (ft) | Flowline Grade ft/ft | Pipe Size (in.) | Full Flow Cap. (cfs) | Total (Q) (cfs) | Mean Full Flow Vel.(V) (ft/s) | Bend Coef. | Curve Coef. | Velocity Head (Vh) (ft) | QVs ($ft^3/s$) | Pipe Coef. (n) | Hj (ft) | Junction (ft) | Bend (ft) | Curve (ft) | Total $H_{HT}$ | Upper F.L + Dia. | Lower H.E. +Hr | Lower H.E | Structure Upper H.E. + $H_{HT}$ | Top/Sill Structure Elevation | Free Board | Structure Number | Remarks | Velocity Mannings Formula (ft/s) |
| 2.1 | 2.1 | 2.0 | 402.71 | 402.42 | 38.78 | 0.0075 | 18 | 9.12 | 6.51 | 3.68 | 0.00 | 0.00 | 0.21 | 1.37 | 0.013 | 0.15 | 0.00 | 0.00 | 0.00 | 0.00 | 404.21 | 404.07 | 403.92 | 404.21 | 408.00 | 3.79 | 2.1 | Outfall Structure | 5.16 |
| 2.0 | 2.0 | | 402.42 | | | | | | | | | | | | | | | | | | Top of Pipe = | | | 403.92 | | | 2.0 | FES | |
| 1.4 | 1.4 | 1.1 | 406.63 | 405.58 | 34.64 | 0.0100 | 12 | 3.57 | 0.74 | 0.94 | 0.00 | 0.00 | 0.01 | 0.01 | 0.013 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 407.63 | 407.29 | 407.27 | 407.63 | 409.83 | 2.20 | 1.4 | Curb Inlet | 4.55 |
| 1.1 | 1.1 | | 405.58 | | | | | | | | | | | | | | | | | | From Below = | | | 407.27 | | | 1.1 | Grate Inlet | |
| 1.3 | 1.3 | 1.2 | 407.16 | 406.58 | 57.72 | 0.0100 | 12 | 3.57 | 0.44 | 0.56 | 0.00 | 0.00 | 0.00 | 0.00 | 0.013 | 0.01 | 0.01 | 0.00 | 0.00 | 0.01 | 408.16 | 408.06 | 408.05 | 408.17 | 410.37 | 2.20 | 1.3 | Curb Inlet | 4.55 |
| 1.2 | 1.2 | 1.1 | 406.58 | 405.58 | 100.12 | 0.0100 | 12 | 3.57 | 2.47 | 3.14 | 0.60 | 0.00 | 0.15 | 0.38 | 0.013 | 0.48 | 0.20 | 0.09 | 0.00 | 0.30 | 407.58 | 407.75 | 407.27 | 408.05 | 409.69 | 1.64 | 1.2 | Grate Inlet | 4.55 |
| 1.1 | 1.1 | 1.0 | 405.58 | 405.00 | 57.93 | 0.0100 | 15 | 6.48 | 5.63 | 4.59 | 0.30 | 0.00 | 0.33 | 1.84 | 0.013 | 0.44 | 0.35 | 0.10 | 0.00 | 0.44 | 406.83 | 406.69 | 406.25 | 407.27 | 408.22 | 0.95 | 1.1 | Grate Inlet | 5.28 |
| 1.0 | 1.0 | | 405.00 | | | | | | | | | | | | | | | | | | Top of Pipe = | | | 406.25 | | | 1.0 | FES | |

| | | | |
|---|---|---|---|
| | MEAN FULL FLOW VELOCITY: | $V = Q_{ACT}/A_{PIPE}$ | JUNCTION LOSSES (JUNC.) = [ $Q_{out}Vh_{out}$ - Sum ($Q_{in}V_{in}$)]x1.33/[$Q_{out}$] |
| | FRICTION LOSS ($H_f$) : | $Hf = 2.87\ n^2\ (LV^2/d^{1.33})$ | BEND LOSES (BEND) = ($V^2$) * ANGLE COEFFICIENT |
| | VELOCITY HEAD : | $V_h = V^2/2g$ | CURVE LOSS=$V_h$*CURVE COEFFICIENT |
| Note(s): | | | |

**Note:**
1. IF MORE THAN ONE INCOMING LINE, CALC. EACH BEND LOSS AND ADD TOGETHER.
2. NO STRUCTURE LOSES TO BE CALCULATED AT A DROP
3. IF $QV_{h(in)} > QV_{h(out)}$, NO JUNCTION LOSES TO BE CALCULATED.

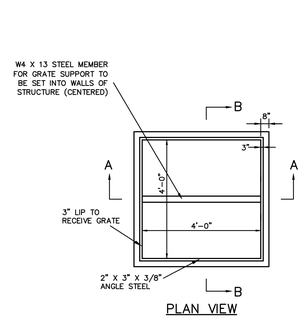
## 100-YEAR PIPE HYDRAULICS

OUTFALL STRUCTURE NOTES:
1) CONTROL STRUCTURE TO BE REINFORCED CONCRETE: WALL THICKNESS IS 8" w/ TWO (2) ROWS OF #4 STEEL.

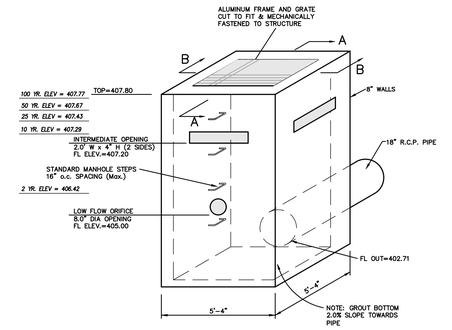
2) OUTFALL STRUCTURE SHALL BE PRE-CAST OR CAST-IN-PLACE.

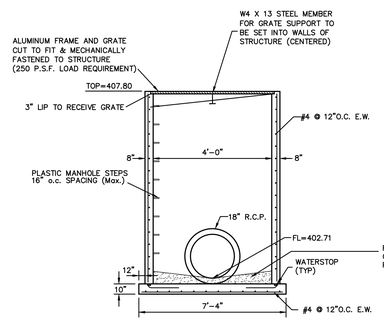
3) CONTRACTOR SHALL PROVIDE A HIGH LEVEL OF CARE WHEN PLACING & COMPACTING "CLAY" SOILS AROUND OUTFALL STRUCTURE & PIPING. THE GEOTECHNICAL ENGINEER SHALL BE PRESENT TO CONFIRM THE "LEVEL OF PLACEMENT"

4) ENGINEER APPROVED SHOP DRAWINGS MUST BE SUBMITTED TO MSD FOR REVIEW PRIOR TO THE CONSTRUCTION OF THIS STRUCTURE. MSD CONTACT: BRIAN DUNN (314) 768-6387.

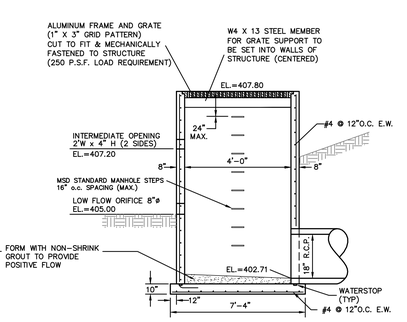



PLAN VIEW




SECTION B-B




SECTION A-A

## OUTFALL STRUCTURE #2.1

(N.T.S.)

UTILITY CONFLICT NOTE:
CONTRACTOR SHALL NOTIFY THIS ENGINEER IMMEDIATELY OF ANY POTENTIAL UNDERGROUND UTILITY CONFLICT AT TIME OF EXCAVATION.

ALL DETAILS SHOWN ON THESE PLANS ARE FOR THE CONVENIENCE OF THE CONTRACTOR. THE DETAILS ARE TO BE VERIFIED PER BRYANT'S STANDARD CONSTRUCTION SPECIFICATIONS ALL METHODS, MEANS AND MATERIALS SHALL CONFORM TO BRYANT'S CURRENT STANDARD CONSTRUCTION SPECIFICATIONS.


PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH. (636) 530-9100 FAX (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS REGISTERED PROFESSIONAL ENGINEER G. M. STOCK No. 25116

06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
|---|---|
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
SEWER PROFILES

SHEET NO.:
8.0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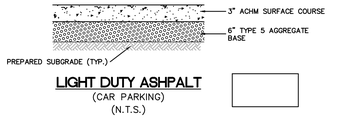
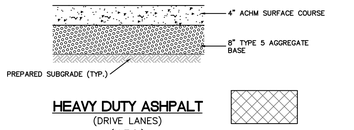
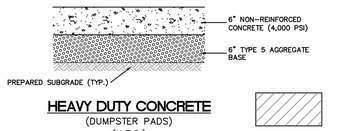



## LIGHT DUTY ASHPALT
(CAR PARKING)
(N.T.S.)




## HEAVY DUTY ASHPALT
(DRIVE LANES)
(N.T.S.)

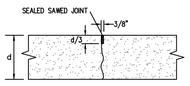



## HEAVY DUTY CONCRETE
(DUMPSTER PADS)
(N.T.S.)

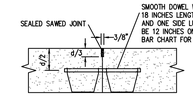
**PAVEMENT DETAILS ARE SUBJECT TO GEOTECHNICAL ENGINEER, OWNER AND CONTRACTOR VERIFICATION AND APPROVAL PRIOR TO CONSTRUCTION**

PAVEMENT NOTES:

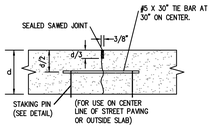
1. ALL MEANS AND METHODS OF CONCRETE AND ASPHALT CONCRETE SHALL BE IN ACCORDANCE WITH THE CITY OF BRYANT STANDARD CONSTRUCTION SPECIFICATIONS AND ACI 330R-01. IT IS THE CONTRACTOR'S RESPONSIBILITY TO OBTAIN CURRENT EDITIONS PRIOR TO CONSTRUCTION.
2. ALL PAVEMENT SECTIONS AND DETAILS ARE SUBJECT TO GEOTECHNICAL ENGINEER AND OWNER REVIEW AND APPROVAL PRIOR TO SUBMISSION OF SHOP DRAWINGS.
3. IT IS THE CONTRACTOR'S RESPONSIBILITY TO APPLY THE RECOMMENDATIONS SUPPLIED IN THE GEOTECHNICAL ENGINEERING REPORT.
4. ALL EXPOSED CONCRETE EDGES TO BE CHAMFERED.
5. ALL CONCRETE SHALL BE 4,000 PSI, 28-DAY STRENGTH, AIR ENTRAINMENT IN THE RANGE OF 6% TO 8% MAXIMUM SLUMP OF 4 INCH +/- 1 INCH IS ACCEPTABLE.
6. PAVEMENT SECTIONS WITHIN THE PUBLIC RIGHT-OF-WAY TO BE REVIEWED AND APPROVED BY THE CITY OF KANSAS CITY.
7. IT IS THE CONTRACTORS RESPONSIBILITY TO HIRE A THIRD PARTY TESTING AGENCY FOR THE PLACEMENT AND SUBGRADE TESTING OF THE PROPOSED PAVEMENT.



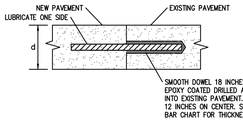

SAWED CONTROL JOINT



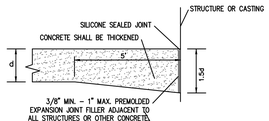

TRANSVERSE CONSTRUCTION JOINT



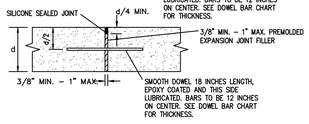

LONGITUDINAL JOINT



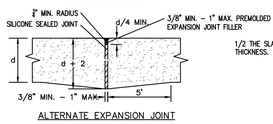

TRANSITION BETWEEN NEW & EXISTING PAVEMENT




ISOLATION JOINT



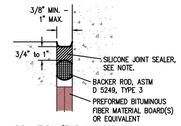

EXPANSION JOINT



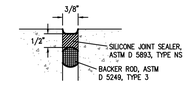

ALTERNATE EXPANSION JOINT

| DOWEL BARS – EPOXY COATED | | |
|---|---|---|
| PAVEMENT THICKNESS | BAR SIZE DIAMETER | LENGTH |
| 7 INCHES | 1 INCH | 18 INCHES |
| 8 INCHES | 1 INCH | 18 INCHES |
| 9 INCHES | 1–1/4 INCHES | 18 INCHES |
| 10 INCHES | 1–1/4 INCHES | 18 INCHES |
| 11 INCHES or < | 1–1/2 INCHES | 18 INCHES |

## JOINT DETAILS
(N.T.S.)




ISOLATION/EXPANSION JOINT DETAIL

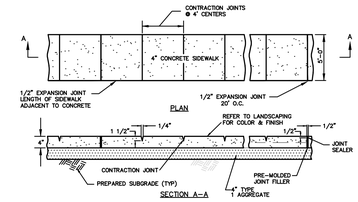



CONSTRUCTION, CONTROL AND LONGITUDINAL JOINT DETAIL

STAKING PIN

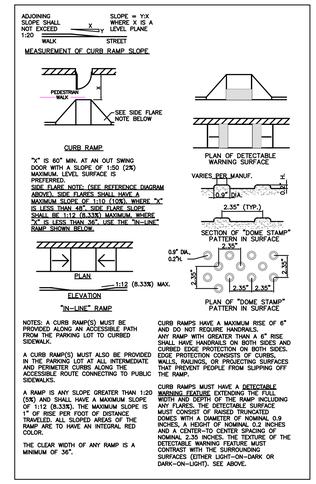
## JOINT NOTES

1. CONSTRUCTION JOINTS ARE REQUIRED BETWEEN ALL POURS SEPARATED BY MORE THAN 90 MINUTES TIME.
2. FIFTEEN FOOT (15) MAXIMUM SPACING BETWEEN CONTROL JOINTS. PAVING CONTRACTOR SHALL FOLLOW "GUIDE FOR DESIGN AND CONSTRUCTION OF CONCRETE PARKING LOTS" AS REPORTED BY ACI COMMITTEE 330.
3. FILL JOINTS TO WITHIN 1/8" OF SURFACE WITH JOINT SEALER.
4. ISOLATION JOINTS REQUIRED AROUND ALL UTILITY STRUCTURES THAT ARE LOCATED WITHIN THE LIMITS OF CONCRETE PAVEMENT.
5. EXPANSION JOINT MAY BE REQUIRED DEPENDING ON COLD WEATHER, i.e. IF PAVING OCCURS WHEN AMBIENT TEMPERATURES ARE BELOW 40 DEGREES




## SIDEWALK DETAIL
(N.T.S.)
(NOT FOR USE IN WITHIN R/W)

NOTE:
EXPANSION JOINT MATERIAL SHALL BE INSTALLED IN THE WALK FOR ITS FULL WIDTH AND DEPTH AT INTERVALS OF APPROX. 20', CONTROL JOINTS AT INTERVALS OF 5' CENTERS.




NOTES: A CURB RAMP(S) MUST BE PROVIDED ALONG AN ACCESSIBLE PATH FROM THE PARKING LOT TO CURBED SIDEWALK.

A CURB RAMP(S) MUST ALSO BE PROVIDED IN THE PARKING LOT AT ALL INTERMEDIATE AND PERIMETER CURBS ALONG THE ACCESSIBLE ROUTE CONNECTING TO PUBLIC SIDEWALKS.

A RAMP IS ANY SLOPE GREATER THAN 1:20 (5%) AND SHALL HAVE A MAXIMUM SLOPE OF 1:12 (8.33%). THE MAXIMUM SLOPE IS 1" OF RISE PER FOOT OF DISTANCE TRAVELED. ALL SLOPED AREAS OF THE RAMP ARE TO HAVE AN INTEGRAL RED COLOR.

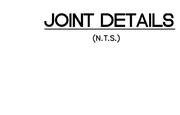
THE CLEAR WIDTH OF ANY RAMP IS A MINIMUM OF 36".

CURB RAMPS HAVE A MAXIMUM RISE OF 6" AND DO NOT REQUIRE HANDRAILS.

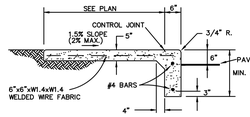
ANY RAMP WITH GREATER THAN A 6" RISE SHALL HAVE HANDRAILS ON BOTH SIDES AND SHALL HAVE CURBS OR WALLS WITH SIDES. EDGE PROTECTION CONSISTS OF CURBS, WALLS, RAILINGS, OR PROJECTING SURFACES THAT PREVENT PEOPLE FROM SLIPPING OFF THE RAMP.

CURB RAMPS MUST HAVE A DETECTABLE WARNING FEATURE EXTENDING THE FULL WIDTH AND DEPTH OF THE RAMP INCLUDING ANY FLARES. THE DETECTABLE WARNING MUST CONSIST OF RAISED TRUNCATED DOMES WITH A DIAMETER OF NOMINAL 0.9 INCHES, A HEIGHT OF NOMINAL 0.2 INCHES AND A CENTER-TO CENTER SPACING OF NOMINAL 2.35 INCHES. THE TEXTURE OF THE DETECTABLE WARNING FEATURE MUST CONTRAST WITH THE SURROUNDING SURFACES (EITHER LIGHT-ON-DARK OR DARK-ON-LIGHT). SEE ABOVE.

## HANDICAP RAMP DETAILS

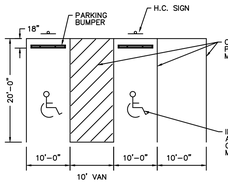



## CONCRETE CURB AND GUTTER DETAIL
(n.t.s.)




NOTE: EXPANSION JOINT MATERIAL SHALL BE INSTALLED IN THE WALK FOR ITS FULL WIDTH AND DEPTH AT INTERVALS OF APPROX. 50', CONTROL JOINTS AT INTERVALS OF 1.5' TIMES ITS WIDTH.

## OPTIONAL INTEGRAL SIDEWALK/CURB DETAIL
(n.t.s.)

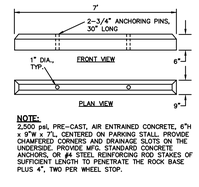



PAVEMENT MARKING PAINT:
1. LATEX, WATERBORNE EMULSION, LEAD AND CHROMATE FREE, READY MIXED, COMPLYING WITH FS TT-P-1952, WITH DRYING TIME OF LESS THAN 3 MINUTES.
2. WHITE FOR TYPICAL PARKING STALLS, BLUE FOR HANDICAP STALLS, VERIFY WITH OWNER.

## PAINTED HANDICAP SYMBOL
(N.T.S.)



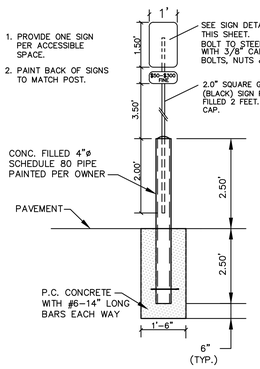

## TYPICAL PARKING STALLS
(N.T.S.)



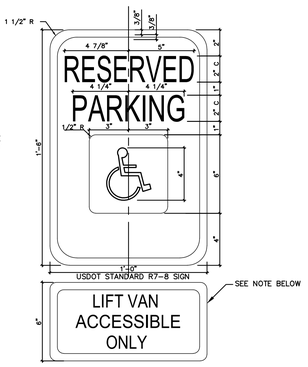

NOTE:
2,500 psi, PRE-CAST, AIR ENTRAINED CONCRETE, 6"H x 9"W x 7'L, CENTERED ON PARKING STALL PROVIDE CHAMFERED CORNERS AND DRAINAGE SLOTS ON THE UNDERSIDE. PROVIDE MFG. STANDARD CONCRETE ANCHORS, OR #4 STEEL REINFORCING ROD STAKES OF SUFFICIENT LENGTH TO PENETRATE THE ROCK BASE PLUS 4", TWO PER WHEEL STOP.

## PRE-CAST PARKING BUMPER
(N.T.S.)

NOTES: 1. PROVIDE ONE SIGN PER ACCESSIBLE SPACE.
2. PAINT BACK OF SIGNS TO MATCH POST.

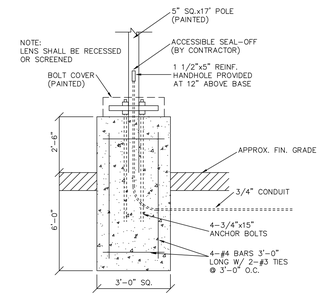



## ACCESSIBLE PARKING SIGN
(N.T.S.)

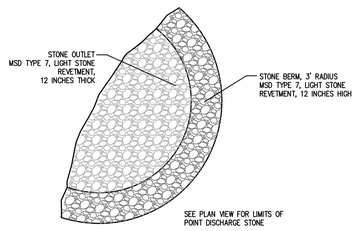



NOTE (R7-8 SIGN): THIS IS A STANDARD SIGN AND MAY BE ORDERED FROM ANY TRAFFIC SIGN SUPPLIER BY NUMBER. THE SIGN MUST BE SUPPLEMENTED WITH A "LIFT VAN ACCESSIBLE ONLY" SIGN AS APPLICABLE AND/OR AMOUNT OF THE FINE FOR ILLEGALLY PARKING IN THE RESERVED SPACE(S) A MUNICIPALITY MAY IMPOSE. CONFIRM WITH LOCAL REGULATIONS.

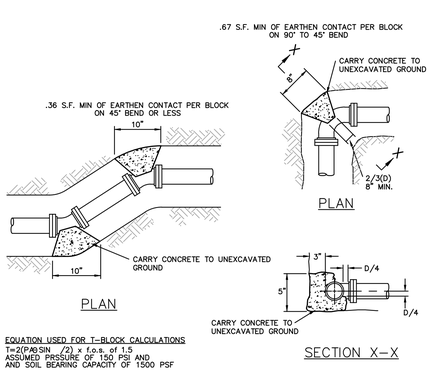
## ACCESSIBLE SIGN DETAIL
(N.T.S.)




## LIGHT POLE BASE
(n.t.s.)




## POINT DISCHARGE STONE
(N.T.S.)



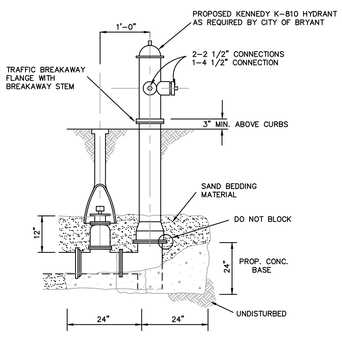

EQUATION USED FOR T-BLOCK CALCULATIONS
T=2(P•S)SIN /2) x f.o.s. of 1.5
ASSUMED PRESSURE OF 150 PSI AND
AND SOIL BEARING CAPACITY OF 1500 PSF

A = CONTACT BEARING AREA OF BLOCK WITH EARTH IN SQUARE FEET

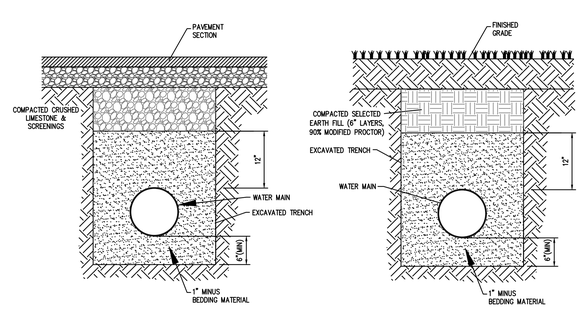
| PIPE DIA. IN. | PLUG | 45° WYE | TEE CONNECTION | UP TO 22.5° | UP TO 45° | UP TO 90° |
|---|---|---|---|---|---|---|
| | A (SQ. FT.) | A (SQ.FT.) | A (SQ.FT.) | A (SQ.FT.) | A (SQ.FT.) | A (SQ.FT.) |
| 4" and smaller | 0.5 | 1.4 | 2.6 | 1.8 | 2.2 | 2.0 |
| 6" | 1.5 | 3.0 | 6.0 | 4.0 | 4.5 | 4.5 |
| 8" | 2.5 | 5.0 | 9.5 | 6.5 | 9.5 | 8.0 |
| 10" | 4.1 | 8.0 | 13.0 | 9.5 | 12.5 | 12.5 |
| 12" | 5.5 | 11.5 | 19.0 | 13.5 | 16.0 | 18.0 |
| 16" | 9.0 | 18.0 | 33.0 | 23.0 | 27.0 | 32.0 |
| 20" | 14.0 | 28.0 | 51.0 | 36.0 | 42.0 | 50.5 |

NOTES:
1. BEARING AREAS ARE BASED ON UNDISTURBED SOIL WITH A BEARING CAPACITY OF 1,000 POUNDS PER SQUARE FOOT. FOR A LESSER SOIL BEARING CAPACITY THESE AREAS SHALL BE INCREASED ACCORDINGLY.
2. ALL CONCRETE THRUST BLOCKS SHALL BE 3000 p.s.i. CONCRETE.
3. THRUST BLOCKS SHALL BE POURED AGAINST UNDISTURBED EARTH.
4. NO JOINT SHALL BE COVERED WITH CONCRETE.
5. JOINTS THAT LOCATED AGAINST THRUST BLOCKS ARE TO BE WRAPPED IN A CLOTH MATERIAL.
6. APPROVED MECHANICAL JOINT RESTRAINTS ARE REQUIRED AT ALL VERTICAL BENDS AND MAY BE USED IN LIEU OF THRUST BLOCKS AT HORIZONTAL BENDS AT THE OPTION OF THE ENGINEER, AT NO ADDITIONAL COST TO THE OWNER.

## THRUST BLOCK DETAIL
(N.T.S.)




## FIRE HYDRANT DETAIL
(n.t.s.)




## WATER SERVICE PIPE BEDDING DETAIL
(N.T.S.)
(NOT FOR USE IN ArDOT R/W)

PREPARED BY:
STOCK & ASSOCIATES
Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9101
e-mail: general@stockassoc.com
Web: www.stockassoc.com

SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS — GEORGE M. STOCK — 25116 — REGISTERED PROFESSIONAL ENGINEER — 06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

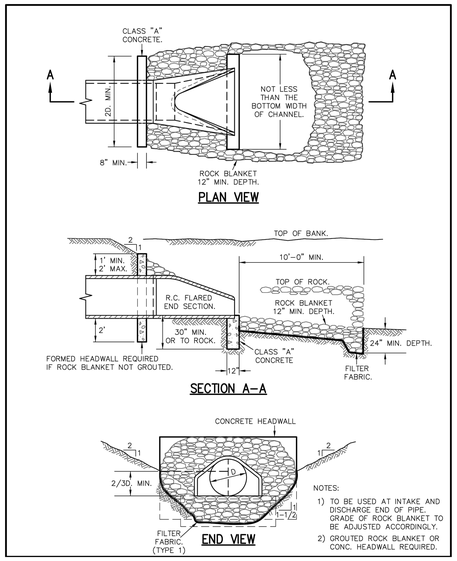
REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

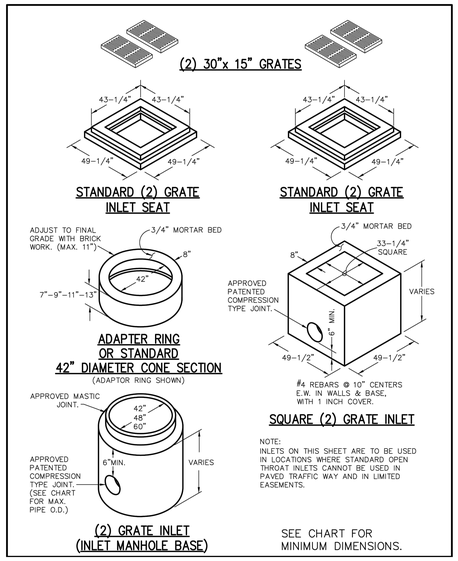
SHEET TITLE:
CONSTRUCTION DETAILS

SHEET NO.:
9.0

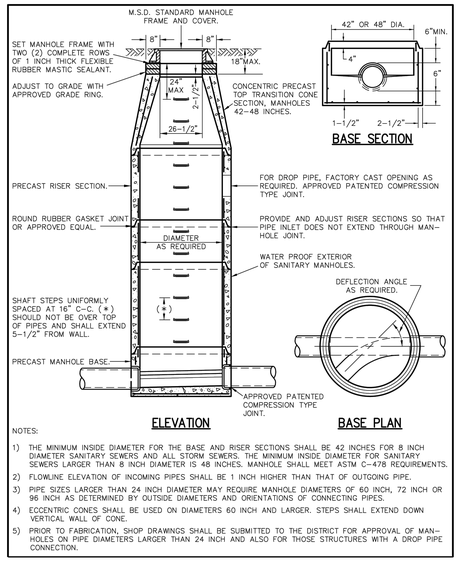
Drawing File: G:\DRAWINGS\2025\7775\Civil\Permanent\7775 Detail.dwg, LAYOUT: ES Cover Sheet, PLOTTED: Jun 25, 2025, 9:51am, PLOTTED BY: Lisa Weber



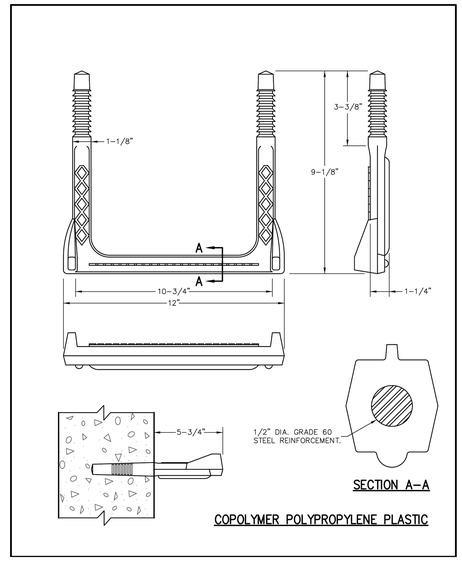

## FLARED END SECTION
(N.T.S.)



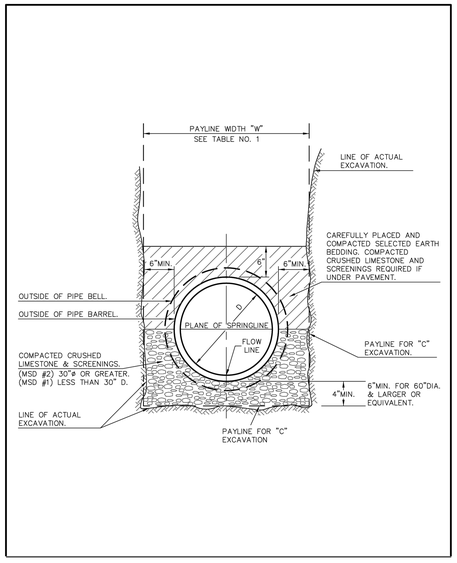

## 2-GRATE INLETS PRECAST CONCRETE
(N.T.S.)



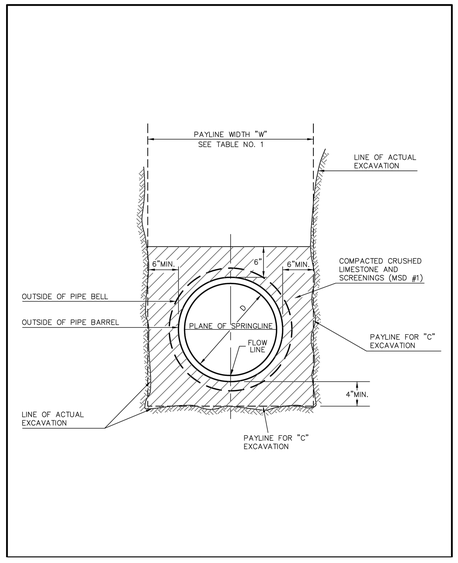

## PRECAST CONCRETE MANHOLE
(N.T.S.)



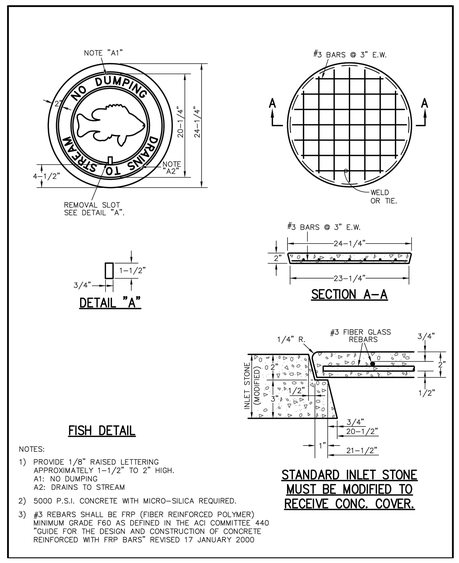

## MANHOLE STEP FOR PRECAST AND CAST-IN-PACE MANHOLE
(N.T.S.)



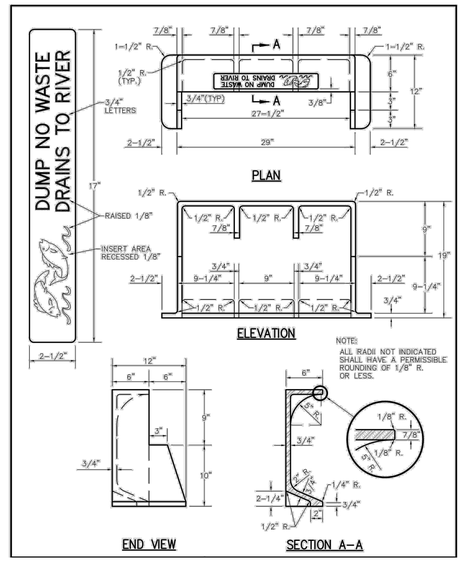

## PIPE BEDDING CLASS "C" (MODIFIED FOR REINFORCED CONCRETE PIPE)
(N.T.S.)




## PIPE BEDDING CLASS "C" (FOR ALL 6" TO 18" PIPE EXCEPT REINFORCED CONCRETE PIPE)
(N.T.S.)




## PRECAST CONCRETE INLET COVER AND STONE
(N.T.S.)




## CAST IRON SIDE INTAKE UNIT FOR GRATED INLETS - 249 LBS
(N.T.S.)

ALL DETAILS SHOWN ON THESE PLANS ARE FOR THE CONVENIENCE OF THE CONTRACTOR. THE DETAILS ARE TO BE VERIFIED PER BRYANT'S STANDARD CONSTRUCTION SPECIFICATIONS. ALL METHODS, MEANS AND MATERIALS SHALL CONFORM TO BRYANT'S CURRENT STANDARD CONSTRUCTION SPECIFICATIONS.

PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH: (636) 530-9100 FAX: (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com

SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS GEORGE M. STOCK 6-25116 REGISTERED PROFESSIONAL ENGINEER
06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
CONSTRUCTION DETAILS

SHEET NO.:
9.1

Drawing File: G:\Stock\7700\2025\7775\Civil\Drawings\7775Base.dwg LAYOUT: C9 Civil Details 7X17FTD Jun 26, 2025 - 3:51pm PLOTTED BY: Lucas Wood

## STORMWATER DIFFERENTIAL RUNOFF

| PRE-DEVELOPED | | | |
|---|---|---|---|
| | ACRES | C*I | TOTAL Q(100) |
| GRASS | 1.26 | 5.10 | 6.40 |
| PVMT/ROOF | 0.15 | 9.50 | 1.40 |
| | | TOTAL Q(100) = | 7.81 |

| POST-DEVELOPED | | | |
|---|---|---|---|
| | ACRES | C*I | TOTAL Q(100) |
| GRASS | 0.61 | 5.10 | 3.09 |
| PVMT/ROOF | 0.80 | 9.50 | 7.58 |
| | | TOTAL Q(100) = | 10.67 |
| | | | |
| | | DIFFERENTIAL = POST - PRE = + | 2.86 |

**TABLE 1**
**Allowable Peak Discharge**
**Pre-Developed Conditions**

| *Design Storm (Year)* | *Pre-Development Runoff (c.f.s.)** | *Volume (ac-ft)* |
|---|---|---|
| 2 | 2.53 | 0.210 |
| 10 | 4.61 | 0.377 |
| 25 | 5.77 | 0.472 |
| 50 | 7.22 | 0.593 |
| 100 | 7.75 | 0.637 |

* = Includes offsite drainage onto subject property

PREPARED BY:
STOCK & ASSOCIATES
Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH. (636) 530-9100 FAX (636) 530-9103
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:

# GOOD DAY FARM - BRYANT

3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

STATE OF ARKANSAS
GEORGE M. STOCK
REGISTERED PROFESSIONAL ENGINEER
No. 5115
06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
EXISTING DRAINAGE AREA MAP

SHEET NO.:
C10.0


DRAWING FILE: S:\PROJECTS\2025\7775\Drawings\7775Site.dwg, LAYOUT: C10.0-EX, DAVE PUTTER, Jun 25, 2025 - 3:56pm, PLOTTED BY: Dave Mead

## GOOD DAY FARM - BRYANT

2024-7775

### STORMWATER RUNOFF CALCULATIONS

Q=CIA
Q=PEAK FLOW, C=RUNOFF COEFF., I=RAINFALL INTENSITY, A=DRAINAGE AREA

100 YEAR 5-MIN
I=10 IN/HR
C (IMPERVIOUS)=0.95*
C (PERVIOUS) = 0.51*
*=FROM TABLE 400-1

**POST-DEVELOPMENT RUNOFF**

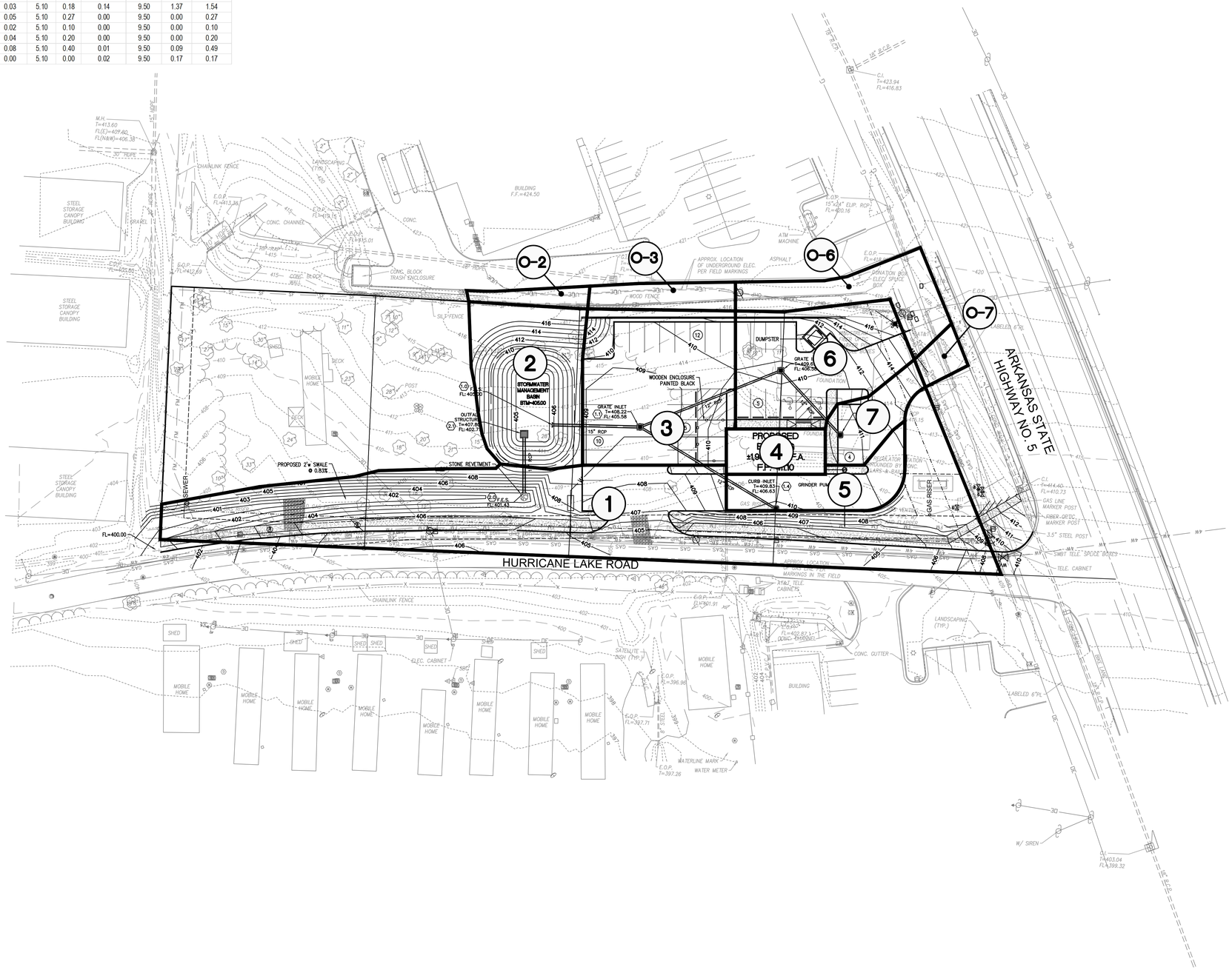
| SUBAREA | AREA ( SQ.FT ) PERVIOUS | AREA ( SQ.FT ) IMPERVIOUS | TOTAL AREA SQ.FT | TOTAL AREA AC | PERVIOUS ACREAGE | C*I (PERV.) | Q (PERV.) | IMPERVIOUS ACREAGE | C*I (IMPRV.) | Q (IMPRV.) | Q (TOTAL) |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1 | 15,088 | 12,945 | 28,033 | 0.64 | 0.35 | 5.10 | 1.77 | 0.30 | 9.50 | 2.82 | 4.59 |
| 2 | 7,501 | 0 | 7,501 | 0.17 | 0.17 | 5.10 | 0.88 | 0.00 | 9.50 | 0.00 | 0.88 |
| 3 | 0 | 10,160 | 10,160 | 0.23 | 0.00 | 5.10 | 0.00 | 0.23 | 9.50 | 2.22 | 2.22 |
| 4 | 0 | 1,960 | 1,960 | 0.04 | 0.00 | 5.10 | 0.00 | 0.04 | 9.50 | 0.43 | 0.43 |
| 5 | 0 | 3,415 | 3,415 | 0.08 | 0.00 | 5.10 | 0.00 | 0.08 | 9.50 | 0.74 | 0.74 |
| 6 | 1,500 | 6,268 | 7,768 | 0.18 | 0.03 | 5.10 | 0.18 | 0.14 | 9.50 | 1.37 | 1.54 |
| 7 | 2,292 | 0 | 2,292 | 0.05 | 0.05 | 5.10 | 0.27 | 0.00 | 9.50 | 0.00 | 0.27 |
| O-2 | 854 | 0 | 854 | 0.02 | 0.02 | 5.10 | 0.10 | 0.00 | 9.50 | 0.00 | 0.10 |
| O-3 | 1,689 | 0 | 1,689 | 0.04 | 0.04 | 5.10 | 0.20 | 0.00 | 9.50 | 0.00 | 0.20 |
| O-6 | 3,424 | 400 | 3,824 | 0.09 | 0.08 | 5.10 | 0.40 | 0.01 | 9.50 | 0.09 | 0.49 |
| O-7 | 0 | 779 | 779 | 0.02 | 0.00 | 5.10 | 0.00 | 0.02 | 9.50 | 0.17 | 0.17 |

**TABLE 2**
**Peak Discharge - Post-Developed Conditions**

| Design Storm (Year) | Allowable Discharge (cfs) | Post-Developed Discharge (cfs) |
|---|---|---|
| 2 | 2.53 | 1.81 |
| 10 | 4.61 | 3.73 |
| 25 | 5.77 | 5.83 |
| 50 | 7.22 | 6.44 |
| 100 | 7.75 | 6.92 |

**Stormwater Detention Summary**

| Design Storm (Year) | Basin Discharge (cfs) | Basin WSEL (feet) | Basin Freeboard (feet) |
|---|---|---|---|
| 2 | 1.81 | 406.46 | 3.54 |
| 10 | 3.73 | 407.31 | 2.69 |
| 25 | 5.83 | 407.44 | 2.56 |
| 50 | 6.44 | 407.72 | 2.28 |
| 100 | 6.92 | 407.82 | 2.18 |




GRAPHIC SCALE

( IN FEET )
1 inch = 30 ft.


PREPARED BY:
STOCK & ASSOCIATES Consulting Engineers, Inc.
257 Chesterfield Business Parkway
St. Louis, MO. 63005 PH. (636) 530-9100 FAX (636) 530-9130
e-mail: general@stockassoc.com
Web: www.stockassoc.com


SITE IMPROVEMENT PLANS FOR:
# GOOD DAY FARM - BRYANT
3205 HIGHWAY 5 N.
BRYANT, ARKANSAS 72019

06/25/25

GEORGE M. STOCK E-25116
CIVIL ENGINEER
CERTIFICATE OF AUTHORITY NUMBER: 000996

REVISIONS:

| | |
|---|---|
| DRAWN BY: L.C.W. | CHECKED BY: G.M.S. |
| DATE: 05-14-2025 | JOB NO: 2025-7775 |
| M.S.D. P #: | BASE MAP #: |
| S.L.C. H&T #: | H&T S.U.P. #: |
| M.D.N.R. #: | |

SHEET TITLE:
PROPOSED DRAINAGE AREA MAP

SHEET NO.:
C10.1


Document is C:\DRAWINGS\2025\7775\Drawings\7775 Base Map 24X36 ESI 5 ft Add PLOTTED Jun 26, 2025 - 3:58pm PLOTTED BY: Laura Arnold

Legal Description – 2224 Brandon Loop, Bryant, AR

All that part of the SW ¼ of the SW ¼ Section 21, Township 1 South, Range 14 West, Saline County, Arkansas, described as follows: Beginning at the SW corner of said Section 21, and run thence East along the South line for 600' to the West line of roadway; run thence N 01°31' E along West line of road for 250'; thence West parallel with the South line for 203' to the Point of Beginning of the land herein described; From said point run thence N 88° 25' 22" W 203.58'; thence N 2°28' 30" E 100' to a point that is 409.2' West of the West line of road; run S 88° 30' 15" E 204.60'; thence S 3°03' 12" W 100.31' to the Point of Beginning. Tract contains 0.47 acres, more or less.

NAME OF DEVELOPMENT: SPRINGHILL TAVERN

CURRENT ZONING: C2

NAME AND ADDRESS OF OWNER: RONALD EDWARDS SR.
NAME AND ADDRESS OF DEVELOPER: RONALD EDWARDS SR.
2205 BRANDON RD.
BRYANT, ARKANSAS 72022

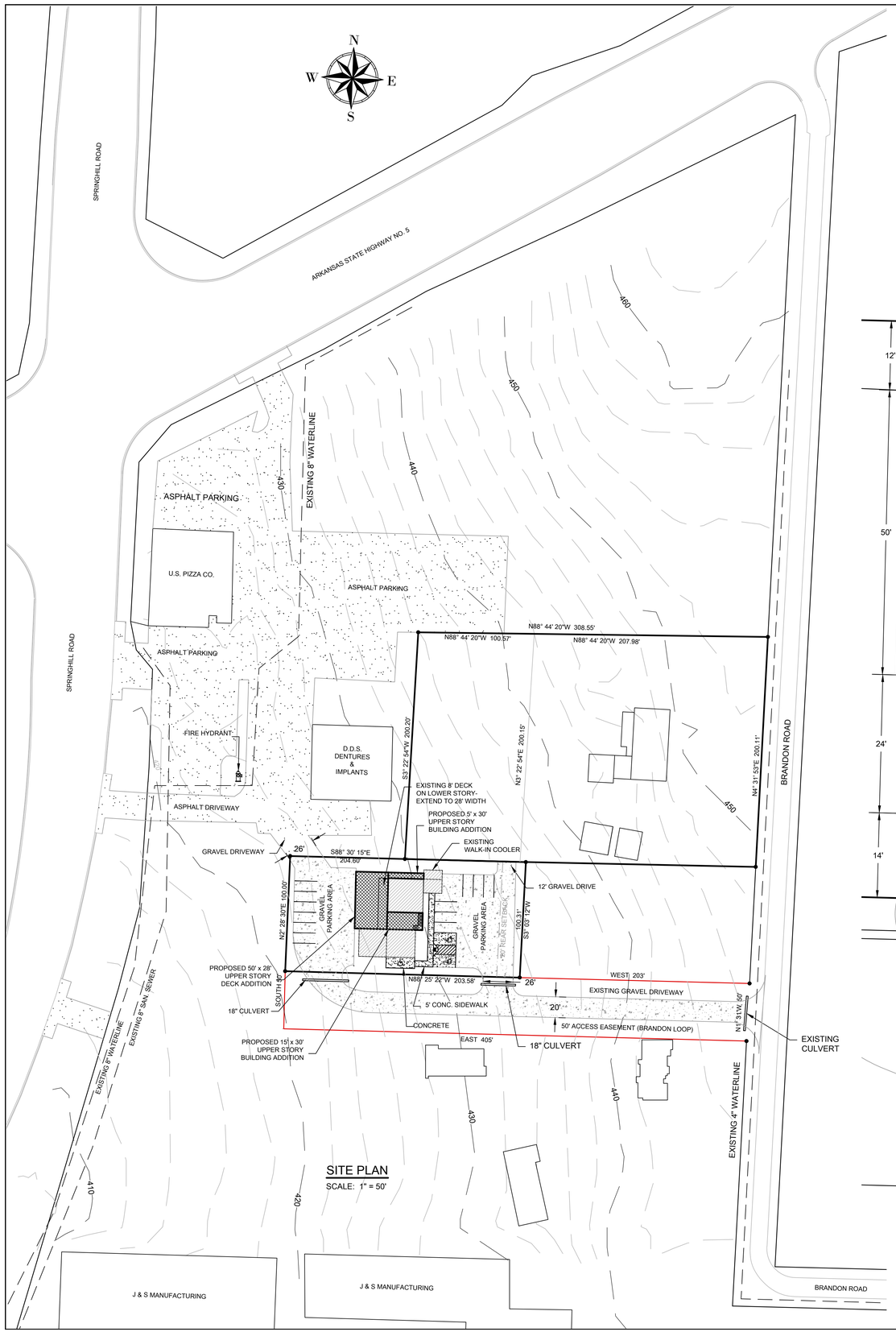
PHYSICAL ADDRESS OF PROJECT: 2224 BRANDON LOOP
BRYANT, ARKANSAS 72022

Legal Description – 2205 Brandon Road, Bryant, AR

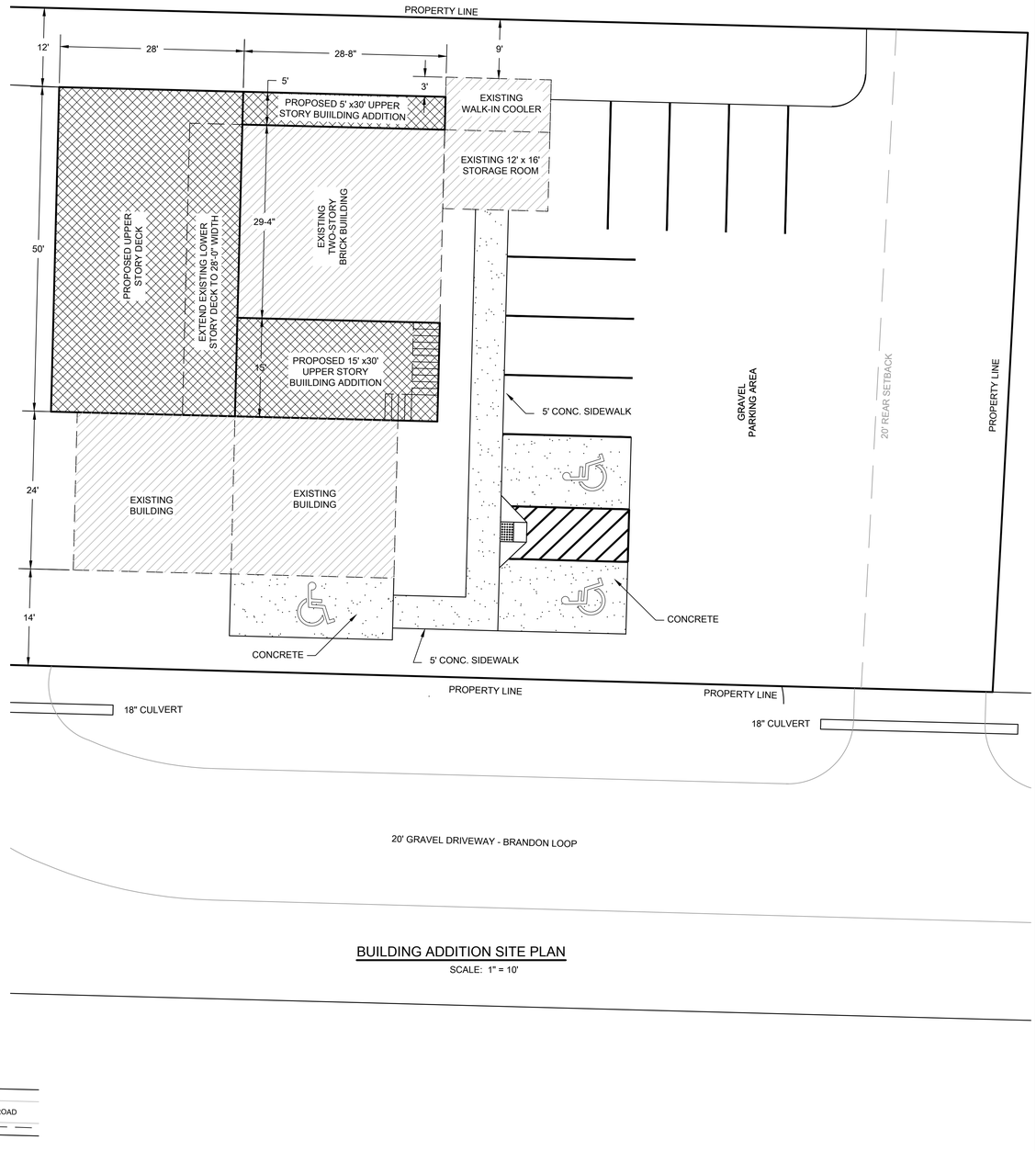
Part of the W ½ of the SW ¼ Section 21, Township 1 South, Range 14 West, Saline County, Arkansas, more particularly described as follows: Commencing at the SW corner of said W ½ SW ¼, thence East 600' to the West line of Brandon Road; thence N 01° 37' E along said road 350' to the Point of Beginning of land herein described; thence N 04° 31' 53' E 200.11'; thence N 88° 44' 20" W 308.55'; thence S 03° 22' 54" W 200.20'; thence S 88° 47' 30" E 99.93'; thence S 88° 47' 33" E 204.62' to the Point of Beginning. Tract contains 1.39 acres, more or less.

Legal Description – Road Easement, Brandon Loop, Bryant, AR

Part of the SW ¼ of the SW ¼ Section 21, Township 1 South, Range 14 West, Saline County, Arkansas, described as follows: Beginning at the SW corner of said Section 21, and run thence East 600' to the West line of roadway; run thence N 01°31' E along West line of road for 200' to the Point of Beginning of easement; thence N 01°31' E along West line of road for 50'; thence West parallel with the South line for 406.3'; thence South 50'; thence East to the Point of Beginning.




## SITE PLAN
SCALE: 1" = 50'




## BUILDING ADDITION SITE PLAN
SCALE: 1" = 10'

MICHAEL BOLIN
& ASSOCIATES, INC.
CONSULTING ENGINEERS
P.O. BOX 605, BENTON, AR 72018, (501) 776-2692
FAX (501) 776-2619 EMAIL: cmbolin@sbcglobal.net

BRYANT, ARKANSAS

SPRINGHILL TAVERN
2224 BRANDON LOOP

BUILDING ADDITION SITE PLAN

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
No. 4197
MICHAEL BOLIN

AS-BUILT DATE:

CONTACT PERSON:
M. BOLIN

SCALE:
AS SHOWN

DATE: MAY 2025

BUILDING ADDITION SITE PLAN

JOB NO.

SHEET NO.
1 OF 1

CREEKSIDE ADDITION, PHASE 2
REPLAT LOT 15 AND TRACT E

Bryant Planning Commission

# Subdivision Checklist

**Approved by**
**Bryant Planning Commission**
**07/14/2003 Revised 6/18/2007**

## Instructions

The attached checklist must be completed by the owner and subdivision engineer and must be submitted along with the Preliminary Plat Plan and other specified documentation for review and approval by the Planning Commission. The owner may not begin developing the subdivision until the review of the Preliminary Plat plan is approved.

**No changes or alterations can be made to the approved Preliminary Plat Plan** without Planning Commission approval.

When all lots have been surveyed, the utilities and drainage measures are in place, and roads have been constructed, the owner and engineer will submit a Final Plat Plan for approval by the Commission. This Final Plat Plan will incorporate all approved changes and will be verified by the City Engineer. No lots will be sold or rights-of-way and easements conveyed until the Final Plat has been submitted and approved.

**Fees due to City of Bryant upon submission of Preliminary Plat application**

- $300.00 + $3.00 per lot - for Subdivision preliminary plat review
- $250.00 or $25.00 per lot **(whichever is greater)** - Stormwater Detention and Drainage Plan Engineering Fee
- A Surety Bond or Cashier's check in the amount of 10% of the estimated development cost must be furnished within 10 days after Preliminary Plat approval.

**Fees due to Bryant Water and Sewer Department upon submission of Final Plat application**

- $100 per lot - Water/Sewer Impact Fee
- $100 per Subdivision Phase - Water/Sewer Flushing Fee

**Fees due to City of Bryant upon submission of Final Plat application**

- $25.00 + $1.00 per lot - for Subdivision Final Plat review

# City of Bryant Subdivision Checklist

**Subdivision/Project Name** CREEKSIDE ADDITION, PHASE 2 REPLAT LOT 15 AND TRACT E

**Contact Person** GEORGE WOODEN **Phone** (501) 408-4650

**Mailing Address** P. O. BOX 116, BENTON, AR 72018

## I. Basic Information Needed On The Plat

- ▲ 1. Name of Subdivision/Project
- ▲ 2. Current zoning R-1
- ▲ 3. Name and Address of owner of Record
- ▲ 4. Illustrate Source of Title giving deed record book and page number
- ▲ 5. Name & address of the sub-divider
- ▲ 6. Date of Survey
- ▲ 7. Vicinity map locating streets, highways, section lines, railroad, schools, & parks within ½ mile
- ▲ 8. Legal description of the property with exact boundary lines
- ▲ 9. Acreage of property
- ▲ 10. Number of Lots
- ▲ 11. Lot area in square feet
- ▲ 12. Lot lines with appropriate dimensions
- ▲ 13. Building setback lines
- ▲ 14. Preliminary Engineering certificate seal and signature on each page
- ▲ 15. Certificate of Engineering Accuracy
- ▲ 16. Certificate of Owner
- ▲ 17. Certificate of Final Plat Approval
- ▲ 18. Certificate of Recording
- ▲ 19. Show scale (not less than 1" = 100')
- ▲ 20. North Arrow
- ▲ 21. Show Title block
- ▲ 22. Show adjoining property owners
- ▲ 23. Layout of all proposed streets including traffic control devices (stop signs, speed limit, etc.)
- 24. Layout of all subdivision entrance street upgrades
- ▲ 25. Layout of all proposed alleys
- ▲ 26. Layout of all proposed sidewalk systems
- ▲ 27. Layout identifies any FEMA flood plain and flood way property within the 100-year flood elevation. (Provide Corp of Engineers 404 Permit if required)
- ▲ 28. Drainage easements for stormwater run-off and detention giving dimensions, locations, and purpose
- ▲ 29. Layout accommodates Master Street Plan segments within the boundaries
- ▲ 30. Street layout ties to existing adjoining subdivision stub-out streets and provides stub-out streets for future adjoining subdivisions.
- ▲ 31. Street width and right-of-way properly shown for each functional classification
- ▲ 32. Street centerlines showing angles of deflection, intersection, radii, length oftangents and arcs, and degree of curvature with basis of curve data
- ▲ 33. Typical cross section of streets
- ▲ 34. Location and name of existing streets
- ▲ 35. New street names that are not similar to existing street names
- ▲ 36. Show street lights
- ▲ 37. Show Fire Hydrant placement

- ▲ 38. Show and label all permanent & proposed easements
- ▲ 39. Any proposed open space must be shown
- ▲ 40. Show the direction and flow of all water courses entering the tract
- ▲ 41. Show the direction and flow of all water courses leaving the tract
- ▲ 42. The drainage area of all water courses above the points of entry.
- ▲ 43. The downstream drainage channel and drainage structures substantially impacted by the subdivision/project.
- ▲ 44. Show source of water supply
- ▲ 45. Show location of waste water connection to municipal main & sanitary sewer layout
- ▲ 46. A phasing plan outlining the boundaries for each phase

## II. Additional Information Needed, But Not Necessarily On The Plat

- ▲ 47. Natural features within the proposed subdivision including drainage channels, bodies of water, wooded areas, and other significant features
- ▲ 48. Existing streets, buildings, water courses, railroads. Culverts, utilities and easement on and adjacent to the tract.
- ▲ 49. Where method of disposal of wastewater is other than connection to a public waste water system, detailed information shall accompany the plat.
- ▲ 50. Calculations and field notes, including drainage calculations along with support drawing
- 51. Stormwater detention plan approval from City Engineer (attach copy of approval)
- ▲ 52. The Certificate of Preliminary Engineering Accuracy on each set of street and drainage plans.
- ▲ 53. ADA Accessibility Standard Form completed (and attached)
- ▲ 54. A Bill of Assurance has been prepared for this subdivision (and attached)
- ▲ 55. All lots comply with minimum square footage area and minimum lot width at the front building line
- ▲ 56. Street pavement design will be as specified by City or AHTD design procedures, approved by the City Engineer.
- ▲ 57. Made the "One Call" prior to site clearance or other excavation activity

## III. Preliminary Plat Attachments

**(Application will not be accepted until all attachment requirements are met)**

- ▲ 58. **Letter to Planning Commission** stating your request
- ▲ 59. Completed **Checklist**
- ▲ **60. Completed agreement to provide performance assurance**
- ▲ 61. **Subdivider Performance Bond or Cashier's Check** for infrastructure installation
- ▲ 62. Landscaping plan of any proposed common open space
- ▲ 63. **Draft of Bill of Assurance** proposed for the subdivision (if applicable)
- ▲ 64. **20 copies of Preliminary Plat Plan (folded)** that includes vicinity map (minimum size 17" X 34" paper)
- ▲ 65. **Two (2) IBM compatible diskettes or CDR's** with pertinent data and Plat in CAD compatible .DXF electronic file format
- ▲ 66. Copy of **Stormwater Detention approval**
- ▲ 67. 2 copies **Plan and profile** of all streets
- ▲ 68. Receipt for **$300.00 + $3.00 per lot for preliminary Subdivision fee**
- ▲ 69. Receipt for **$250.00 or $25.00 per lot (whichever is greater) for Stormwater Detention and Drainage Plan review**
- ▲ 70. Copy of **ADEQ Stormwater Pollution Prevention Plan** for property parcel containing one acre or larger.

## III. Final Plat Attachments

**(APPLICATION WILL NOT BE ACCEPTED UNTIL ALL ATTACHMENT REQUIREMENTS ARE MET)**

- 71. **Letter to Planning Commission** stating your request
- 72. Completed **Checklist**
- 73. **20 copies of Final Plat Plan (folded)** that includes vicinity map (minimum size 17" X 34" paper)
- 74. **Two (2) IBM compatible diskettes or CDR's** with pertinent data and Plat in CAD compatible .DXF electronic file format
- 75. **Bill of Assurance** including provisions set out in Title 15 Subdivision Regulations 15.16.01
- 76. Copy of **Water & Sewer Commission approval** or....
- 77. State Health Department approval of any new water supply and/or sewage system.
- 78. **Letter submitted by a Registered Professional Engineer, certifying that all infrastructure improvements and installations have been installed** in accordance with the submitted construction plans and drawings and the standards established by the City of Bryant and are functioning properly.
- 79. Infrastructure Maintenance Bond or Cashier's check.
- 80. Check for **$25.00 + $1.00 per lot for final Subdivision fee**
- 81. Check for **Water Sewer impact fees ($100.00 Flushing Fee and $100.00 impact fee per lot)**

CREEKSIDE ADDITION, PHASE 2 REPLAT LOT 15 AND TRACT E

Name of Subdivision

George P. Wooten

Surveyor

I HAVE COMPLIED WITH THE REQUIREMENTS LISTED ABOVE AND HAVE CHECKED ALL OF THE BOXES ON THE CHECKLIST WHICH APPLY TO THIS PROJECT SUBMITTAL.

Mike A. Lake

Owner Signature

Vernon J Williams

Engineer Signature

---

## CITY USE

Preliminary Plat Approved _____

Planning Commission Date _____

---

Final Plat Approved _____

Planning Commission Date _____

---

Proof of Recording - County _____

County Clerk _____ Date _____

GNE

3825 Mt Carmel Rd.
Bryant, AR 72022

**GarNat Engineering, LLC**

P.O. Box 116
Benton, AR 72018

July 14, 2025

Colton Leonard
City Planner
City of Bryant
210 SW 3rd Street
Bryant, AR 72022

Re: Replat of Lot 15 and Tract E – Creekside Addition, Phase 2

Dear Mr. Leonard:

Please allow this letter and the following list of enclosures to serve as my application for approval of the referenced replat. It is my desire that this matter be included on the agenda for your August 2025 City of Bryant Planning Commission meeting. The developer for the project is Diamond Development II, 1599 Lawson Oaks, Little Rock, Arkansas, 72210, jbhastingsjr@aol.com, 501-690-6601.

List of Enclosures

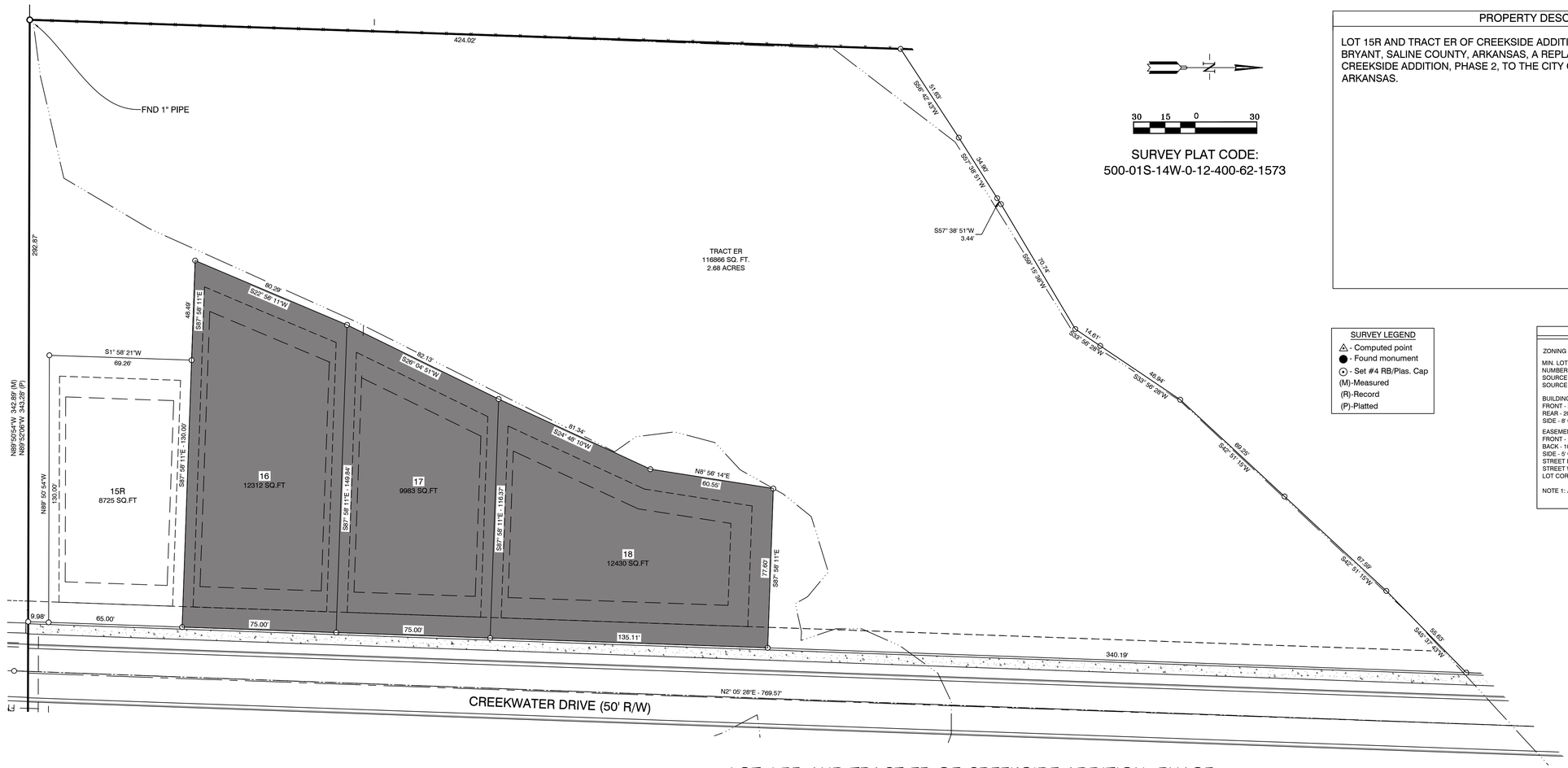
- Bryant Subdivision Checklist
- 8 copies of the replat
- Final replat review fee of $27.00

If you have questions or need any additional information, please do not hesitate to contact me.

Sincerely,

George P. Wooden

GarNat Engineering, LLC
George P. Wooden, PS #1573




SURVEY PLAT CODE:
500-01S-14W-0-12-400-62-1573

30 15 0 30

| PROPERTY DESCRIPTION: |
|---|
| LOT 15R AND TRACT ER OF CREEKSIDE ADDITION, PHASE 2, TO THE CITY OF BRYANT, SALINE COUNTY, ARKANSAS, A REPLAT OF LOT 15 AND TRACT E, CREEKSIDE ADDITION, PHASE 2, TO THE CITY OF BRYANT, SALINE COUNTY, ARKANSAS. |

SURVEY LEGEND
- △ - Computed point
- ● - Found monument
- ⊙ - Set #4 RB/Plas. Cap
- (M)-Measured
- (R)-Record
- (P)-Platted

PROPERTY SPECIFICATIONS:

ZONING CLASSIFICATION: R-1

MIN. LOT SIZE: 6000 S.F.
NUMBER OF LOTS: 1
SOURCE OF WATER: SALEM WATER USERS ASSOCIATION PWA
SOURCE OF SEWER: CITY OF BRYANT

BUILDING SETBACKS:
FRONT - 20' OR AS SHOWN
REAR - 20' OR AS SHOWN
SIDE - 8' OR AS SHOWN

EASEMENTS: UTILITY & DRAINAGE (D.E. & U.E.)
FRONT - 10' OR AS SHOWN
BACK - 10' OR AS SHOWN
SIDE - 5' OR AS SHOWN
STREET RIGHT OF WAYS: 50' OR AS SHOWN
STREET WIDTH: 28' BOC TO BOC
LOT CORNERS: SET #4 REBAR WITH CAP

NOTE 1: ALL GRINDER PUMPS AND SEWER SERVICE LINES WILL BE PRIVATE.

STATE OF ARKANSAS
REGISTERED PROFESSIONAL ENGINEER
NO. 9551
VERNON J. WILLIAMS

# LOT 15R AND TRACT ER OF CREEKSIDE ADDITION, PHASE 2, TO THE CITY OF BRYANT, SALINE COUNTY, ARKANSAS, A REPLAT OF LOT 15 AND TRACT E, CREEKSIDE ADDITION, PHASE 2, TO THE CITY OF BRYANT, SALINE COUNTY, ARKANSAS

## PLAT CERTIFICATES:

**OWNER:**
**Name:** Diamond Development II
**Address:** 1599 Lawson Oaks Drive, Little Rock, AR 72210

**DEVELOPER:**
**Name:** Diamond Development II
**Address:** 1599 Lawson Oaks Drive, Little Rock, AR 72210

**CERTIFICATE OF OWNER:**
We, the undersigned, owners of the real estate shown and described herein do hereby certify that we have laid off, platted and subdivided, and do hereby lay off, plat and subdivide said real estate in accordance with the within plat.

Date: _____ Signed: _____
Jim Hastings
1599 Lawson Oaks Drive, Little Rock, AR 72210

Date: _____ Signed: _____
Michael A. Lake
1599 Lawson Oaks Drive, Little Rock, AR 72210

Source of Title: SALINE COUNTY, ARKANSAS
Saline County Document# 2014-25641 & 2004-112595

**CERTIFICATE OF ENGINEERING ACCURACY:**

I, Vernon J. Williams, hereby certify that this plat correctly represents a survey and a plan made by me or under my supervision; that all monuments shown hereon actually exist and their locations, size, type, and material are correctly shown; and that all requirements of the City of Bryant Subdivision Rules and Regulations have been fully complied with.

Date: _____ Signed: _____
Vernon J. Williams
Registered Professional Engineer
No. 9551, Arkansas

**CERTIFICATE OF RECORDING:**

**CERTIFICATE OF SURVEYING ACCURACY:**

I, George P. Wooden, hereby certify that this plat correctly represents a boundary survey made by me or under my supervision; that the boundary lines shown hereon correspond with the description in the deeds cited in the above Source of Title; and that all monuments which were found or placed on the property are correctly described and located.

Date: _____ Signed: _____
George P. Wooden
Registered Land Surveyor
No. 1573, Arkansas

**CERTIFICATE OF FINAL PLAT APPROVAL:**

Pursuant to the City of Bryant Subdivision Rules and Regulations, this document was given approval by the Bryant Planning Commission. All of the document is hereby accepted, and this certificate executed under the authority of said rules and regulations.

Date: _____ Signed: _____
Lance Penfield, Chairman
Bryant Planning Commission

## DOCUMENTS USED:

- SURVEY PLAT OF RECORD RASBURRY SURVEYING 10/23/2014
- DEED OF RECORD 2014 PAGE 25641 WILLIAMS TO DIAMOND DEVELOPMENT II
- DEED OF RECORD 2004 PAGE 112595 THOMAS TO DIAMOND DEVELOPMENT II
- SURVEY PLAT OF RECORD MIDLAND FARM SUBDIVISION BY HENRY N. CONWAY 8/13/1951
- FINAL PLAT CREEKSIDE ADDITION, PHASE 2, DOCUMENT 2024-002360 BY GARNAT ENGINEERING FILED 02/12/2024
- REPLAT CREEKSIDE ADDITION, PHASE 2, DOCUMENT 2024-009671 BY GARNAT ENGINEERING FILED 06/04/2024

## BASIS OF BEARINGS:

BENCHMARK(S) PROVIDED ARE REBAR AND COORDINATES ON BENCHMARKS ARE NORTH AMERICAN DATUM 1983, ARKANSAS SOUTH ZONE, US SURVEY FEET, GRID COORDINATES AND ELEVATIONS ARE NAVD 1988. COORDINATES AND ELEVATIONS WERE ESTABLISHED USING GPS AND WERE PROCESSED USING THE NATIONAL GEODETIC SURVEY'S "ONLINE POSITIONING USER SERVICE" (OPUS).

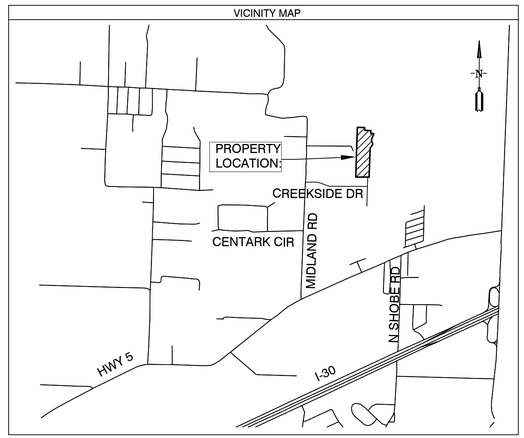
## CERTIFICATIONS:

BY AFFIXING MY SEAL AND SIGNATURE, I GEORGE P. WOODEN, PS NO. 1573, HEREBY CERTIFY THAT THIS DRAWING CORRECTLY DEPICTS A SURVEY COMPILED UNDER MY SUPERVISION ON OCTOBER 12, 2022.

THIS SURVEY WAS BASED ON LEGAL DESCRIPTIONS AND TITLE WORK FURNISHED BY OTHERS AND DOES NOT REPRESENT A TITLE SEARCH.

THIS PROPERTY IS LOCATED IN THE 100 YEAR FLOOD PLAIN. THE PROPERTY SHOW ON THIS PLAT IS LOCATED IN ZONE "X" AND ZONE "AE" OF THE F.E.M.A. MAP PANEL 05125C0240E EFFECTIVE DATE JUNE 5, 2020.

VICINITY MAP




| DATE | REVISION | BY |
|---|---|---|
| | | |

**GNE** Designing our client's success


GarNat Engineering, LLC
P.O. Box 116 (72018)
3825 Mt. Carmel Road
Bryant, AR 72022
Ph (501) 408-4650
Fx (888) 900-3068
garnatengineering@gmail.com


CREEKSIDE ADDITION, PHASE 2

PART OF THE EAST HALF OF THE NORTHWEST QUARTER SECTION 12, T-1-S, R-14-W, SALINE COUNTY, ARKANSAS

REGISTERED PROFESSIONAL SURVEYOR
STATE OF ARKANSAS
NO. 1573
SIGNATURE
GEORGE P. WOODEN

CONTENTS:
REPLAT OF LOT 15 AND TRACT E

PROJECT NO:
18054

DATE:
JULY 10, 2025

SHEET NO:
1

J:\Projects\2018 Projects\18054 Creekside Addition\Drawings\DWGs\18054-Creekside Addition-Phase-2-REPLAT Lot 15R and Tract ER-070825.dwg

# KINFOLK ACRES

ACE SIGNS

**PROPERTY BRAND/EXTENSION:** Kinfolk Acres LLC

**PROPERTY LOCATION:** 22000 I-30 Frontate Rd Suite 7

**PROPERTY CODE:** TBD

**DATE:** 06/12/2025

**SALES REP:** Jason McDonald

**PREPARED BY:** Victoria Phan

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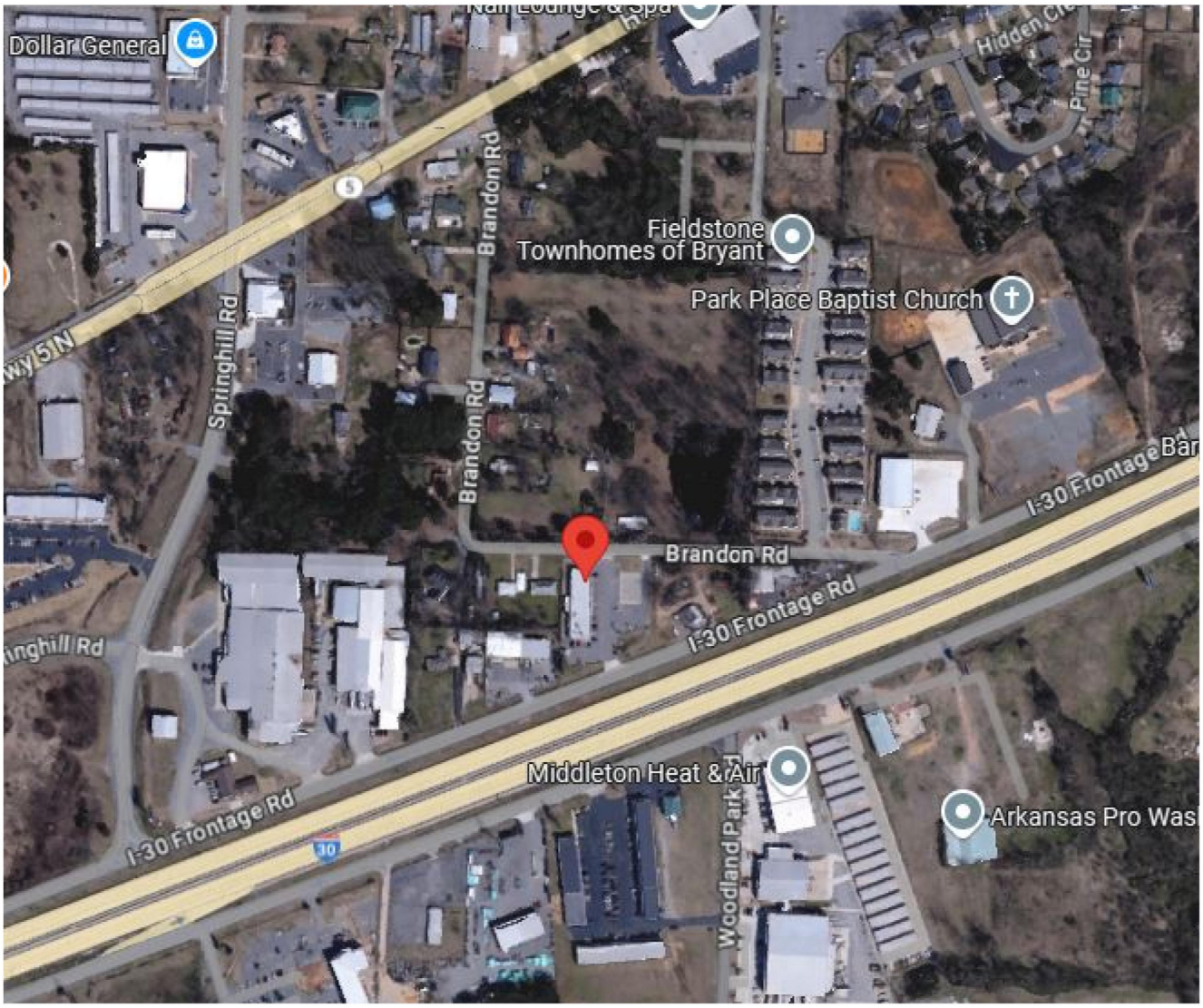
INITIALS: _____

# LOCATION MAP




| | | |
|---|---|---|
| **PROPERTY BRAND/EXTENSION:** Kinfolk Acres LLC | **PROPERTY LOCATION:** 122 Austin Lane Benton, AR 72015 | **PROPERTY CODE:** TBD |
| **DATE:** 06/12/2025 | **SALES REP:** Jason McDonald | **PREPARED BY:** Victoria Phan |

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INITIALS: _____

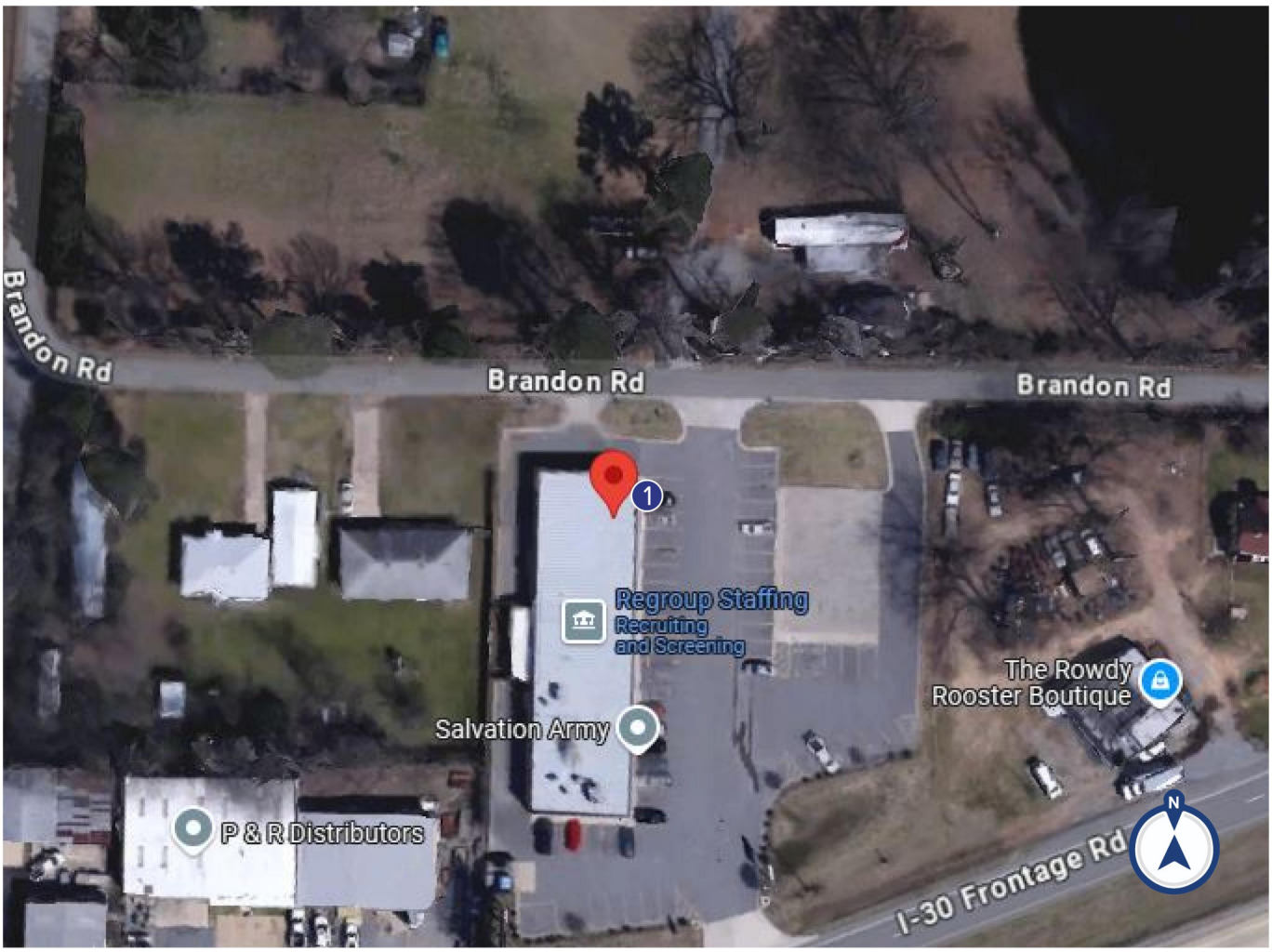
# SITE PLAN

**PROPOSED SIGNS:**

1. WALL CABINET

**EXISTING SIGNS:**

1. NO SIGN




ACE SIGNS

| PROPERTY BRAND/EXTENSION: | PROPERTY LOCATION: | PROPERTY CODE: |
|---|---|---|
| Kinfolk Acres LLC | 122 Austin Lane Benton, AR 72015 | TBD |

| DATE: | SALES REP: | PREPARED BY: |
|---|---|---|
| 06/12/2025 | Jason McDonald | Victoria Phan |

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INITIALS: _____

# 1 WALL CABINET

EXISTING

PROPOSED

RENDERINGS NOT TO SCALE

H3'-7" x W8' Wall cabinet with applied graphics

PANTONE WHITE

TO BE DETERMINED

TO BE DETERMINED

ACE SIGNS

**PROPERTY BRAND/EXTENSION:** Kinfolk Acres LLC

**PROPERTY LOCATION:** 122 Austin Lane Benton, AR 72015

**PROPERTY CODE:** TBD

**DATE:** 06/12/2025

**SALES REP:** Jason McDonald

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INITIALS: _____

WINE
NIGHT

**City of Bryant, Arkansas**
Community Development
210 SW 3rd Street Bryant, AR 72022
501-943-0943

# SIGN PERMIT APPLICATION

Applicants are advised to read the Sign Ordinance prior to completing and signing this form. The Sign Ordinance is available at www.cityofbryant.com under the Planning and Community Development tab.

Note: Electrical Permits may be Required, Please contact the Community Development Office for more information.

Date: 6/27/25

**Sign Co. or Sign Owner**

Name Lumatech
Address 6301 Murray Street
City, State, Zip Little Rock, AR 72209
Phone 501-217-9919 ext 115
Email Address service@lumatechservice.com

**Property Owner**

Name FCPS
Address 212 McClanahan Drive Unit 8
City, State, Zip Bryant, AR 72022
Phone 501-847-0375
Email Address krenuard@fcps-electric.com

**GENERAL INFORMATION**

Name of Business FCPS
Address/Location of sign 212 McClanahan Drive Unit 8 Bryant, AR 72022
Zoning Classification _____

**Please use following page to provide details on the signs requesting approval.** Along with information provided on this application, **a Site Plan showing placement of sign(s) and any existing sign(s) on the property is required** to be submitted**. Renderings of the sign(s) showing the correct dimensions is also required** to be submitted with the application. A thirty-five dollar ($35) per sign payment will be collected at the time of permit issuance. According to the Sign Ordinance a fee for and sign variance or special sign permit request shall be one hundred dollars ($100). Additional documentation may be required by Sign Administrator.

**READ CAREFULLY BEFORE SIGNING**

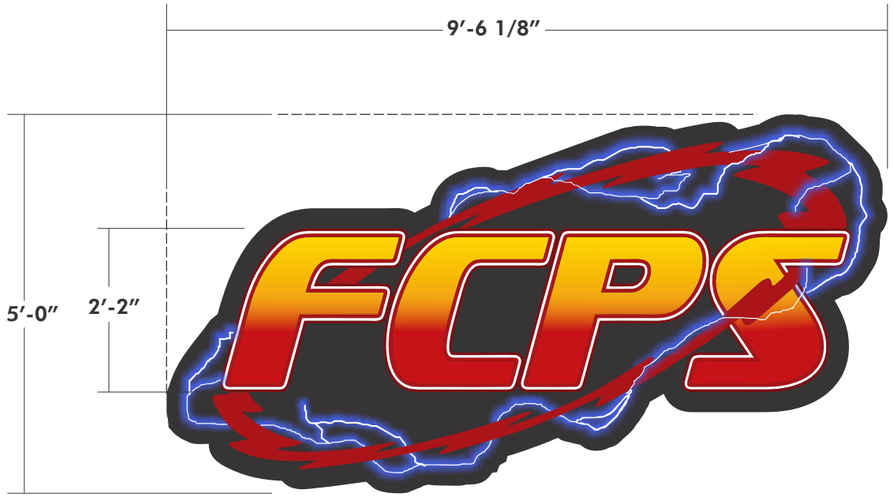
I Michelle Tucker, do hereby certify that all information contained within this application is true and correct. I fully understand that the terms of the Sign Ordinance supersede the Sign Administrator's approval and that all signs must fully comply with all terms of the Sign Ordinance regardless of approval. I further certify that the proposed sign is authorized by the owner of the property and that I am authorized by the property owner to make this application. I understand

that no sign may be placed in public right of way. I understand that I must comply with all Building and Electrical Codes and that it is my responsibility to obtain all necessary permits.

**Use table below to enter information regarding each sign for approval. Please use each letter to reference each sign rendering.**

| SIGN | **Type** (Façade, Pole, Monument, other) | **Dimensions** (Height, Length, Width) | **Sqft** (Measured in whole as rectangle) | **Height of Sign** (Measured from lot surface) | | Column for Admin Certifying Approval |
|---|---|---|---|---|---|---|
| | | | | Top of Sign | Bottom of Sign | |
| A | Facade | 9'-6 1/8" x 5'-0" | 48sqft | 25' | 20' | |
| B | | | | | | |
| C | | | | | | |
| E | | | | | | |
| F | | | | | | |
| G | | | | | | |

212 McCLANAHAN DRIVE UNIT 8
BRYANT, AR 72022




FRONT VIEW SCALE 1/2″=1′-0″

SIDE VIEW

**A**

5″ DEEP CUSTOM CONTOUR SHAPED CABINET PAINTED BLACK WITH WHITE LED ILLUMINATION. FACES TO BE ROUTED ALUMINUM WITH 3/4″ THK. PUSH THRU ACRYLIC GRAPHICS. DECORATION TO BE TRANSLUCENT DIGITALLY PRINTED VINYL WITH UV LAMINATE APPLIED FIRST SURFACE AND WHITE DIFFUSER APPLIED SECOND SURFACE.

SIGN TO BE UL APPROVED AND BEAR UL LABEL

47.55 SQ. FT.

NIGHT VIEW

PROPOSED ELEVATION SCALE NTS

LUMATECH
BRIGHT PEOPLE. BRIGHTER SOLUTIONS.

6301 MURRAY STREET
LITTLE ROCK, AR 72209
888-771-5341
WWW.LUMATECHSERVICE.COM

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CUSTOMER APPROVAL

WE ARE PROUD MEMBERS OF: PLASMA

REVISIONS

1 02-19-2025: Removed Options A/B. Increased Size.
2
3
4
5
6
7

LOCATION

FCPS
212 McCLANAHAN DRIVE UNIT 8
BRYANT, AR 72022

DATED: 01-22-2025
FILENAME: FCPS Exterior Wall Sign v2
CONTACT: RYAN ALLRED
501-217-9919